ANNUAL REPORT FOR TREATABILITY STUDIES AT ROCKY FLATS PLANT "ISCAL YEAR 1991

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U S DEPARTMENT OF ENERGY
Rocky Flats Plant
Golden Colorado

ENVIRONMENTAL RESTORATION PROCRAM

March 1992

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Rocky Flats Plant
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ENVIRONMENTAL RESTORATION PROGRAM

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The Annual Report on the Treatability Studies at Rocky Flats Plant (RFP) summarizes the results and progress of the Treatability Studies Program within the Environmental Restoration (ER) Program for Fiscal Year 1991, October 1, 1990 through September 30, 1991. The ER Program is a comprehensive effort consisting of site characterization, remedial investigations, feasibility studies and remedial/corrective actions to address environmental contamination at the RFP. These activities are pursuant to the Inter-Agency Agreement (IAG) developed among the U.S. Department of Energy (DOE), the U.S. Environmental Protection Agency (EPA), and the Colorado Department of Health (CDH)

The Final Treatability Studies Plan (TSP) was issued in August 1991 and was developed in accordance with Article XI of Attachment 2 of the IAG. The Final TSP evaluated candidate remedial technologies for various types of contamination identified at RFP. The sitewide treatability study program is intended to address technologies applicable to remediation efforts at two or more operable units (OUs) at RFP and is separate from any treatability study testing which may be conducted as part of remedial actions at individual OUs. EPA/DOE correspondence and the Treatability Studies Plan outlined the requirement for annual reports on the Treatability Studies Program. Annual reports supersede the IAG requirements for a Final Treatability Study report in 1993. Annual reports will provide information on the current status of the program and briefly summarize any reports issued for individual treatability studies. Additional site characterization data for RFP will be reviewed and compared to Applicable or Relevant and Appropriate Requirements (ARARs) to determine if any changes in contaminants of concern have occurred. Annual reports will also review and revise the technology evaluation presented in the Final TSP to account for new information on site contamination data, ARARs, and innovative technologies.

The technologies were identified and screened in the Final TSP and Annual Report based on the potential for application to the following contaminant types present in soil, sediments, surface water, and groundwater volatile organic compounds, semivolatile organic compounds, polychlorinated biphenyls (PCBs), inorganics, metals, and radionuclides. The semivolatile organic compounds and PCBs were identified as new contaminant categories for the Annual Report. The technologies which passed the preliminary screening were subjected to a final screening. The final screening determined if the technology should be included in the sitewide treatability test program at this time. Statements of Work (SOWs) were prepared for technologies selected for laboratory or bench-scale testing.

Four water treatment technologies including ozonation, peroxide oxidation, ultraviolet (UV) oxidation, and UV photolysis were identified for bench or laboratory scale treating with application to PCBs in surface water. This supplements the other technologies for surface or groundwater previously identified in the Final TSP, including ion exchange, oxidation/reduction, adsorption, potassium ferrate precipitation (TRU-ClearTM) and ultrafiltration/microfiltration

Soil/sediment treatment technologies were previously selected in the Final TSP for bench or laboratory scale testing and include physical separation, soil washing, the solidification/stabilization/fixation technologies, epoxy polymerization, polyester polymerization, portland cement, masonry cement, gravimetric physical separation (TRU CleanTM), and magnetic separation. Slurry phase bioreactor treatment technology was identified in the Annual Report for possible pilot testing of PCB-contaminated soil/sediment. Ozonation and UV photolysis were identified for pilot testing of volatile organic compounds (VOCs) and semivolatiles in surface water and groundwater. These technologies will continue to be evaluated for suitability for pilot testing as part of the sitewide Treatability Program.

The Final TSP identified the chemical oxidation technologies ozonation, peroxide oxidation, ultraviolet oxidation, and ultraviolet photolysis for pilot testing treatment of VOC-contaminated groundwater/surface water. The evaluation and selection process in this Annual Report eliminated the peroxide oxidation and ultraviolet oxidation technologies from pilot testing as part of the sitewide program because bench and pilot testing of ultraviolet peroxide oxidation is in progress at OU1

Treatability testing in progress for various OUs at RFP include technologies for treatment of radionuclides in soils and surface water, VOCs from groundwater and suspended solids from surface water. UV-oxidation tests for OU1 groundwater evaluated the removal of VOCs using ultraviolet light and hydrogen peroxide. Test results showed removal of VOCs from the aqueous phase. Analysis of the offgas showed that the VOCs may have been stripped versus destroyed. Further evaluation is being conducted to determine if this stripping occurs in full-scale equipment. An on-site operations test is planned for early 1992 as part of the OU1 Interim Remedial Action.

Testing for the removal of actinides by physical size separation from soils at OU2 was conducted using gravimetric separation in conjunction with wet/dry sieving and attrition or rotary scrubbing. Preliminary results suggest that particle size separation warrants further consideration for treatment of soils contaminated with radionuclides. Additional testing using different types of soils and chemical additions to wash water is needed to evaluate its applicability to RFP soils contaminated with radionuclides.

Treatability testing for OU2 included use of granular activated carbon (GAC) for removal of VOCs from contaminated groundwater. Coagulation/precipitation/filtration was evaluated for removal of suspended solids. Treatability tests for the removal of metals and radionuclides using GAC, ion exchange, chemical precipitation and adsorption were planned, but surface water collected for the testing did not contain sufficient concentrations of radionuclides to conduct these tests. Vacuum-enhanced vapor extraction has been identified for pilot-scale in situ testing for the removal of free-phase volatile organic compounds from the subsurface as part of an Interim Measure/Interim Remedial Action (IM/IRA) for OU2. In situ steam stripping is also being considered in the IM/IRA for pilot testing based on bench-scale testing being conducted at Lawrence Livermore National Laboratory. Dehalogenation and chemical oxidation have been identified for bench-scale testing

Bench-scale testing for the Techtran (now known as the Colloid Polishing Filter Method) Technology was conducted on radionuclide-contaminated groundwater from RFP. Eight tests were conducted and evaluated, based on removal of radioactive tracers. Bench-scale tests at RFP were conducted on surface water collected from OU4 and based on the results, a demonstration test will be conducted at RFP. A series of new bench tests will be repeated to provide more data for implementing the demonstration program at OU4 in 1992.

Work plans to test physical separation and magnetic separation processes for removal of radionuclides from soil and plans to test micro/ultrafiltration, oxidation/reduction and potassium ferrate precipitation processes to remove metals, radionuclides or organics from water will be completed in Fiscal Year 1992

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ACRONYMS AND ABBREVIATIONS

Am Americium

AnBAC Anaerobic Biological Activated Carbon

ARAR Applicable or Relevant and Appropriate Requirements
ATTIC Alternative Treatment Technology Information Center

AWQC Ambient Water Quality Criteria

BDAT Best Demonstrated Available Technology

CDH Colorado Department of Health

CERCLA Comprehensive Environmental Response, Compensation, and Liability Act

CLP Contract Laboratory Program

CMFS Corrective Measures/Feasibility Studies
CTMP Comprehensive Treatment Management Plan

DMSO Dimethyl Sulfoxide
DOE Department of Energy

EDTA Ethylenediaminetetraacetic Acid
ELM Emulsion Liquid Membranes
EM Environmental Management
EPA Environmental Protection Agency

ER Environmental Restoration

FFCA Federal Facility Compliance Agreement

GAC Granular Activated Carbon

GPM Gallons Per Minute

HEA Health Effects Assessment IAG Inter-Agency Agreement

IHSS Individual Hazardous Substance Site
IM/IRA Interim Measure/Interim Remedial Action
IM/IRAP Interim Measure/Interim Remedial Action Plan

IR Infrared Radiation
IRA Interim Response Action
IRAP Interim Remedial Action Plan

ISV In Situ Vitrification
ITPH Interceptor Pump House

IWT International Waste Technologies
KPEG Potassium Polyethylene Glycol
LDR Land Disposal Requirements

LLNL Lawrence Livermore National Laboratory

LPDE Low Density Polyethylene
MCL Maximum Contaminant Level
MCLG Maximum Contaminant Level Goal

MDL Minimum Detection Limit

NTIS National Technical Information Service

O&M Operations and Maintenance

OSWER Office of Solid Waste and Emergency Response

OU Operable Unit

PACT Powdered Activated Carbon Treatment

PCB Polychlorinated Biphenyls pCi/l Picocuries per Liter PEG Polyethylene Glycol

ACRONYMS AND ABBREVIATIONS (Concluded)

PQL Practical Quantitation Limit
PSI Peroxidation Systems, Inc

Pu Plutonium Ra Radium

RCRA Resource Conservation and Recovery Act RFEDS Rocky Flats Environmental Data System

RFI RCRA Facility Investigation

RFP Rocky Flats Plant

RI/FS Remedial Investigation/Feasibility Study

RI-CMS/FS Remedial Investigation - Corrective Measures Study/Feasibility Study

ROD Record of Decision

RTIS Remedial Technology Information System

SARA Superfund Amendments and Reauthorization Act

SDWA Safe Drinking Water Act

SITE Superfund Innovative Technology Evaluation

SO Systems Operation
SOW Statement of Work
SVE Soil Gas Vapor Extraction

TBC To-Be-Considered
TCA Trichloroethane
TCE Trichloroethylene

TCLP Toxicity Characteristics Leaching Procedure

TDS Total Dissolved Solids

TEA Triethylamine

TIS Technology Investment Strategy

TSP Treatability Studies Plan

U Uranıum UV Ultraviolet

USCS Unified Soil Classification System

VOA Volatile Organic Analysis
VOC Volatile Organic Compound

WERL Water Engineering Research Laboratory

WQC Water Quality Criteria

WQCC Water Quality Control Commission

 μ g/l Micrograms per Liter

The Annual Report for Treatability Studies at Rocky Flats Plant (RFP) summarizes the results and progress of the Treatability Studies Program within the Environmental Restoration (ER) Program for Fiscal Year 1991, October 1, 1990 through September 30, 1991. The ER Program is a comprehensive effort consisting of site characterization, remedial investigations, feasibility studies, and remedial/corrective actions to address environmental contamination at RFP.

The Final Treatability Studies Plan (TSP) was issued in August 1991 and was developed to evaluate candidate remedial technologies for various types of contamination identified at RFP. The sitewide treatability study program addresses technologies applicable to contaminants identified in two or more operable units (OUs) at RFP and supplements treatability testing which may be conducted for individual OUs. The Final TSP outlined the requirements for Annual Reports on the Treatability Studies Program.

The Annual Report reviews the current status of the program and summarizes the information available for individual treatability studies. Additional site characterization data for RFP are reviewed and compared to Applicable or Relevant and Appropriate Requirements (ARARs). The Annual Report reviews, reevaluates, and rescreens the technologies presented in the Final TSP to account for new information on site contamination data, ARARs, new information on previously identified technologies, and innovative technologies.

The Annual Report provides a mechanism to support the Remedial Investigation/Feasibility Study (RI/FS) and other programs and to transfer and share information and results of treatability testing for those programs they support. The following sections outline the objectives of the report in reviewing and presenting new data, information, and results

1 1 NEW SITE CHARACTERIZATION DATA

To identify changes in the RFP characterization, new site characterization data from the Rocky Flats Environmental Data System (RFEDS) were reviewed. This included inputs to the RFEDS database since the development of the Final TSP, validated and corrected data, and new data from recent sampling and analytical testing programs. New contaminants and changes in the maximum and minimum contaminant concentrations were identified for surface water, groundwater, soils, and sediments

The site characterization data were reviewed to identify if contaminant concentrations in specific media were greater than ARAR values in two or more OUs for screening and evaluation in the Annual Report If ARAR values were exceeded in only one OU, the containment group was not included in the Annual

Report and will be addressed in the feasibility studies for the particular OU Previous summary tables presented in the Final TSP were reviewed and updated for this report

12 REVIEW OF ARARS

An RFP summary of possible and potential sitewide chemical-specific ARARs including Groundwater Quality Standards, Federal Surface Water Quality Standards, Statewide and Basin Surface Water Quality Standards, and Stream Segment Surface Water Standards was reviewed and updated for the Annual Report. The revisions were based on the review of additional site characterization data from RFEDS, the review of new state regulatory standards for groundwater and surface water, and corrections to tables used for the Final TSP. The development of possible and potential sitewide ARARs provides a preliminary list of remediation goals for the development of feasibility assessments and studies. These goals serve to develop alternatives for remedial technologies for particular contaminants and media at RFP. The ARARs listing will continue to be reviewed and refined.

1 3 TREATABILITY STUDY PROJECTS

The Annual Report summarizes treatability studies, interim reports, and other information from research studies available since the Final TSP was issued in August 1991. This information is considered in the review of the treatability technology selection process for future bench-scale and pilot-scale testing and reevaluation of previously selected technologies. Future treatability testing projects for individual OUs and the sitewide program are also discussed.

1 4 SCREENING AND SELECTION OF TECHNOLOGIES

The technology selection completed in the Final TSP was reviewed, reevaluated based on additional data, and expanded for the Annual Report. The site characterization data were reviewed and compared to updated ARARs values to identify major contaminant types and associated media that are present at RFP. A literature search was conducted to identify new, innovative, or emerging technologies for consideration in the screening process. This literature search also compiled new information presently available for review on technologies previously considered in the Final TSP.

Technologies were reviewed, reevaluated, and screened using a two-step process. The preliminary screening process associates technologies with major contaminant categories and their applicability to RFP. The criteria used in the preliminary screening process include applicability, removal efficiency, potential to meet the cleanup goal, technology maturity, operations and maintenance (O&M) requirements, implementability, and adverse impacts

The final screening process evaluated significant advantages and compared proven technologies to determine if they should be included in the sitewide Treatability Studies Program. This included

effectiveness, cost, O&M, and reduction in adverse impacts. This final screening for inclusion of technologies in the sitewide Treatability Studies Program for bench and pilot-scale testing will be reevaluated in each Annual Report. Information on the cost of pilot-scale treatability testing was developed for the selected technology. New Treatability Statements of Work (SOWs) were developed for new technologies selected for the sitewide Treatability Studies Program.

1.5 ANNUAL REPORT ORGANIZATION

This first Annual Report on Treatability Studies is divided into five sections and four appendices. Section 1 0 provides an introduction and Annual Report objectives. Section 2 0 presents and reviews new site contamination data and ARARs, and describes the literature search for new information on technologies. Section 3 0 summarizes the status of treatability studies at RFP and future treatability testing. Section 4 0 presents the procedures used to review the technology selection and the results of the review. Section 5 0 lists the references reviewed in developing this document.

Appendices include Appendix A - Potential Applicable or Relevant and Appropriate Requirements (ARARs) for the Sitewide Treatability Studies Program, Appendix B - Technology Data Summaries for Groundwater/Surface Water Treatment Technologies Reviewed in the Annual Report, Appendix C - Technology Data Summaries for Soil/Sediment Treatment Technologies Reviewed in the Annual Report, and Appendix D - Statements of Work for New Technologies Selected for Treatability Tests

This section reviews new site contaminant data, ARARs, and additional literature for revising, updating and expanding screening tables previously completed in the Final TSP. New analytes at concentrations greater than possible and potential ARARs must be found in two or more OUs to be included in sitewide treatability studies. If ARARs values were exceeded in only one OU, the particular contamination was not considered in the Final TSP or Annual Report but will be evaluated in feasibility studies for the particular OU.

2 1 SUMMARY OF NEW CONTAMINANT DATA

To update the contaminant data in the Annual Report, maximum concentrations that were reported in the August 1991 Final TSP were reviewed against maximum values obtained from the RFEDS computer database. In many instances, this updating has resulted in increases in the maximum values reported in Table 2-1. This is not necessarily due to actual increases in contamination levels, but results from updating data that previously existed but had not been inputed to RFEDS. For a few analytes, such as calcium in groundwater, surface water, and soils, maximum concentrations shown in Table 2-1 were reduced from those previously reported in the Final TSP (Table 4-2). Some values used in the Final TSP were taken from draft reports or were considered preliminary. These data were subject to change following finalization of the reports or validation of the data. The data used to update maximum concentrations in Table 2-1 were extracted from RFEDS, prior to January 1992, and are also subject to change based on revisions to the database.

A number of new analytes are reported in Table 2-1 These include maximum and minimum values in the following categories

- Metals category
 - Boron (groundwater)
 - Phosphorous (groundwater, surface water, sediments)
- Anions
 - Orthophosphate (groundwater, surface water)
 - Phosphate (groundwater, surface water)
 - Total Kjeldahl nitrogen (surface water)
 - Total organic carbon (surface water, soils)

- Radionuclides
 - Plutonium (Pu) 238 (groundwater, surface water, sediments)
- Volatiles
 - Bromoform (groundwater, surface water)
 - Dibromochloromethane (surface water)

Plutonium has historically been reported as Pu 239, 240 The recent appearance of Pu 238 in the RFEDS database is being investigated

The largest number of new analytes were found in the semivolatiles category. New compounds listed in Table 2-1 that have been identified for the Annual Report include acenaphthylene, aldrin, alpha-BHC, alpha-chlordane, ametryn, atrazine, benzo(a)pyrene, benzoic acid, benzyl alcohol, beta-BHC, butyl benzyl phthalate, 4-chloro-3-methylphenol, 4-chlorophenyl phenyl ether, cyanazine, delta-BHC, dibenzo(a,h)anthracene, dibenzofuran, dicamba, 1,4-dichlorobenzene, dichloroprop, 2,4-dimethylphenol, 2,4-dinitrotoluene, endosulfan, ethyl parathion, gamma-BHC (Lindane), hexachlorobenzene, isophorone, 4-methylphenol, naphthalene, 2-nitrophenol, 4-nitrophenol, 4-nitroanaline, N-nitroso-di-N-propylamine, pentachlorophenol, prometon, prometryn, propazine, simazine, simetryn, terbuthylazine, and 1,2,4-trichlorobenzene

Polychlorinated biphenyls (PCBs)-Arochlor-1254 have been detected in surface water, sediments, and soils at RFP during preliminary investigations. Maximum values that were identified during preliminary investigation for the Aroclor-1254 are shown in Table 2-1

22 ARAR IDENTIFICATION

To provide a basis for determination of preliminary contaminants of concern, ARARs were developed based on Section 121(d) of the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA), as amended by the Superfund Amendments and Reauthorization Act of 1986 (SARA), which requires that fund-financed, enforcement, and federal facility remedial actions comply with applicable or relevant and appropriate federal laws or promulgated state laws, whichever are more stringent. A summary of possible or potential sitewide chemical-specific ARARs is presented in Appendix A in Table A-1, Groundwater Quality Standards, Table A-2, Federal Surface Water Quality Standards, Table A-3, Statewide and Basin Surface Water Quality Standards, and Table A-4, Stream Segment Surface Water Quality Standards. Values presented in Appendix A of this report were corrected and updated from Appendix A in the Final TSP to include chemicals suspected to be present at RFP and current (as of February 1, 1992) federal and state health and environmental statutes and regulations. These ARARs are considered preliminary and will be subject to change as new federal and

state standards are imposed, and as additional information from the baseline risk assessment and site characterization investigations for each OU become available for development of feasibility studies. The final ARARs determination for each OU will be completed as part of the record of the decision process conducted for that specific OU

Possible or potential sitewide ARARs were selected from Appendix A for comparison to sitewide maximum and minimum analyte concentrations in Section 2.3. The ARARs selected for comparison include maximum contaminant level (MCL) for drinking water, federal Ambient Water Quality Criteria (AWQC), and Colorado statewide, basinwide and stream-segment standards for surface water, groundwater, and radionuclides. The EPA's Health Effects Assessment (HEA) criteria for the ingestion of carcinogens and systemic toxicants in soil and water (U.S. EPA 1989a) were also selected. To-beconsidered (TBC) maximum contaminant level goals (MCLGs), not yet effective, were not selected as ARARs for use in the Final TSP and Annual Report.

As the Remedial Investigations for RFP proceed, additional information will become available through the risk assessment process which will allow a determination of acceptable contaminant concentrations to ensure protection of human health and the environment. Development of a preliminary list of possible or potential chemical-specific ARARs allows the establishment of a list of preliminary remediation goals in the Feasibility Study process. This is a tentative listing of contaminants and preliminary anticipated cleanup concentration or risk levels for each medium. Preliminary remediation goals will serve to focus the development of alternatives on remedial technologies that can achieve the remediation goals. As more information becomes available, chemical-specific ARARs may become more refined as constituents are added or deleted.

Possible and potential ARAR values from Appendix A were selected for comparison to maximum and minimum analyte levels in Table 2-1 A comparison of the ARAR values for surface water, groundwater, and soil is presented in Table 2-2 to show the revisions between Annual Report and Final TSP document (Table 4-2) A number of these changes were due to an expanded listing of chemical data available from the RFEDS database Other changes were due to new state regulatory standards for groundwater and surface water. The process for selecting potential ARAR values was also modified slightly from that presented in the Final TSP For the Annual Report, the most stringent federal or state standard (excluding MCLGs at zero) or HEA criterion was used as the principal ARAR for both surface water and groundwater Maximum Contaminant Level TBCs (standards to become effective in 1992 or 1993) were included for consideration as potential ARARs. For those chemicals which had no federal or state standard, the lowest systemic or carcinogenic HEA criterion was used for surface water and Where any of these standards were below the detection limit (minimum value in Table 2-1), the detection limit was listed as the potential ARAR The decision was made for the Annual Report to include the state agricultural values for consideration in developing the possible and potential ARARs The Final TSP did not consider the state agricultural values when developing the ARARs

The potential soil ARARs/TBCs were based on the lowest HEA criterion (systemic or carcinogenic) with the detection limit used as the default value where the lowest HEA criterion was below the detection limit. This process is consistent with the methodology used in the Final TSP. The potential ARAR value for plutonium in soils or sediments was based on State of Colorado (1985) Rules and Regulations Pertaining to Radiation Control. The potential ARARs for gross alpha and gross beta emissions in soils and sediments were based on DOE and CDH requirements (U.S. DOE, February 1990 and CDH, December 1985)

2 3 SUMMARY OF CONTAMINANTS IN TWO OR MORE OUS AND COMPARISON TO ARARS

The following subsections review data screening conducted by media for the Annual Report The results of the comparison to ARARs and identification of analytes which exceeded ARARs in two or more OUs are presented in Table 2-3

2 3 1 Groundwater

Elevated levels (e.g., above ARARs) of inorganics, metals, volatile and semivolatile organics, and radionuclides have been detected at various individual hazardous substance sites (IHSS's) within a given OU. Those analytes which exceeded ARARs in two or more OUs have been considered in sitewide treatability studies.

As shown in Table 2-3, maximum values in groundwater exceeded ARARs in two or more OUs for the inorganic chemicals chloride, cyanide, nitrate, nitrate + nitrite, and sulfate. In addition, pH values and total dissolved solids (TDS) concentrations exceeded ARARs for groundwater. These were noted in the Final TSP and no additional analytes were identified for the Annual Report.

Metals exceeding ARARs, as noted in the Final TSP for groundwater in two or more OUs, included arsenic, cadmium, chromium, iron, lead, manganese, and selenium. Additional analytes identified for the Annual Report include aluminum, cobalt, copper, mercury, nickel, vanadium, and zinc

Maximum values in groundwater exceeding ARARs in two or more OUs, as reported in the Final TSP, include 1,1-dichloroethene, 1,1,1-trichloroethane, 1,1,2-trichloroethane, carbon tetrachloride, methylene chloride, tetrachloroethene, trichloroethene, and vinyl chloride. Additional volatile organics identified for the Annual Report include 1,2-dichloroethane, 1,2-dichloroethene, 1,2-dichloropropane, benzene, and chloroform.

Semivolatile organics in groundwater were not identified in the Final TSP in two or more OUs—Based on the review of the database output, bis(2-ethylhexyl)phthalate and N-nitrosodiphenylamine were identified above groundwater ARARs for the Annual Report

Radionuclides exceeding ARARs in two or more OUs for groundwater for the Final TSP include gross alpha activity. Additional radionuclides exceeding ARARs for the Annual Report include gross beta activity, radium (Ra) 226, Ra 228, strontium 90, tritium, and uranium (U) total

232 Surface Water

As reported in the Final TSP, maximum values in surface water exceeding ARARs in two or more OUs for the inorganic chemicals include chloride, nitrate, nitrate + nitrite, and sulfate. Values of pH both higher and lower than ARARs were recorded for surface water, and total dissolved solids (TDS) concentrations also exceeded ARARs in surface water in the Final TSP. Cyanides were the only additional analyte or parameter identified for the Annual Report.

Metals exceeding ARARs, as noted in the Final TSP for surface water in two or more OUs, include aluminum, antimony, arsenic, barium, beryllium, cadmium, chromium, iron, lead, and manganese Additional metal analytes were identified for the Annual Report and include copper, mercury, nickel, selenium, silver, thallium, and zinc

Volatile compounds exceeding ARARs in two or more OUs as reported in the Final TSP include 1,1-dichloroethene, carbon tetrachloride, methylene chloride, tetrachloroethene, and trichloroethene Additional analytes were identified for the Annual Report and include 1,1,2-trichloroethane, 1,1,2,2-tetrachloroethane, 1,2-dichloroethene (total), chloroform, and vinyl chloride

For the Annual Report, semivolatile compounds exceeding ARARs in surface water in two or more OUs include alpha-chlordane, bis(2-ethylhexyl)phthalate, di-n-butylphthalate, naphthalene N-nitrosodiphenylamine, and phenol Based on preliminary investigation results, PCBs were reported at concentrations above ARARs in surface water for more than two OUs

The radionuclides identified in the Final TSP as exceeding ARARs include gross alpha and gross beta activity and plutonium (Pu) 239+240, radium (Ra) 226, tritium and uranium (total) in two OUs Additional radionuclides were identified for the Annual Report and include americium (Am) 241, and Ra 228

2 3 3 Soils and Sediments

Few chemicals were reported in the Final TSP as exceeding ARARs in soils or sediments. This is due to the soil and sediments database being more limited than the database for groundwater and surface water. Also, few ARARs are available for soils and sediments, and numerical values of ARARs which do exist are relatively high. The only chemicals reported in the Final TSP at concentrations exceeding ARARs were the metal beryllium in soils and sediments and the radionuclides gross alpha activity in soils and sediments, and Pu 239+240 in soils and sediments. For the Annual Report, PCB Arochlor-1254,

based on preliminary investigation results, was the only additional analyte reported in concentrations above ARARs in soils

24 LITERATURE SEARCH

A literature search of published materials was conducted to obtain and review new information on treatment technologies. The following computer databases were researched using Dialog as a gateway

- Enviroline
- Pollution Abstracts
- Environmental Bibliography
- Compendex
- National Technical Information Service (NTIS)

Initially, a list of titles was generated based on the search using key words and subjects. This material was reviewed and abstracts were requested for articles and papers identified as appropriate. A review of journal articles, conference proceedings, and federal publications was also conducted to complement the database searches. This literature search was used to supplement the previous information compiled for the Final TSP. This included references developed for application to Superfund sites, Resource Conservation and Recovery Act (RCRA) Best Demonstrated Available Technology (BDAT) studies, standard engineering textbooks, DOE studies, and other project experience. The following technology databases were accessed.

- Alternative Treatment Technology Information Center (ATTIC), U.S. EPA
- Technology Data Base DOE Research and Waste Management, Oak Ridge, Tennessee
- Remedial Technology Information System (RTIS), DOE Idaho National Engineering Laboratory, Idaho Falls, Idaho
- National Technical Information Service, U.S. Department of Commerce, Springfield,
 Virginia
- Rocky Mountain Arsenal Technology Data Base, U.S. Army Program Manager's Office,
 Commerce City, Colorado
- Office of Solid Waste and Emergency Response (OSWER) Bulletin Board System, U S
 EPA Technology Innovation Office, Washington, D C
- Water Engineering Research Laboratory (WERL), Treatability Data Base System, Risk Reduction Engineering Laboratory, U.S. EPA, Cincinnati, Ohio

New references reviewed and used in this report are presented in Section 5 0 and in the appendices for each technology data summary

This section summarizes treatability studies interim reports and results from other RFP research studies generated since the Final TSP. This information was considered in the review of the treatability technology selection for the Annual Report. The status of the projects and plans for Fiscal Year 1992 are also discussed.

One research report has been issued and addresses the bench-scale testing of physical size separation for treatment of radionuclide-contaminated soils at OU2 New and additional information on the Colloid Polishing Filter Method (formerly Techtran) process for treatment of radionuclides in water were reported Bench-scale tests were conducted using RFP groundwater

Bench-scale tests of granular activated carbon (GAC) treatment of water contaminated with volatile organic compounds (VOCs) have been conducted on surface waters from OU2 Bench-scale tests for removing suspended solids by coagulation, precipitation, and filtration were also conducted Bench-scale tests of the use of ultraviolet (UV) hydrogen peroxide oxidation treatment of OU1 groundwater contaminated with VOCs were conducted

Pilot-scale tests were performed as part of the OU2 surface water IM/IRA and are planned for the OU2 subsurface IM/IRA. The screening process for bench and pilot-scale studies is described in Section 4.0

3 1 BENCH-SCALE TESTING

3 1 1 OU1 Groundwater IM/IRA Tests

Bench-scale tests were conducted for treatment of OU1 groundwater contaminated with VOCs using UV/hydrogen peroxide oxidation treatment. In September 1991, bench-scale testing was performed to further evaluate the oxidation of chlorinated solvents in groundwater using ultraviolet light and hydrogen peroxide. The purpose of this investigation was to determine operating and design parameters prior to the startup of the OU1 Interim Measure/Interim Remedial Action (IM/IRA) full-scale unit in 1992.

A single composite sample was prepared from groundwater taken from five representative wells in OU1 and sent to Peroxidation Systems, Inc. (PSI), in Tucson, Arizona. PSI performed four optimization tests to determine the best operating conditions prior to running a confirmation test.

Based on preliminary results, the tests demonstrated that concentrations of volatiles in effluent water were reduced to acceptable levels. Analysis of off-gas samples taken during testing yielded values as high as 3100 ppb 1,1,1-trichloroethane. It appears that a significant level of reduction occurred due to

stripping caused by the evolution of gas bubbles. At this time, an evaluation has not been completed to establish if similar stripping occurs in full-size equipment. Test results showed that destruction/removal efficiencies were greater with a hydrogen peroxide concentration of 50 ppm as opposed to 100 ppm, and a pH of 5 as opposed to an unadjusted pH of 7.5. The test indicated improved performance after pretreatment consisting of the addition of a flocculent (alum) combined with filtration. The results of this bench-scale test will be used as a basis for the system operation scheduled for early 1992.

3 1 2 OU2 Surface Water IM/IRA Tests

Bench-scale tests were conducted on samples of OU2 surface water contaminated with VOCs using several types of GAC in a column configuration. Analyses of the water sample prior to treatment indicated that the following VOCs were present. 1,2-dichloroethane [97 micrograms per liter μ g/l)], chloroform (33 μ g/l), 1,1,1-trichloroethane (13 μ g/l), carbon tetrachloride (140 μ g/l), trichloroethane (97 μ g/l), and 1,1,2,2-tetrachloroethane (52 μ g/l). Preliminary results indicate that VOCs can be removed to below detection limits for all experimental conditions tested. No differences were indicated among the various types of GAC tested.

Bench-scale treatability tests were also performed to evaluate coagulation/precipitation/filtration technologies for removal of suspended solids. Jar settling tests and a combination of jar settling followed by sand column filtration tests were conducted. Several different coagulants were tested at various dosage rates and pH levels. Preliminary results show that direct filtration without using coagulants may be feasible. Provisions for chemical addition and precipitation may be required for full-scale treatment. These operations would be used periodically when influent suspended solids levels are elevated.

In addition to the tests described above, the OU2 Treatability Study Program planned to conduct bench-scale testing for removal of radionuclides and metals from surface water using GAC, ion exchange, chemical precipitation, and adsorption on selected adsorbents. These tests were not performed because OU2 surface water did not contain sufficient concentrations of radionuclides for bench-scale testing.

3 1 3 Physical Separation

The removal of actinides from soils at OU2 was bench tested in 1989, and the results are presented in Research Report RFP-4479 dated September 12, 1991. Removal of actinide-contaminated fine clay particles from soils was tested using a gravimetric separator (mineral jig) in conjunction with wet sieving In addition, dry sieving, attrition scrubbing, and rotary scrubbing were evaluated.

Wet sieving removed more than 98 percent of the radionuclide activity from coarse gravel to coarse sands, less than 50 0 to 4 0-mm, based on the Unified Soil Classification System (USCS) grain-size scale. When the soil was first size-separated and then wet sieved, more than 99 percent of the activity was removed. The decontaminated soils fraction of less than 50 0 to 4 0-mm represented greater than 50 weight percent of the untreated soils in each test.

Actinide removal from coarse to medium sands, less than 4 0- to 2 4-mm, and fine sands, less than 2 4-to 0 42-mm, followed a selected sequence. Attrition scrubbing removed more contamination than wet sieving which removed more contamination than rotary scrubbing. Attrition scrubbing was found to enhance the actinide removal prior to wet sieving of coarse to medium sands and fine sands by 10 percent and 20 percent, respectively. The mineral jig removed actinide-containing clays from the <0 42-mm fractions. The americium was lowered from 100 to 11 pCi/g in 4 weight percent of the soil (<0 42 to 0 25 mm).

The tests discussed above were the results of bench testing of gravimetric physical separation (TRU CleanTM) and other size separation techniques for the removal of radionuclide contamination from RFP soils. These were research tests conducted using wind-blown soils obtained from the southeast corner of the 903 Pad. The test showed that significant decontamination of coarse particle size ranges could be achieved. The tests did not evaluate soil washing to remove radionuclides from the soil particles. Additional tests using different types of soil from other areas of contamination at RFP would be useful. The report did not present any conclusions regarding whether the available data were sufficient to establish that physical separation techniques should be implemented for cleanup of radionuclide contaminated soils at RFP.

These preliminary results suggest that particle size separation warrants further consideration for treatment of soils contaminated with radionuclides. Additional testing will be required to determine if this technology is applicable for implementation at RFP. Soil washing and gravimetric physical separation (TRU Clean) were selected for inclusion in the sitewide Treatability Test Program in the Final TSP.

3 1 4 Colloid Polishing Filter Method

Bench-scale tests were conducted for the Techtran process (now known as the Colloid Polishing Filter Method). This technology has been selected for demonstration at RFP as part of the EPA Superfund Innovative Technology Evaluation (SITE) program. The contaminated groundwater was passed through filter beds composed of Filter-Flow-1000 material with and without chemical pretreatment. The work was carried out with RFP groundwater recovered from the OU4 interceptor pump house (ITPH) #95, using radioactive tracers (Pu 239, Am 241 and Ra 226). The ITPH #95 water, mostly bicarbonate (pH 7 6), contained approximately 31 picocuries per liter (pCi/l) of U 238. The purpose of these experiments was

to evaluate the feasibility of the technology and to establish an optimum condition for maximum retention of radionuclides such as U, Pu 239, and Am 241

Eight different experimental conditions were tested including various values of pH adjustment and additions of sodium sulfide and/or sodium bisulfite. The purpose of sodium bisulfite was to reduce U+6 to the U+4 state and Pu+4 to the Pu+3 state. The sodium sulfide addition was added to generate insoluble metal sulfides and allow them to precipitate

The influent or intermediate effluent and final effluent were analyzed for various major and trace elements with special emphasis on U, Pu 239, and Am 241 radionuclides. Based on the radionuclide results, all eight experimental conditions appear favorable for a future demonstration. The retention factors for U, Pu 239, and Am 241 range from 200 to 1000 (which equals approximately 95 5 to 99 9 % removal). Since the effluent values are below or at the detection limits (0.05 pCi/l), the true retention factors may be higher. It has not yet been determined which process conditions are most favorable for retention. Additional bench tests are in progress. A decision will be made based on these tests prior to the OU4 field demonstration planned for 1992.

3 2 PILOT-SCALE TESTING

A pilot test of the use of GAC treatment of OU2 surface water contaminated with VOCs is in progress. This program is to be expanded to include microfiltration for the removal of heavy metals and radionuclides. A test of the pilot groundwater extraction and treatment system at OU1 is planned for March 1992.

3 2 1 OU1 IM/IRA Systems Operation Test

The OU1 IM/IRA Systems Operation (SO) Test on the Total System is an IAG scheduled evaluation of the overall performance of the groundwater recovery and treatment system. The testing is scheduled to take place in spring 1992. The test objectives are to ensure proper operation of each component, evaluate the performance of the system, determine operating parameters, and identify potential problems in future operations.

The test includes hydrostatic testing, which was initiated in summer 1991, of lines and process equipment, instrument calibration, and testing of the groundwater recovery system. However, a major portion of the test will be committed to the evaluation of the UV/hydrogen peroxide treatment system and the ion exchange system. The OU1 IM/IRA bench-scale test on UV/hydrogen peroxide treatment was used as a precursor to the SO test. This test indicated the need for evaluating precipitation, VOC emissions, and adsorption of the UV light by suspended solids, as well as overall removal efficiency for VOCs. Testing of the ion exchange system will include testing the regeneration system, evaluating

removal efficiencies, and adjusting the operating parameters of the system to achieve improved performance

Upon completion of the testing, and after analytical results are received, an SO test report will be prepared. The SO test report will detail the tests performed and the results of those tests, as well as make conclusions and recommendations about the groundwater recovery/treatment system.

3 2 2 OU2 Surface Water IM/IRA Pilot Tests

A pilot GAC treatment system for treatment of surface water in OU2 began operation in spring 1991 and is scheduled to continue operation until summer 1992. The system was designed to treat 1,1-dichloroethene, 1,1-dichloroethane, 1,2-dichloroethane, chloroform, carbon tetrachloride, trichloroethene, and tetrachloroethene. The system has been effective in treating VOCs. However, only 1,2-dichloroethene, carbon tetrachloride, trichloroethene, and tetrachloroethene have been identified above detection limits in the surface water collected for testing. The system design capacity was 60 gallons per minute (gpm), while the average flow rate treated to date has been 14 gpm. No major problems have been encountered. A draft report on the pilot treatability study is due to the agencies in spring 1992.

A pilot test of a radionuclide removal system is planned as Phase II of this test program. This will involve the addition of a microfiltration system for the removal of radionuclides and heavy metals to the existing GAC process. The microfiltration system is expected to begin operation in the spring of 1992 and operation is planned to continue through summer 1993.

3 3 TREATABILITY STUDY WORK PLANS

Pilot-scale treatability testing to address the residual free-phase VOCs for OU2 and the radionuclide contamination beneath 903 pad for OU2 will be evaluated and coordinated through the Subsurface Interim Measure/Interim Remedial Action Plan (IM/IRAP). In situ vacuum-enhanced vapor extraction has been identified for implementation of a pilot test in the Subsurface IM/IRA. In situ steam stripping is being considered for pilot testing in the IM/IRA and potentially has the capability to recover VOCs and radionuclides. This technology is presently being tested at Lawrence Livermore National Laboratory in Livermore, California. Bench-scale treatability testing of dehalogenation and chemical oxidation will be conducted in the future to determine if these remedial technologies are applicable for the OU2 site and warrant pilot-scale testing. The Subsurface IM/IRAP will be released for public comment in 1992.

Two physical separation treatability study work plans (TRU Clean[™] and Magnetic Separation) for the treatment of radionuclide-contaminated soil will be submitted to the EPA and CDH for their review in November 1991. A work plan for soil washing of plutonium will be developed and soil washing experiments will be performed in 1992.

The work plan for Treatability Studies of Different Types of Oxidation/Reduction Processes will be completed and submitted to EPA and CDH for review early in 1992. Bench-scale tests are planned in 1992. A work plan for the Ultrafiltration/Microfiltration Treatability Study is presently under development and will be submitted to the EPA and CDH in early 1992. Bench-scale tests are planned in 1992. A work plan for testing potassium ferrate precipitation (TRU-Clear) for removal of radionuclides, metals, and organics from water will be prepared in Fiscal Year 1992.

A feasibility study will be conducted for OU1 in fiscal year 1992 The feasibility study process may include additional treatability studies for soil/sediments and groundwater/surface water

3 4 REMEDIATION TECHNOLOGIES

As part of the overall treatability study program outlined in the IAG, DOE has initiated a comprehensive investigation of methods potentially available for use in corrective/remedial action. These studies are consistent with section XI of the IAG and will cover the range of alternatives required for the analysis of remedial alternatives during both IRA planning and Corrective Measures/Feasibility Studies (CM/FS). Under this program, studies will be conducted to provide sufficient data to allow remedial alternatives to be fully developed and evaluated during feasibility studies, to support the remedial design of selected alternatives, and to reduce cost and performance uncertainties for remedial alternatives. Sitewide treatability studies are being performed to expedite the screening of treatment technologies and alternatives. In the same manner, this program will expedite the remediation process by evaluating and testing existing and innovative technologies that enhance site characterization and assessment, subsurface contaminant collection and recovery, and in situ remediation. Projects are in progress or will be developed with DOE's Office of Technology Development, EPA's Office of Research and Development, the U.S. Geological Survey, and various universities. Potential activities include the evaluation, development, testing, and demonstration of procedures and technologies in the following categories.

- Environmental Characterization and Assessment (eg, geophysical techniques, drilling technologies, downhole chemical sensors, in situ radiometric detectors, hydrologic testing, monitoring system design, data mapping and display, contaminant fate and transport, two-phase flow systems, hydrologic and geochemical modeling, statistical and geostatistical analysis)
- In situ Remediation (eg, groundwater contaminant recovery systems, soil vapor extraction, steam stripping, dehalogenation, chemical oxidation, bioremediation)

In Fiscal Year 1992, RFP will plan, organize, and implement a program of applied environmental research, technology evaluation and testing in the areas of site characterization, assessment and in situ remediation that focuses specifically on technical RFP environmental restoration issues

3 5 RELATED TECHNOLOGY DEVELOPMENT PROGRAMS

3 5 1 Radionuclide Control Plan

A work plan titled Final Work Plan for the Control of Radionuclide Levels in Water Discharges from RFP will be issued in January 1992 as part of the Inter-Agency Agreement. This work plan requires identification of potential improvements in treatment to be used in the event that water quality for the terminal ponds exceeds Colorado standards. The work plan includes proposals in four areas. (1) improving present treatment, (2) characterizing the physicochemical nature of radiochemical contaminants, (3) tracking potentially applicable treatment methods developed by others, and (4) considering additional bench-scale treatability tests.

RFP currently provides treatment to remove certain waterborne contaminants from RFP pond water prior to discharge. Treatment includes particulate filtration and GAC. Analysis of available data indicates that current operation is minimally effective at removing radiochemical contaminants, which are thought to be associated with colloids/particulates in the micron to sub-micron size range. Improvements to the current treatment approach will be pursued in the future. General facility improvements are being implemented including consolidating operations into a weather-proofed facility and providing piped conveyances for Pond B-5 and Pond C-2 water to the Pond A-4 Treatment Facility. Treatment process enhancements to be evaluated include installation of improved bag/cartridge filters and multimedia sand filters. Bag/cartridge filter improvement evaluation will involve testing of various filter bags and cartridges to determine particulate removal efficiencies. A pilot testing program will be initiated to evaluate multimedia sand filtration as the first or second unit operation in the treatment process. Particle counting technologies are being used to directly measure filtration effectiveness and produce specific particle distributions for unit (treatment) operations which can remove micron-sized particles.

The characterization of radionuclide contaminants will include chemical characterization and speciation and identification of sources and potential source control measures. The characterization will identify factors important to changes in solubility, complexation, and adsorption of radiochemical contaminants. This information will assist in developing and implementing specific treatment approaches for removal of low-level radiochemical contaminants from pond water. The study will also identify sources and transport mechanisms that result in radiological contaminants in RFP pond water. This effort will be accompanied by identification and testing of appropriate control technology to eliminate exceedances of Colorado standards.

The work plan includes provision for evaluating potentially applicable technologies and conducting bench-scale treatability testing, as appropriate. This will include monitoring the technology review process and treatability test programs conducted as part of the sitewide Treatability Studies Program Technology evaluations and testing conducted at individual OUs will also be monitored. The work plan

proposes conducting annual reviews of these potentially applicable technologies which will be incorporated and addressed in future annual reports

3 5 2 Comprehensive Treatment and Management Plan

The Land Disposal Requirements (LDR) requires hazardous waste to be treated to meet the best demonstrated available technology (BDAT) prior to being placed in a landfill. EPA has identified BDAT as either specific technologies (e.g., incineration) or as specified numerical standards. In addition, in order to discourage generators from attempting to avoid the disposal standards simply by storing the waste forever, the LDR regulations prohibit indefinite storage of hazardous and mixed wastes. In order to comply with these LDR provisions, the RFP Federal Facility Compliance Agreement (FFCA) was implemented. Implementation of the requirements of the FFCA allows for continued operation (i.e., generation and storage of mixed waste) while providing time for DOE to develop the technologies required to come into full compliance with the LDR regulations.

The Comprehensive Treatment and Management Plan (CTMP) is the foundation on which ultimate compliance with LDR is based. This plan will describe why treatment technologies are needed, how specific technologies were selected, and the applicability of technologies to the LDR problem at RFP Schedules and milestones for developing and implementing the chosen technologies will be identified. The Annual LDR Progress Report is a requirement and will provide an update and status on the scope and magnitude of LDR mixed-waste issues at RFP including quantities in storage, storage locations, progress in LDR determinations and characterization efforts, and treatment technology implementation. Ultimate compliance can not be achieved until such time that LDR wastes can be treated and disposed of in the proper manner. As a result, the majority of activities involved in this project are centered around the development and implementation of treatment technologies for hazardous and radioactive waste. The IAG treatability studies program is focused on treatment of soil and water contaminated with much lower levels of hazardous constituents than LDR wastes.

3 5 3 Technology Investment Strategy

To help focus resources on the projects that have the greatest potential, RFP is working toward a Technology Investment Strategy (TIS). This strategy is the management plan for technology development activities, priorities and resources. A systems analysis approach is being developed to determine which projects to pursue, which projects to abandon, and what criteria to use in making those choices. Projects will be ranked in order of importance and solutions developed utilizing formalized decision analysis techniques. Solutions identified for consideration can include administrative changes, implementing waste minimization technologies, implementing waste treatment technologies, or developing additional characterization or analysis capabilities. The systems analysis methodology will provide the basis for selecting technologies for the CTMP. The strategy will seek to leverage RFP efforts.

with technical research and development efforts at other DOE laboratories, universities, and, when applicable, private-sector companies

This Annual Report has been designed to review, reevaluate and rescreen technologies identified in the Final TSP for inclusion in the Treatability Studies Program based on new site characterization data, ARARs, and the literature search. The Annual Report also evaluates and screens new technologies identified or additional information obtained on existing and innovative technologies.

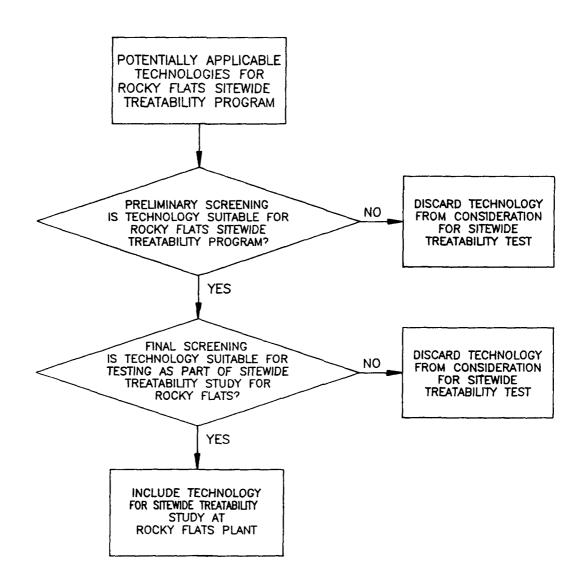
The methodology for technology selection employed for the Annual Report is the same as that applied in the Final TSP. This section briefly summarizes that methodology and presents the results of the updated technology screening for the Treatability Studies Program.

4 1 TECHNOLOGY SELECTION PROCESS

The site characterization data were reviewed and compared to available ARARs to identify major contaminant types and associated media that exist at RFP. A literature/database search was conducted to identify new information on technologies potentially applicable to the contaminant types and media identified in two or more OUs at RFP. These technologies were then subjected to a two-step screening process. The preliminary screening identified those technologies suitable for application at RFP. The final screening identified which of these technologies to include in the sitewide Treatability Studies. Program. The two-step screening method is illustrated in Figure 4-1. Statements of Work (SOWs) were prepared for new technologies selected for treatability testing.

4 1 1 Review of Site Characterization Data and ARARs

The site characterization data and ARARs were updated as previously described in Sections 2.1 and 2.2 Information on ARARs was updated as described in Section 2.2. The updated site characterization data were compared in Section 2.3 to identify those contaminants which were found to exceed ARARs in two or more operable units at RFP. The contaminants identified were grouped in categories of contaminant type (e.g., volatile organics) and media (e.g., groundwater)



US DEPARTMENT OF ENERGY Rocky Flats Plant, Golden, Colorado

SPECIFIC SELECTION PROCESS AS APPLIED TO TECHNOLOGIES TO BE INCLUDED IN ROCKY FLATS SITEWIDE TREATABILITY TEST PROGRAM

4 1 2 Review of Technology Data

The review of technology data included a status review of ongoing treatability test programs at RFP and a review of new information on potentially applicable technologies. The status of treatability tests in progress at RFP was summarized in Section 3.0. Sources of information that were used include literature/database searches, review of conference proceedings, EPA guidance documents, government reports, and vendor information. The review included technologies applicable to newly identified contaminant categories, newly identified technologies, and new information on previously screened technologies.

4 1 3 Preliminary Screening Process

The preliminary screening of treatment technologies consisted of identifying and associating the applicable technologies with the major contaminant categories, and screening to select technologies suitable for application at RFP. The following criteria were applied in identification of technologies for screening.

- Potential applicability to new major contaminant categories that were identified
- New technologies identified with potential applicability to any major contaminant category
- Innovative technologies for which new information relevant to the selection process was obtained from other RFP testing programs or from literature
- Applicability to contaminant categories in two or more OUs

The criteria for technologies applicable to two or more OUs were previously applied during the final screening in the Final TSP

New technologies identified and technologies applicable to newly identified contaminant categories were included in the preliminary screening process. Technologies previously screened in the Final TSP, for which additional information was available, were also included. Technology data summaries were prepared for each technology included in the screening process. These data summaries are presented in Appendix B for groundwater/surface water treatment technologies and in Appendix C for soil/sediment treatment technologies.

The preliminary screening process is illustrated in Figure 4-2 Criteria for the preliminary screening include the following

- Applicability
- Removal efficiency
- Potential to meet cleanup goal

- Technology maturity
- O&M requirements
- Implementability
- Adverse impacts

The decision to retain a technology for evaluation of treatability testing was an engineering judgment based on the information available from the literature search and other sources

4 1 4 Final Screening Process

The final screening process selected those technologies suitable for inclusion in the sitewide Treatability Study Program and is illustrated in Figure 4-3. An evaluation was made if additional information from treatability testing was needed for selection of the technology for application at RFP. If additional information was not required, the technology was not considered for testing

The technology was then compared to other proven technologies. If the technology offered no significant advantages in terms of effectiveness, cost, O&M requirements, or reduction in adverse impacts, it was eliminated from further consideration for testing. Those technologies retained after evaluation according to these criteria were included in the treatability program if the technology could be tested at the laboratory or bench scale. A preliminary assessment was made of the anticipated EPA, state, and community acceptance of pilot testing of those technologies which would require treatability testing at this scale. Technologies were not selected or rejected for pilot testing based on this preliminary assessment on acceptance by the EPA, state, and community

The final screening process for the Annual Report is intended to review and update the technology selection completed in the Final TSP. The final screening process includes those technologies retained following the preliminary screening process and those technologies previously considered in the final screening process in the Final TSP, for which new information is available having substantial impact on the screening process. The final screening also included technologies which were retained in the Final TSP after preliminary screening and not subjected to final screening because no analytes were identified that exceeded ARARs in two or more OUs in the Final TSP. These technologies were subjected to a final screening based on the updated review of ARARs and contamination data in this Annual Report

Statements of Work (SOWs) were prepared for new technologies selected for the sitewide Treatability Studies Program for the Annual Report. These SOWs are included in Appendix D of this report and supplement SOWs prepared for the Final TSP. An order of magnitude cost estimate was prepared for pilot testing of identified technologies to serve as an input into decisions regarding priority and scheduling of tests.

POTENTIALLY APPLICABLE TECHNOLOGIES FOR ROCKY FLATS SITEWIDE TREATABILITY PROGRAM

PRELIMINARY SCREENING CRITERIA

- APPLICABILITY TO CONTAMINANT TYPE AND MATRIX
- REMOVAL EFFICIENCY
- POTENTIAL TO MEET CLEANUP GOALS
- . TECHNOLOGY MATURITY
- OPERATING AND MAINTENANCE REQUIREMENTS
- IMPLEMENTABILITY
- ADVERSE IMPACTS

TECHNOLOGY SUITABLE FOR ROCKY FLATS SITEWIDE TREATABILITY PROGRAM?

YES

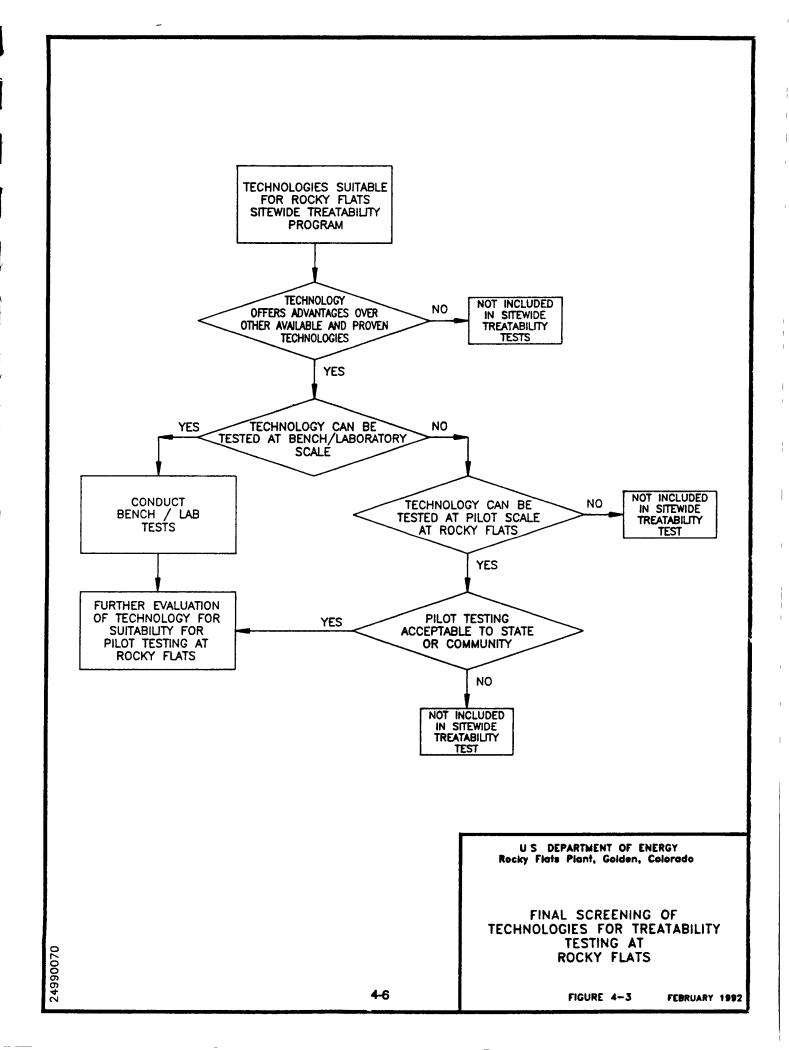
SCREEN TECHNOLOGY FOR SUITABILITY FOR BENCH, LAB, OR PILOT TESTING AT ROCKY FLATS DISCARD TECHNOLOGY FROM CONSIDERATION FOR SITEWIDE TREATABILITY TEST

NO

U S DEPARTMENT OF ENERGY Rocky Flats Plant, Golden, Colorado

PRELIMINARY SCREENING OF TECHNOLOGIES FOR SUITABILITY FOR ROCKY FLATS SITEWIDE TREATABILITY PROGRAM

24990060



4 1 5 Pilot Testing Evaluation

The process for evaluating the suitability of technologies for pilot testing is presented in Figure 4-4. This procedure, adapted from the EPA guidance document for conducting treatability studies, was designed to allow the continuous evaluation of new information for each technology based on bench-scale testing and a literature search through the life of the treatability program. The technologies selected for pilot testing in the Final TSP and the Annual Report will be reevaluated annually. The review will include additional information on ARARs, permits, cleanup levels, agency approval, and environmental risks of pilot testing. Relative costs for implementing a program for pilot and full-scale testing will be prepared, as appropriate

42 TECHNOLOGIES EVALUATION AND SELECTION SUMMARY

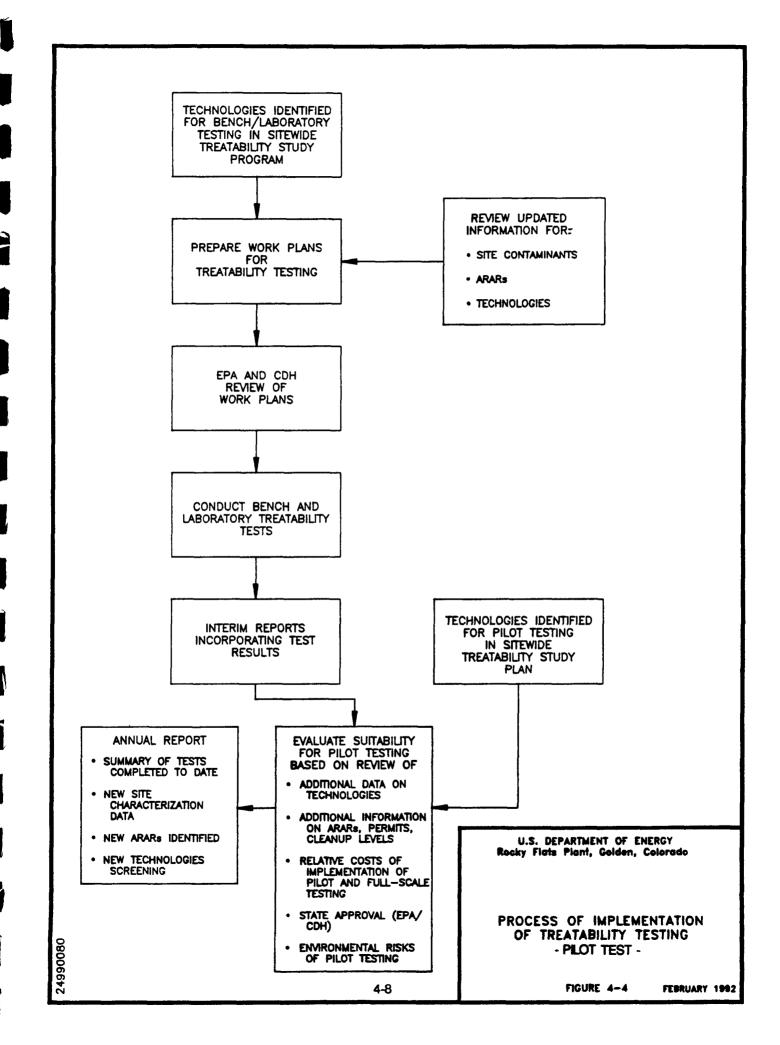
This section presents the results of the technology selection process for technologies that are appropriate for inclusion in the sitewide Treatability Studies Program. The technologies which were preliminarily screened are presented in Section 4.2.1. The final technology screening process results are presented in Section 4.2.2.

A technology data summary was prepared for each treatment technology subjected to screening. The data summaries for groundwater/surface water treatment technologies are included in Appendix B, while those for soil/sediment treatment technologies are included in Appendix C. Statements of Work were prepared for each technology selected for testing and are presented in Appendix D 6.

421 Preliminary Screening

The technologies applicable to groundwater or surface water matrices identified for preliminary screening are listed in Table 4-1A. This table includes technologies applicable to these contaminant groups volatile organics, semivolatile organics, PCBs, inorganics, metals, and radionuclides. Some new technologies identified for the preliminary screening are not innovative or emerging technologies but were not previously identified in the literature search for the Final TSP. The technologies applicable to soil or sediment matrices which were identified for preliminary screening are listed in Table 4-1B. This table includes technologies applicable to the contaminant groups PCBs, metals, and radionuclides. Two or more OUs were identified to have contaminant concentrations which exceeded ARARs for each of these contaminant groups, as presented in Table 2-2. The contaminant group PCBs was previously discussed in the Final TSP, but no technologies were screened prior to the Annual Report.

The preliminary screening for groundwater/surface water technologies is presented in Table 4-2A and that for soil/sediment technologies is presented in Table 4-2B. The technologies retained for final screening are presented in Table 4-3A for groundwater/surface water, and Table 4-3B for soil/sediments



The groundwater/surface water technologies included for final screening for the contaminant group semivolatiles includes technologies which were retained following preliminary screening in the Final TSP These technologies were not subjected to final screening in the Final TSP since, at that time, semivolatile contaminants were not identified in two or more OUs. The rationale for rejection of those technologies not retained is presented in Table 4-4A for groundwater/surface water, and Table 4-4B for soil/sediments.

422 Final Screening

The final screening process for groundwater/surface water technologies is presented in Table 4-5A, and for soil/sediment treatment technologies in Table 4-5B. The final screening process in these tables includes some technologies which were previously subjected to final screening in the Final TSP for which new information warranted a new review.

The groundwater/surface water treatment technologies identified for laboratory or bench-scale testing in the final screening process are presented in Table 4-6A. Adsorption, ion exchange, oxidation/reduction, ultrafiltration/microfiltration, and potassium ferrate precipitation (TRU-Clear) were all previously selected in the Final TSP. Potassium ferrate precipitation is to be tested for the removal of radionuclides and metals and potentially, organics. The other technologies are to be tested on both metals and radionuclides. Oxidation technologies such as ozonation, peroxide oxidation, UV oxidation, and UV photolysis technologies were identified for testing with application to PCBs. SOWs are included in Appendix D.

The soil/sediment treatment technologies identified for laboratory or bench-scale testing in the final screening process are presented in Table 4-6B. Magnetic separation, gravimetric physical separation (TRU Clean[™]), chemical soil washing, and the solidification/stabilization technologies (polymerization-epoxy, polymerization-polyester, portland cement, and masonry cement) were all previously identified for testing in the Final TSP. Magnetic separation and gravimetric physical separation (TRU Clean[™]) were identified for testing with application to radionuclides. The rest of the technologies are applicable to testing for radionuclides and metals.

The Final TSP selected oxidation technologies such as ozonation, peroxide oxidation, UV oxidation, and UV photolysis for pilot-scale treatability testing of VOC-contaminated water. Bench and pilot-scale tests of UV/oxidation and hydrogen peroxide oxidation technologies are completed or will be completed in the future for OU1. If the information from these tests is sufficient to evaluate these technologies for implementation, inclusion of the oxidation technologies as part of the sitewide treatability program will not be necessary. If the test results are inconclusive or are not applicable, the technologies will be identified for testing in the sitewide treatability program. Other pilot scales are in progress or will be performed as part of IM/IRA at OU2 and are reviewed in Section 3.2

Ozonation, UV photolysis, and slurry phase bioreactor treatment have been identified for pilot-scale testing as part of the Sitewide Program and are presented in Table 4-7. These technologies will continue to be evaluated as described in Figure 4-4 for suitability for pilot-scale testing. Slurry phase bioreactor treatment is applicable to PCB-contaminated soil/sediment. An order of magnitude cost estimate was prepared to provide input into decisions regarding priority and scheduling of future treatability tests. This cost estimate is an engineering judgment based on experience in previous testing for using bioreactors for soil treatment and the EPA guidance document on treatability testing. This cost estimate includes preparation of work plans, assembly of equipment, treatability testing operation, analytical testing, and preparation of a report on results and evaluation.

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TABLE 2-1

ANALYTE CONCENTRATIONS FOR COMBINED OPERABLE UNITS 1-16
AND LIPPER AND LOWER SOUTH INTERCEPTOR DITCHES

	Grou	Groundwater		Surfac	Surface Water			Soils		Sediments		
Parameter	Maximum *	Minimum	Potential ARAR	Meximum*	Minimum,*	Potential ARAR	Maximum⁺	Minimum	Potential**	Meximum*	Minimum	Potential** ARAR
METALS (TOTAL AND DISSOLVED) (mg/L)	VED) (mg/L)			(mg/L)			(mg/kg)			(mg/kg)		
Aluminum	37.7	0 200	0.2	293	0 200	0 200	70600	9		33900	\$	
Antimony	0 628	0 0 0 0		0 643	0900	0900	22	12	8	69 7	12	
Areemo	30	0 0 0 0	900	1 03	0 0 10	0 05	64	20		49.2	7	
Barrum	0 943	0 200	0,	11600	0 200	10	1899	4	4000	706	\$	
Beryllium	0 0 4	0 005	0	0110	0 005	0 005	183	10	0 143	15.5	10	
Boron	0 218	50	20									
Cedmium	0 0352 BR	0 005	0 005	25	0 005	0 002	119	0 +		19.5	10	
Calcium	99 9 BR	5 000		1590	5 000		254000	2000		132000	2000	
Cestum	40	1 000		12	1 000		2410	200		• 001		
Chromum	0 172 BR	0 0 10	900	0 298	0 0 1 0	0 05	781	20	8000(III)	84	20	
Cobalt	0 22	0 0 0 0	900	0 489	0 0 0 0		88 9	Ç		433	5	
Copper	3 13	0 025	0 2	0 908	0 025	0 025	73 6	50		275	20	
Iron	76.6	0 100	03	3220	0 100	0 30	75900	20		33300	50	
Lead	2.8	0 005	0 05	0 950	0 005	0 005	869	10		255	0	
Lithum	1 79	0 100	2 5	85.2	0 100		001	8		958	20	
Magnetium	788	5 000		391	2 000		23300	2000		103000	2000	
Manganese	11 34	0 0 15	900	7 72	0 0 15	0 020	3540	30		1950	30	
Mercury	0 0 1 3	0 0002	0 002	3 9 7	0 0002	0 0002	114	0 2		1.5	0 2	
Molybdenum	1 92 BR	0 200		0 680	0 200		38 65	5		177	\$	
Nickel	117	0 040	0 2	0 82	0 040	40	543	80	2000	89.2	80	
Phosphorus	1 210	0 040		12	0 0 0 40					655	200	

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TABLE 2-1

Peremeter Meximum I	Groundwater		Surfa	Surface Water			Soile		Sedimenta	•	
METALS (TOTAL AND DISSOLVED) (Cont	Meximum Minimum++	Potential • ARAR	Maximum	Мінтит	Potential ARAR	Meximum	Minimum.**	Potential** ARAR	Maximum⁺	Minimum	Potential** ARAR
	inued) (mg/L)		(mg/L)			u)	(mg/kg)		(mg/kg)		
Potassium 7050	5 000		4260	5 000		8020	2000		67000	2000	
Selemum 100 3	0 002	0100	0 55	0 005	900 0	6 51	10		213	10	
Silicon 58 4			44	0100					2470	4 6	
Silver 0 217	17 0 0 0 1 0	0 0 0 0	0 148	0100	0 0 1 0	40 9	20	200	411	20	
Sodium 4447	5 000		9080	5 000		44000	2000		1480	2000	
Strontium 82.4	0 200		119	0 200		1030	5		1230	9	
Thellum 0 544	44 0 050		0 0 0 2 9	0 0 0 0	0 0 0 0	5 74	20		06	20	
Tin 1121	21 0 200		1 53	0 200		382	\$		1080	9	
Vanadium 0.85	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	1 65	0 0 0 0		2590	ţ.		• • •	9	
Zine 50	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20	28 7	0 0 0 0	0110	487	40		735	40	
ANIONS (mg/L)			(mg/L)			(mg/kg)			(mg/kg)		
Arranome			65	0.5	0.5						
Alkalınıty as CaCO ₃ 3151	9		341	0					8230		
Bicarbonate as CaCO ₃ 2640	5		4100	10					3200		
Carbonate as CaCO ₃ 510	5		270	6					130		
Chlonde 1100	50	250	1200	20	230	8			210		
Cyanide 3 8	0 0 1	0.2	90	0 0 1	0 01	19.8			10		
Fluoride 8.2	50	20	7.7	20	20						
Nitrate as N 1450	50	100	1186	50	100	43			35.86		

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These are based on burner health and environmental nek assessment criteria developed for screening purposes or applicable state or federal requirements
Anstyce below detection limit
Anstyce below detection in the detection of the det

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TABLE 2-1

	Gro	Groundwater		Surfac	Surface Water			Soile		Sediments		
Parameter	Maximum*	Minimum	Potential ARAR	Meximum*	Minimum	Potential ARAR	Meximum	Minimum	Potential ** ARAR	Meximum⁺	Minimum.**	Potential** ARAR
ANIONS (Continued) (mg/L)				(mg/L.)			(mg/kg)			(mg/kg)		
Nitrate + Nitrite as N	12100	50	10 0	7800	5.0	10 0	3400	!		163		
Nitrite se N	198	20	20	430	50	20				3.1	0 7	
Orthosphate Phosphate	15	0 0		2.1	9 6							
Sulfate	19000	50	250	1900	20	250	400			744		
Sulfide	13	20	_	120	2.0	20	200	0		23		
Total Kjeldahi Nitrogen				61	-							
Total Organic Carbon				30.9	2		56000					
INDICATORS (mg/L)				(mg/L)			(mg/kg)			(mg/kg)		
Biochemical O ₂ Demand				260	2 0							
Conductivity Min (umho/cm)				737	10							
Conductivity Max (umho/cm)				37120	10							
Dissolved Oxygen (mg/L)												
Minimum				00	90	30						
Maximum				20	0 5							
Of and Greese	32			439	50		267			1100		
Percent Solids (%)												
Minmum							78 9			14.7		
Maximum							96.4			98.95		

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= These sheed on furnal health and environmental nek assessment criteria developed for accessing purposes or applicable state or federal requirements
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= Analyzed below defection limit
= Bedrook (including some westlested bedrook)
= Bedrook (including some westlested bedrook)
= Bedrook (including some westlested bedrook)
= Maximum concentration may be a one turne measurement. Values compiled from both recent and historic date checked against Rocky Flate Environmental Date System
= Value given is detection or quantitation limit for analysis in accordance with Statement of Work for General Redocherwistry and Routine Analytical Services Protocol (G R R A S P) v 1 1, 1990 EG&G Rocky Flate Environmental
= Puttonium 238-238
= Redum 226-228
= Redum 226-228
= Amminia as M
= Sum of polychlorinated biphenyls (PCBs) in water

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TABLE 2-1

	Grou	Groundwater		Surface	Surface Water			Soile		Sediments		
Parameter	Mexemum⁺	Мінншит÷	Potential ARAR	Meximum⁴	Minimum	Potential ARAR	Meximum⁺	Minimum	Potential **	Maxmum⁺	Minimum * *	Potential** ARAR
INDICATORS (mg/L)				(mg/L)			(mg/kg)			(mg/kg)		
pH minimum (pH unite)	5 98	0.1	9 2	3.4	0.1	6 5	5 65			6.1		
pH maximum (pH units)	12	0	8 5	10 2	0.1	8 2	111			96		
Minimum				20								
Maximum				33		_						
Total Dissolved Solids (mg/L) 3	37000	5	400	47000	01	250						
Total Suspended Solids (mg/L) 2	20000	20		46000	2.0							
RADIONUCLIDES (TOTAL AND DISSOLVED) (PCIL.)	SSOLVED) (pCi/L)			(pCI/L)			(pCi/g)			(pCi/g)		
Amencium 241	89 6	0 0		06	0 0 1	30	22	0 02		1 467	0 02	
Cesium 137	7 72	10		12	10		4.7	0 1		32	0	
Gross Alpha	2000	20	10	2107	20	7.0	480	4 0	20	77	4 0	50
Gross Beta	1200	40	50	3800	4 0	50	49.9	5	200	53	5	8
Plutonium 238	0 040	0 0 1	0 05	0 031	0 0 1					0 0 1 6	0 03	
Plutonium 239 + 240	8 13	0 0 1	15(a)	120	0 0	15(a)	180	0 03	60	33	0 03	60
Rednum 226	3 54	0.5		30	0 5	2(p)	9	0 2		1 96	0 5	
Redium 228	13 95	10	(Q)S	52	0 5	2(p)	2.8	0.5		4 41	0 5	
Strontium 89 + 90	7 52	10		4 27	10		1.9	-		2 53	-	
Strontium 90	12.4	10	8	33 34	10	80	4 57	-		66 0	-	
Tritium	12000	400	200	13000	400	500	3.9	400		580	400	

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These set bead on which meth and environmental risk assessment criteria developed for screening purposes or applicable state or federal requirements
Analyzed below detection limit
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Badrock (including stone westlered badrock)
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Maximum cross one time messurement
Values compiled from both recent and liestone data checked against Rocky Flate Environmental Data System
Value given is detection may be a one time messurement
Value given is detection or quantitation limit for analysis in accordance with Statement of Work for General Radiochemistry and Routine Analytical Services Protocol (G R R A S P) v 1 1 1990 EG&G Rocky Flate Environmental
Plutonium 238 + 240
Radium 226 + 228
Arminonia as N
Sum of polychlorinated biphenyle (PCBs) in water

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TABLE 2-1

	Gr	Groundwater		Surface	Surface Water			Sorte		Sediments		
Parameter	Maximum⁺	Minimum	Potential ARAR	Maximum⁺	Minimum	Potential ARAR	Meximum⁺	Minimum	Potential**	Meximum*	Minimum	Potential**
RADIONUCLIDES (TOTAL AND DISSOLVED) (Continued) (pC//L)	DISSOLVED) (Conti	rued) (pC//L)		(pCI/L)			(pCi/g)			(pCl/g)		
Uranium 233 + 234	1000	90		1050	90		3.7	03		411	03	
Uranium 233 + 238 + 239	169	90		1431	90					3 32	0 3	
Uranium 235	47	90		65 5	90		101	03	_	134	03	
Uranium 235 + 236	90	90		47.5	90					0 15		
Uramum 238	750	90		1211	90		39	0 3		3 82	0 3	
Uranum (Total)	63.7	90	O.	1023	9 0	20	40	BR 03		4 8	03	
VOLATILES (ug/L)				(ng/L)		_	(ug/kg)			(ug/kg)		
1 1 Dichloroethane	344	60		90	5.0		49	9				
1 1 Dichloroethene	48000	20	^	143	20	7.0	110	w	12000	50 5	20	
1 1 1 Trichloroethane	30250	20	200	42	20	200	290	50	7000000	30	20	
1 1 2 Trichloroethane	14740	20	20	09	20	20	62	50	120000			
1 1 2 2 Tetrachloroethane	15	20	ų,	440	60	20						
1.2 Dichloroethane	16000	20	9	23			120	60	7700			
1.2 Dichloroethene (Total)	14000	90	8	460	20	8	140	20	_			
1 2 DicHoropropane	9	50	ß	7.0	20	50	30	9				
1 3 DrcMoropropene	3	50		7.0	50	0	60	50	3900			
2 Butenone	280	5		76	0		530	100	_	12000	5	
2 Chloroethytvinylether				50			31	10 0				
2 Hexanone	975	5		87			4.					

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TABLE 2-1

ANALYTE CONCENTRATIONS FOR COMBINED OPERABLE UNITS 1-16
AND UPPER AND LOWER SOUTH INTERCEPTOR DITCHES
(Continued)

		Groundwater	vater			Surface Water	Vater			,	Soils		Š	Sediments		
Parameter	Meximum		Minimum.*	Potential ARAR	Мехатит		Mınımum	Potential ARAR	Мехитит	Ę	Minimum++	Potential **	Meximum		Minamum * *	Potential** ARAR
VOLATILES (Continued) (ug/L)					(ug/L)				(ug/kg)				(ug/kg)			
4-Methyl 2 Pentanone	36		10 0		32		01		120	ר	10		220		10	
Acetone	4100	•	100	4000	970	•	5	4000	2400	•	2	8000000	7300		9	
Benzene	83	_	20	20	83			2	12	7	2	24000	30	_	10	
Bromodichloromethane	10	-	20	0	90			700								
Bromoform	0	_	20	50	30	7	S	200								
Bromomethane	7.0	_	10.0	0	80	_		48	80	7	2	30000				
Carbon Dreulfide	28		50	4000	29			4000	150			8000000	13	_	50	
Cerbon Tetrechlonde	28000		20	20	1005			50	180	•		5400				
Chlorobenzene	73		20		94			8	150		55	2000000	04	_	50	
Chloroethene	17		100		34				ß	7						
Chloroform	5427		20	50	84			20	130	7	20	110000	18		50	
Chloromethene	11		100		38								9		0	
Dibromochloromethene					20		20	09								
Ethylbenzene	16		20	680	18		20	680	780		20	8000000	40		50	
Methylene Chlonde	4100		20	50	340		20	50	590	8		93000	16000		50	
Styrene	6		20	8	9		20	8	17	7		23000	20	_	50	•
Tetrachloroethene	528000		20	50	280		20	20	10000		50	140000	80		50	
Toluene	270	-,	50 1	000	94		20	1000	860			0000000	120		50	
Trichloroethene	221860		20	50	2500		20	20	17000		20	64000	39		50	

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TABLE 2-1

	Gro	Groundwater			Surfac	Surface Water			S	Soils		ipes	Sedimente	
Parameter	Mexamum	Minimum++	Potential ARAR	Maximum	E	Mnimum + +	Potential ARAR	Maximum		Minimum	Potential ** ARAR	Mexamum ⁺	Minimum	Potential**
VOLATRES (Continued) (ug/L)				(ug/L)				(ug/kg)				(ug/kg)		
Vinyl Acetate	39 J	10		30	f	10								
Vinyl Chlonde Xylenes (Total)	930 50 J	10 50 1	10 10000	5 Q		50 tc	10000	3300		5 0 200000000	00000	57 J	10 5 0	
SEMIVOLATILES (TOTAL) (ug/L)				(ng/L)				(ug/kg)				(ug/kg)		
Acenaphthene				20	, ,	10	520	29	7	330		2400	330	
Acenaphthylene												450	330	
Aldrin				90 0		0 05	0 05							
Alpha BHC				0 0 1	7	0 05	0 05					47)	80	
Afpha-chlordene			•	2 6		0.5	0 2							
Ametryn				d 18		90 0		•						
Anthracene				2 0	7	5	•	180	7	330		2900	330	
Atrazine				27200		0 05	30							
Benzo (a) Anthracene				2 0	7	01	01	120	7	330	224	7100	330	
Benzo (b) Fluoranthene				30	7	10	10	350	7	330	•	7100	330	
Benzo (k) Fluoranthene				40	7	5	10	320	٦,	330		8300	330	
Benzo (g h ı) Perylene								9	7	330		5700	330	
Benzo (a) Pyrene				30	7	100	0	230	7		609	6300	330	

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These are based on human health and environmental risk assessment criteria developed for screening purposes or applicable state or federal requirements
Analyzed below detection limit and environmental packs of the selection of the se

TABLE 2-1

ANALYTE CONCENTRATIONS FOR COMBINED OPERABLE UNITS 1-16
AND UPPER AND LOWER SOUTH INTERCEPTOR DITCHES
(Continued)

		Groun	Groundwater			Surfa	Surface Water				Soils		Sediments	onts	
Parameter	Mexamum⁺		Minmum⁺	Potential ARAR	Maximum	wm	Mınımum⁺	Potential ARAR	Mexir	Maxımum⁺	Minimum.*	Potential** ARAR	Maxmum	Minimum *	Potential ** ARAR
SEMI VOLATILES (TOTAL) (Continued) (ug/L)	tinued) (ug/L				(ug/L)				(ug/kg)				(ug/kg)		
Benzo (k) Pyrene									130	7	330				
Benzoic Acid					0 80	7	22		9	, 7	1600		3300	1600	
Benzyl Alcohol				.	43		01	-						!	
Bets-BHC					0		0 05	900					13000	80	
Bis (2 ethylhexyl) Phthalete	8	J BR	01	5	220			10	18000	•	330	83000	14	330	
Butyl Benzyl Phthalate	20	-	01		30	7	0	3000	510	7	330		540	330	
4-Chloro 3 methylphenol					0 1	7		30	740		330	•			
4-Chlorophenyl Phenyl Ether									6	7	330				
Chrysene	420		0		20	7	01	01	550	7	330		8200	330	
Cyanazine					0 3		0								
4 4-00T					90 0	7	0	0					95	16	
Delta-BHC					0 02		0 05						32	80	
Dibenzo (a h) Anthrecene													1200	330	
Dibenzofuran					0	7							1000		
Dreamba					2 1		0 27								
1 4-Dichlorobenzene					4	7	0	75							
Dichloroprop					8		0 65								
Diethyl Phthalate				 ,	9	7		23000	31		330 60	90000000	1200	330	
Di n-Butyl Phthalate	170	J BR	10	10	20	•	10	10	3643	-	330	8000000	3100	330	

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These are based on human health and environmental risk assessment criteria developed for screening purposes or applicable state or federal requirements

Analyzed below detection large detection and detection and the service of the screen service of the service o

Trestability Studies Arnual Report Rocky Flets Plant Golden, Colorado 22861/R1T 2 1 02 12 82/RPT

TABLE 2-1

		Groun	Groundwater			Surface Water	Water			8	Sorls		Š	Sediments	
Parameter	Meximum*		Minimum	Potential ARAR	Meximum		Minimum	Potential ARAR	Махетит	£	Minimum * *	Potential** ARAR	Meximum⁴	Minimum	Potential**
SEMI-VOLATILES (TOTAL) (Continued) (ug/L)	ntinued) (ug/L)				(eg/L)				(ug/kg)				(ug/kg)		
Di n-Octyl Phthalate	56	J BR	01		24	•	10		370	٦	330		2000	330	
2 4-Dimethylphenol				_	09	7	10	2120					•		
2 4-Dinitrotoluene					4 0	7		01				•			
Endosulfan													1600	8	
Ethyl Parathron	0 04				270			0 13						•	
Fluoranthene	5		01		20	7	0	42	1900		330		16000	330	
Fluorene					30	7	01	0	350		330		2000	330	
Gamma-BHC (Lindene)													20	80	
Hexachlorobenzene													440	330	
Indeno (1 2 3 cd) Pyrene									80	7	330		2000	330	
Isophorone					10	7	5	01							
2 Methylnaphthalene				_	21	7	õ	_					350	330	
2 Methylphenol					43		5						2300	330	
4-Methylphenol					8		0						2300	330	
Naphthalene					25		01	0					1100	330	s
2 Nitrophenol	30	~	5									_			
4-Nitrophenol	20	7	8						160	7	1600				
4-Nitroanline													5300 J	1600	
N Mtroso-di n-Propylemme				•	ND.	7	5	5							

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 These sets based on human health and environmental risk assessment criteria developed for accessing purposes or applicable state or federal requirements
 Anytzad below detection limit health and environmental based on human health and detection limit for an adversary of a set of the control of the c

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TABLE 2-1

ANALYTE CONCENTRATIONS FOR COMBINED OPERABLE UNITS 1-16 AND UPPER AND LOWER SOUTH INTERCEPTOR DITCHES (Concluded)

	B	Groundwater		Sur	Surface Water			Soils		Pes	Sediments	
Parameter	Maximum	M-mmum ⁺	Potential ARAR	Maximum	Митит	Potential ARAR	Maxamum		Potential**	•• Maximum •	Minimum	Potential**
SEMI VOLATRES (TOTAL) (Continued) (ug/L)	ntirued) (ug/L)			(ug/L)			(ug/kg)			(ug/kg)		
		ءِ	۽	300	t 0	10	880	J 330	0	2000	330	
N WILLOSCONDINGTHING	75.	2	2	20	ß	20	110	J 1600	0 200000	350	1600	
rentechnological	·	3	}		0	9	500	330	0	16000	330	
Phenol	10	0	9	39	0	10	320	J 33	0000000000000	999	330	
Prometon	· ·			0 0	0 03							
Prometon				0 18	90 0							
December				2.4	0 03							
Presse				4	01	10	880	330	0	19000	330	
Simazina				330	90 0	40						
Simetryn				0 64	0 0							
Terbuthviazine				4-								
1.2 4. Trichlorobenzene				4	10	700				40	330	
DOLVCH CRIMATED RIPHENYI S (PCBs) (unf.)	S (PCBa) (un/L)											
4254				12	10 10	10	440000		00	0 00 1 600000	160	
Arocior 1254												

NOTE Analytical data received prior to October 1988 not subjected to validation procedure. Some of the chemical values reported in this table have not yet been validated and the analyte list may be changed after the data are validated

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TABLE 2-2 COMPARISON OF ARARS CHANGES BETWEEN FINAL TSP AND ANNUAL REPORT

Parameter	Media	Final TSP	Annual Report
Metals (Total and Dissolved) (mg/L)		
Aluminum	Groundwater	5 0	0 2
Antimony	Groundwater	0 01	0
Antimony	Surface Water	0 146	0 060
Antimony	Soil	3000 ug/kg	30 mg/kg
Boron	Groundwater		5 0
Cadmium	Groundwater	0 01	0 005
Cadmium	Surface Water	0 01	0 005
Chromium	Soil	400(VI)	8000(III)
Copper	Groundwater	1 0	0 2
Copper	Surface Water	1 0	025
Lead	Surface Water	0 05	0 005
Lithium	Groundwater		25
Mercury	Surface Water	002	0002
Nickel	Surface Water	0 1	0 4
Selenium	Surface Water	01	005
Silver	Surface Water	05	01
Thallium	Surface Water		05
Zinc	Groundwater	5 0	20
Zinc	Surface Water	50	110
Anions (mg/L)			
Chloride	Surface Water	250	230
Cyanide	Groundwater	10	0 2
Cyanide	Surface Water	10	01
Fluoride	Surface Water		5
Nitrite as N	Groundwater		5
Indicators (mg/L)			
Dissolved Oxygen (min)	Groundwater		3

TABLE 2-2
COMPARISON OF ARARS CHANGES BETWEEN
FINAL TSP AND ANNUAL REPORT
(continued)

Parameter	Media	Final TSP	Annual Report
Total Dissolved Solids	Groundwater	500	400
Total Dissolved Solids	Groundwater	500	250
Radionuclides (Total and Dissolved) (pCi/L)			
Gross Alpha	Groundwater	15	7
Gross Alpha	Surface Water	15	7
Gross Beta	Groundwater	50	5
Radium 226	Groundwater		5
Radium 228	Groundwater		5
Tritium	Groundwater	20,000	500
Uranıum (Total)	Groundwater		5
Volatiles (ug/L)			
1,1,2-Trichloroethane	Groundwater	28	5
1,1,2-Trichloroethane	Surface Water		5
1,1,2,2-Tetrachloroethane	Groundwater	••	5
1,1,2,2-Tetrachloroethane	Surface Water		5
1,2-Dichloroethene (Total)	Groundwater	70	100
1,2-Dichloroethene (Total)	Surface Water	70	100
1,2, Dichloropropane	Surface Water		5
1,3-Dichloropropene	Surface Water		10
Benzene	Soil		24,000
Bromodichloromethane	Groundwater		5 0
Bromodichloromethane	Surface Water	•••	700
Bromoform	Groundwater		5 0
Bromoform	Surface Water		700
Bromomethane	Groundwater		10
Bromomethane	Surface Water		48

Sheet 2 of 5

TABLE 2-2
COMPARISON OF ARARS CHANGES BETWEEN
FINAL TSP AND ANNUAL REPORT
(continued)

Parameter	Media	Final TSP	Annual Report
Bromomethane	Soil		30,000
Carbon disulfide	Groundwater		4000
Carbon disulfide	Surface Water		4000
Carbon disulfide	Soil		8,000,000
Chloroform	Groundwater	100	5
Chloroform	Surface Water	100	5
Dibromochloromethane	Surface Water		6
Ethylbenzene	Surface Water	1400	680
Styrene	Groundwater		100
Styrene	Surface Water		100
Styrene	Soil		23,000
Tetrachloroethene	Groundwater	10	5
Toluene	Groundwater	2420	1000
Toluene	Surface Water	14,300	1000
Xylenes (Total)	Groundwater	7,000	10,000
Xylenes (Total)	Surface Water	7,000	10,000
Semivolatiles (Total) (ug/L)			
Acenaphthene	Surface Water		520
Aldrın	Surface Water		05
Alpha-BHC	Surface Water		05
Alpha-chlordane	Surface Water	**	5
Anthracene	Surface Water		10
Atrazıne	Surface Water		30
Benzo(a)Anthracene	Surface Water		10
Benzo(b)Fluoranthene	Surface Water		10
Benzo(k)Fluoranthene	Surface Water		10
Benzo(a)Pyrene	Surface Water		10

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TABLE 2-2
COMPARISON OF ARARS CHANGES BETWEEN
FINAL TSP AND ANNUAL REPORT
(continued)

Bis(2-ethylhexyl)Phthlate	Parameter	Media	Final TSP	Annual Report
Butyl Benzyl Phthalate Surface Water - 3,000 4-Chloro-3-methylphenol Surface Water - 30 Chrysene Surface Water - 10 4,4-DDT Surface Water - 1 1,4-Dichlorobenzene Surface Water - 75 Diethyl Phathalate Surface Water - 23,000 Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dimethyphenol Surface Water - 2120 2,4-Dimethyphenol Surface Water - 0 13 Fluorenthene Surface Water - 0 13 Fluorenthene Surface Water - 42 Fluorene Surface Water - 10 N-Nitroso-di-n-Propylamine Surface Water - 10 N-Nitrosodiphenylamine Groundwater - 10 N-Nitrosodiphenylamine	Beta-BHC	Surface Water		05
4-Chloro-3-methylphenol Surface Water 30 Chrysene Surface Water 10 4,4-DDT Surface Water 1 1,4-Dichlorobenzene Surface Water 75 Diethyl Phathalate Surface Water 23,000 Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 Di-n-Butyl Phatalate Surface Water 2120 2,4-Dimethyphenol Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluorente Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol	Bis(2-ethylhexyl)Phthlate	Surface Water	15,000	10
Chrysene Surface Water 10 4,4-DDT Surface Water 1 1,4-Dichlorobenzene Surface Water 75 Diethyl Phathalate Surface Water 23,000 Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dinity Departing Surface Water 2120 2,4-Dinitrotoluene Surface Water 0 13 Fluoranthene Surface Water 0 13 Fluoranthene Surface Water 10 Isophorone Surface Water 10 Naphhalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol <t< td=""><td>Butyl Benzyl Phthalate</td><td>Surface Water</td><td></td><td>3,000</td></t<>	Butyl Benzyl Phthalate	Surface Water		3,000
4,4-DDT Surface Water 1 1,4-Dichlorobenzene Surface Water 75 Diethyl Phathalate Surface Water 23,000 Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dimethyphenol Surface Water 2120 2,4-Dinitrotoluene Surface Water 0 13 Fluoranthene Surface Water 0 13 Fluorenthene Surface Water 10 Isophorone Surface Water 10 Nophalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Phenol Grou	4-Chloro-3-methylphenol	Surface Water		30
1,4-Dichlorobenzene	Chrysene	Surface Water		10
Diethyl Phathalate Surface Water 23,000 Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dimethyphenol Surface Water 2120 2,4-Dinitrotoluene Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Groundwater 50 Phenol Grou	4,4-DDT	Surface Water		1
Di-n-Butyl Phatalate Groundwater 4 10 Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dimethyphenol Surface Water 2120 2,4-Dinitrotoluene Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Surface Water 10 Phenol Surface Water	1,4-Dichlorobenzene	Surface Water	**	75
Di-n-Butyl Phatalate Surface Water 4 10 2,4-Dimethyphenol Surface Water 2120 2,4-Dinitrotoluene Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Diethyl Phathalate	Surface Water		23,000
2,4-Dimethyphenol Surface Water 2120 2,4-Dinitrotoluene Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Groundwater 10 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Dı-n-Butyl Phatalate	Groundwater	4	10
2,4-Dintrotoluene Surface Water 10 Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Surface Water 3500 10 Phenol Surface Water 3500 10	Dı-n-Butyl Phatalate	Surface Water	4	10
Ethyl Parathion Surface Water 0 13 Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Surface Water 3500 10 Phenol Surface Water 3500 10	2,4-Dimethyphenol	Surface Water		2120
Fluoranthene Surface Water 42 Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 50 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Groundwater 10 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	2,4-Dinitrotoluene	Surface Water		10
Fluorene Surface Water 10 Isophorone Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Ethyl Parathion	Surface Water		0 13
Surface Water 10 Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Fluoranthene	Surface Water		42
Napthalene Surface Water 10 N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Surface Water 3500 3,000,000	Fluorene	Surface Water		10
N-Nitroso-di-n-Propylamine Surface Water 10 N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Surface Water 3500	Isophorone	Surface Water		10
N-Nitrosodiphenylamine Groundwater 10 N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Napthalene	Surface Water		10
N-Nitrosodiphenylamine Surface Water 10 Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	N-Nitroso-di-n-Propylamine	Surface Water		10
Pentachlorophenol Groundwater 50 Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	N-Nitrosodiphenylamine	Groundwater		10
Pentachlorophenol Surface Water 50 Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	N-Nitrosodiphenylamine	Surface Water		10
Pentachlorophenol Soil 200,000 Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Pentachlorophenol	Groundwater	*-	50
Phenol Groundwater 10 Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Pentachlorophenol	Surface Water		50
Phenol Surface Water 3500 10 Phenol Soil 3,000,000	Pentachlorophenol	Soil		200,000
Phenol Soil 3,000,000	Phenol	Groundwater	•••	10
	Phenol	Surface Water	3500	10
Pyrene Surface Water 10	Phenol	Soil		3,000,000
	Pyrene	Surface Water		10

TABLE 2-2 COMPARISON OF ARARS CHANGES BETWEEN FINAL TSP AND ANNUAL REPORT (continued)

Parameter	Media	Final TSP	Annual Report
Simazine	Surface Water		4
1,2,4-Trichlorobenzene	Surface Water		700
Aroclor-1254	Surface Water		10
Aroclor-1254	Soil		09

TABLE 2-3

LIST OF CHEMICALS REPORTED ABOVE ARARS IN TWO OR MORE OPERABLE UNITS

		Operable Unit	s (Two or More)	
Contaminant	Reported in Groundwater	Reported in Surface Water	Reported in Soils	Reported in Sediments
METALS			-	
Aluminum	1, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16, USID		
Antimony		2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID		
Arsenic	4, 6, 7, 10, 14, 16	5, 6, BACK		
Barium		2, 4, 5, 6, 7, 8, 10, 14, 16, USID, LSID		
Beryllium		2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID	1, 2, 4, 5, 6, 8, 9, 10, 12, 13, 14, 15, 16	
Cadmium	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 14, 16	2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID		
Chromium	2, 4, 5, 6, 8, 10, 11, 13, 14, 16	2, 4, 5, 6, 7, 8, 10, 13, 14, 16 USID, LSID		
Cobalt	1, 2, 4, 6, 7, 8, 10, 14, 16			
Copper	1, 2, 4, 5, 6, 7, 8, 10, 14, 16	2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16		
Iron	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16 LSID, USID		

TABLE 2-3

LIST OF CHEMICALS REPORTED ABOVE
ARARS IN TWO OR MORE OPERABLE UNITS
(Continued)

Lead 2, 4, 5, 6, 8, 1, 2, 4, 5, 6, 7, 9, 10, 11, 14, 8, 9, 10, 11, 16 13, 14, 15, 16, LSID, USID	ported in Reported in Soils Sediments
9, 10, 11, 14, 8, 9, 10, 11, 16 16 13, 14, 15, 16, LSID, USID	
Management 4 0 4 5 0 7 0 7	
Manganese 1, 2, 4, 5, 6, 1, 2, 4, 5, 6, 7, 7, 8, 9, 10, 8, 9, 10, 11, 11, 12, 13, 13, 14, 15, 16, 14, 15, 16 LSID, USID	
Mercury 1, 2, 4, 5, 8, 1, 2, 4, 5, 6, 7, 10, 11, 14, 16 8, 9, 10, 11, 13, 14, 16,	
Nickel 1, 2, 4, 5, 6, 2, 4, 5, 6, 8, 7, 8, 9, 10, 10, 13, 14, 16, 14, 16 BACK	
Selenium 1, 2, 4, 5, 6, 1, 2, 4, 5, 6, 7, 7, 8, 9, 10, 8, 9, 10, 13, 14, 16 14, 16, LSID	
Silver 2, 6, 7, 16 1, 2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16	
Thallium 6, 16	
Vanadium 2, 6, 7, 8, 9, 10, 13, 16	
Zinc 1, 2, 5, 6, 8, 1, 2, 4, 5, 6, 7, 10, 14, 16 8, 9, 10, 13, 14, 15, 16	
INORGANICS	
Chloride 1, 4, 7 4, 7	
Cyanide 2, 4, 6, 8, 9, 2, 5, 6, 7, 8, 9, 10, 14, 16 10, 13, 14, 16	

TABLE 2-3

LIST OF CHEMICALS REPORTED ABOVE ARARS IN TWO OR MORE OPERABLE UNITS (Continued)

		Operable Unit	s (Two or More)	
Contaminant	Reported in Groundwater	Reported in Surface Water	Reported in Soils	Reported in Sediments
Nitrate and Nitrate + Nitrite	4, 6, 8, 10, 14, 16	1, 2, 4, 8		
Sulfate	1, 2, 4	4, 5, 7		
pH below minimum		1, 2, 4, 5, 6, 7, LSID, USID		
pH above maximum	2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13,14, 15, 16	6, 7, 9, LSID, USID		
Total Dissolved Solids	1, 2, 4, 7	1, 4, 5, 6, 7, 11, LSID		
RADIONUCLIDES				
Americium 241		2, 4, 8, 10, 14, 16		
Gross Alpha	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID, USID	1, 2, 4, 5, 6, 8, 9, 10, 11, 13, 14, 15, 16	1, 5, 6, 8, 9, 10, 13, 14, 15, 16
Gross Beta	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16, LSID, USID		
Plutonium 239 + 240		2, 4, 8, 10, 14, 16	1, 2, 4, 6, 8, 10, 13, 14, 16	5, 6, 8, 9, 10, 14, 16
Radium 226	4, 6, 8, 10, 14, 16	2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID, BACK		
Radium 228	4, 8, 10, 16	2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16		

TABLE 2-3

LIST OF CHEMICALS REPORTED ABOVE ARARS IN TWO OR MORE OPERABLE UNITS (Continued)

		Operable Units	(Two or More)	
Contaminant	Reported in Groundwater	Reported in Surface Water	Reported in Soils	Reported in Sediments
Strontium 90	2, 5, 6, 7, 8, 10, 16			
Tritium	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 16		
Uranıum (Total)	1, 2, 4, 6, 7, 8, 9, 11, 13, 14, 15, 16	1, 2, 4, 5, 6, 8, 9, 10, 13, 14, 16, USID		
VOLATILE ORGANICS				
1,1-Dichloroethene	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16	2, 6, 8, 9, 10, 13, 14, 16		
1,1,1-Trichloroethane	1, 2, 4, 8, 10, 14, 15, 16			
1,1,2-Trichloroethane	1, 2, 5, 10, 12, 14, 15, 16	6		
1,1,2,2-Tetrachloroethane		4, 6, 8, 10, 14, 16		
1,2 - Dichloroethane	1, 2, 4, 6, 8, 10, 13, 14, 16			
1,2 - Dichloroethene (total)	1, 2, 4, 5, 6, 8, 9, 10, 13, 14, 15, 16	2, 8, 9, 10, 13, 14, 16		
1,2-Dichloropropane	7, 16			
Benzene	1, 4, 7, 8, 10, 11, 14, 16			
Carbon Tetrachloride	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 14, 15, 16	2, 5, 6, 8, 9, 10, 13, 14, 16		

TABLE 2-3

LIST OF CHEMICALS REPORTED ABOVE
ARARS IN TWO OR MORE OPERABLE UNITS
(Concluded)

		Operable Units	(Two or More)	
Contaminant	Reported in Groundwater	Reported in Surface Water	Reported in Soils	Reported in Sediments
Chloroform	1, 2, 4, 5, 6, 7, 8, 9, 10, 13, 14, 15 16	2, 5, 6, 8, 9, 10, 13, 14, 16		
Methylene Chloride	1, 2, 4, 5, 6, 7, 9, 10, 11, 12, 15, 16	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16, LSID		
Tetrachloroethene	1, 2, 4, 5, 6, 7, 8, 9, 10, 12, 13, 14, 15, 16	1, 2, 5, 6, 7, 8, 9, 10, 13, 14, 16		
Trichloroethene	1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16	1, 2, 5, 6, 7, 8, 9, 10, 13, 14, 16, LSID		
Vinyl Chloride	6, 7, 9, 10, 13, 14, 15, 16	6, 8, 9, 10, 13, 14, 16		
SEMIVOLATILE ORGANICS				
Alpha-Chlordane		1, 9		
Bis(2-ethylhexyl)phthalate	5, 6, 9, 13	5, 6, 8, 10, 16		
Dı-N-Butyl Phthalate		5, 6		
Naphthalene		6, 7, 16		
N-Nitrosodiphenylamine	1, 2, 5, 6, 7, 8, 10, 11, 16	5, 6, 13		
Phenol		5, 6, 7		
POLYCHLORINATED BIPHENYLS (PCBs)				
Aroclor-1254		6, 8, 10, 16	8, 10, 12, 13	

TABLE 4-1A

TECHNOLOGIES IDENTIFIED FOR PRELIMINARY SCREENING **GROUNDWATER AND SURFACE WATER**

GROONDWATER A	ND SURFACE WATER		
VOLATILE ORGANICS			
Physical Processes	Chemical Processes		
Aqua Detox (Low Vacuum Steam Stripping) In Situ Air Stripping	Catalytic Oxidation Solar Photocatalytic (1)		
Biological Processes	Thermal Processes		
Aerobic Biological Reactors Aerobic Reductive Dechlorination Cometabolism Biological Process	No Additional Technologies or New Information		
SEMIVOLAT	ILE ORGANICS		
Physical Processes	Chemical Processes		
Aqua Detox (Low Vacuum Steam Stripping) Carbon Dioxide Extraction Biological Processes	Catalytic Oxidation Solar Photocatalytic (1) Thermal Processes		
Anaerobic Biological Activated Carbon Process	Supercritical Water Oxidation (1)		

Anaerobic Reductive Dechlorination Cometabolism Biological Process

Contact Stabilization **Extended Aeration** In Situ Bioremediation (1) Pure Oxygen Activated Sludge

PCBs		
Physical Processes	Chemical Processes	
Activated Carbon	Catalytic Oxidation	
Freeze Crystallization	Ozonation	
Solvent Extraction	Peroxide Oxidation	
	Solar Photocatalytic	
	Ultraviolet Oxidation	
	Ultraviolet Photolysis	
Biological Processes	Thermal Processes	
Anaerobic Biological Activated Carbon Process	Solar	
Powdered Activated Carbon	Supercritical Water Oxidation	

⁽¹⁾ Denotes technology has been reevaluated based on additional information and review

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TABLE 4-1A

TECHNOLOGIES IDENTIFIED FOR PRELIMINARY SCREENING GROUNDWATER AND SURFACE WATER (Concluded)

INO	RGANICS
Physical Processes	Chemical Processes
No Additional Technologies or New Information	Catalytic Oxidation
Biological Processes	Thermal Processes
Biodenitrification	No Additional Technologies or New Information
N	IETALS
Physical Processes	Chemical Processes
Alternating Current Electro-Coagulation Hardwicka Binata Bark Adsorption Ultrafiltration	No Additional Technologies or New Information
Biological Processes	Thermal Processes
Activated Sludge Biosorption (Bioaccumulation) (1)	No Additional Technologies or New Information
RADIO	DNUCLIDES
Physical Processes	Chemical Processes
Alternating Current Electrocoagulation Emulsion Liquid Membrane Extraction Hollow-Fiber Supported Liquid Membrane	Potassium Ferrate Precipitation (TRU-Clear™)(1)
Biological Processes	Thermal Processes
Biosorption (Bioaccumulation) (1) Enzymatic Microbial Reduction	No Additional Technologies or New Information

(1) Denotes technology has been reevaluated based on additional information and review

TABLE 4-1B

TECHNOLOGIES IDENTIFIED FOR PRELIMINARY SCREENING SOIL AND SEDIMENTS

PC	CBS
Biological Processes	Physical/Chemical Processes
Aerobic Biodegradation Anaerobic Biological Activated Carbon Process Anaerobic Dechlorination Slurry Phase Bioreactor	BEST Process CF Systems Organic Extraction Fenton's Reagent Decomposition Glycolate Dechlorination Surfactant Washing
Thermal Processes	Solidification/Stabilization Processes
Fluidized Bed Incineration Infrared Thermal Treatment Rotary Kiln Incineration Solar Wet Air Oxidation	Chemical Stabilization In Situ Vitrification Vitrification
ME	TALS
Biological Processes	Physical/Chemical Processes
No Additional Technologies or New Information	No Additional Technologies or New Information
Thermal Processes	Solidification/Stabilization Processes
No Additional Technologies or New Information	In Situ Vitrification (1)
RADION	UCLIDES
Biological Processes	Physical/Chemical Processes
No Additional Technologies or New Information	No Additional Technologies or New Information
Thermal Processes	Solidification/Stabilization Processes
No Additional Technologies or New Information	In Situ Vitrification (1) Polymerization - Polyethylene (1)

(1) Denotes technology has been reevaluated based on additional information and review

TABLE 4-2A

PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER

Volatile Organics	Physical
Contaminant Group	Technology Group

Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Applicable to volatile and semivolatile contaminants in groundwater	95+% achievable	, Yes	Commercially available	Complex operations Requires steam	Equipment available	Produces reduced volume solvent stream which requires disposal	Yes
Applicable to most volatile contaminants in groundwater Most effective in high permeability soils	95+% achievable	Yes	Innovative	High for emission control system	Requires installation of horizontal air injection/extraction wells below/above aquifer Will likely require treatment of air emissions	Potential for uncontrolled release of volatile contaminants	Yes

TABLE 4-2A

PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER

Contaminant Group Volatite Organics
Technology Group Chemical

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Solar Photocatalytic	PotenNally applicable to most VOC compounds	Up to 95%	Unknown	Innovative	Unknown	Equípment not currently commercially available	No major impacts identified	S
Catalytic Oxidation	Potentially applicable to most VOC compounds	Unknown	Unknown	Experimental	Unknown	Research into selection of appropriate catalysts in progress Equipment not currently available	No major impacts identified	, og

¹ See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

TABLE 4-2A PRELIMINARY TECHNOLOGY SCREENING GRQUINDWATER AND SURFACE WATER

Contaminant Group Volatile Organics
Technology Group Biological

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Aerobic Biological Reactors	Applicable to volatile petroleum hydrocarbons (BTEX) Not applicable to chlorinated solvents	95+% achievable	Yes	Innovative for application to surface water and groundwater remediation	Close operator- attention and good process control required	Various types of reactor systems available	Potential for VOC emissions to air Produces biomass sludge which must be disposed	Yes
Aerobic Reductive Dechlorination	Applicable to chlorinated solvents in water	Unknown	Unknown	 Innovative 	Unknown	Equipment not commercially available	Unknown	, o
Cometabolism Biological Process	Applicable to chlorinated solvents in water	50 to 60%	8	Emerging	Unknown	Equipment not commercially available	Unknown	, o

1 See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER TABLE 4-2A

Contaminant Group Technology Group

Volatile Organics Thermal

Applicability Technology

Potential to Meet Cleanup Goal Removal Efficiency

Technology Maturity

O & M Requirements

Implementability

Adverse Impacts

Retain Yes/No

No additional technologies or new information on previously identified technologies in Final TSP

Contaminant Group Semivolatile Organics
Technology Group Physical

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Aqua Detox (Low Vacuum Steam Stripping)	Applicable to volatile and semivolatile compounds in water	95+% achievable	, ∀es	Commercially available	Complex operation Requires steam	Equipment available	Produces a reduced volume solvent stream which requires disposal	Yes
Carbon Dioxide Extraction	Applicable to most semivolatile compounds in water	Unknown	Unknown	Innovative	Unknown	Unknown	Unknown	- 8 2

¹ See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Semivolatife Organic	Chemical
Contaminant Group	Technology Group

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Catalytic Oxidation	Potentially applicable to most semivolatile compounds in water	Unknown	Unknown	Experimental	Unknown	Research into selection of appropriate catalysts in progress Equipment not commercially available	No major Impacts identified	- 0 2
Solar Photocatalytic	Potentially applicable to most semivolatile compounds in water	Up to 95%	Unknown	Innovative	Unknown	Equipment not commercially available	No major impacts identified	ço X

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Semivolatile Organics	Biological
Contaminant Group	Technology Group

Technology	Applicability	Removal Efficiency	val Potential to Meet ncy Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Anaerobic Biological Activated Carbon Process	Wide range of organics	Highly vanable potentially 90%	Requires polishing step	Experimental	Unknown	Equipment not commercially available	Unknown	9
Anaerobio Reductive Dechlorination	Applicable to chlorinated semi-volatile organics in water	Unknown	Unknown	Innovative	Unknown	Equipment not commercially available	Unknown	- 92
Cometabolism Biological Process	Applicable to chlorinated organics, phenof, cresol	50 to 60%	9	Emerging	Unknown	Equipment not commercially available	Unknown	ç Š
Contact Stabilization	Wide range of organics	85 to 90%	Requires polishing step	Available	Moderate	Equipment readily available	Produces studge which will require disposal	Yes
Extended Aeration	Wide range of organics	80 to 90%	Requires polishing step	Available	Moderate	Equipment readily available	Produces studge which will require disposal	Yes

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Semivolatile Organics	Biological
Contaminant Group	Technology Group

Technology	Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
in Situ Bioremediation	Wide range of organics	High for high initial concentration s Not effective at low concentration s	Pow.	Innovative	Moderate	Requires careful design of extraction and injection wells	No significant impacts	~ Ž
Pure Oxygen Activated Sludge	Wide range of organics	90 to 95%	Requires polishing step	Available	High	Equipment readily available	Produces sludge which will require disposal	Yes

Semivolatile Organics Thermal	Contaminant Group
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Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Supercritical Water Oxidation	Most semivolatile organics in water	99+% achievable	Υes	Commercially available Innovative in remediating of groundwater and surface water	High energy requirement High pressure operation Potential problems with this technology due to process operating conditions, complexity, and lack of long-term full-scale operating experience	Not Readily implementable, Requires very specialized equipment	No major impacts identified	S >-

Contaminant Group PCBs
Technology Group Physical

Technology	Applicability	Removal Efficiency	wal Potential to Meet Technology ncy Cleanup Goal Maturity	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Activated Carbon	Applicable to PCBs in water at low to moderate concentrations	High	High	Commercially available	High requirement for replacement of carbon	Equipment commercially available	Disposal of PCB contaminated carbon may be a problem	Yes
Freeze Crystallization	Applicable to dilute concentrations of PCB in water	Hgh	Hgh	Commercially available	Moderate Requires high power use for refrigeration	Equipment commercially available	Produces concentrated waste stream which must be treated or disposed	Yes
Solvent Extraction	Applicable to high concentrations of PCBs in water	High at high initial concentrations Choice of solvents critical	Low to Moderate	Commercially available	Moderate	Equipment commercially available	Produces concentrated waste stream which must be treated or disposed	- 0 2

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Contaminant Group PCBs Technology Group Chemical

Technology	Removal Potential to Meet Technology O & M Technology Applicability Efficiency Cleanup Goal Maturity Requirements Im	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	plementa	Adverse Retain ibility impacts Yes/No	Retain Yes/No
Catalytic Oxidation	Potentially applicable to PCBs in water	Unknown	Unknown	Expenmental	Unknown	Research into selection of appropriate catalysts in progress, Equipment not commercially available	No major Impacts identified	- 0 X
Ozonation	Applicable to PCBs in water Not a specific freatment	Medium to high Very compound specific	Yes	Commercially available	Low High chemical demand	Equipment available	No significant impacts	X _{es}
Peroxide Oxidation	Applicable to PCBs in water Not a specific treatment	Medium to high Very compound specific	, ∀es	Commercially available	Low High chemical demand	Equipment available	No significant impacts	Yes
Solar Photocatalytic	Potentially applicable to PCBs in water	Unknown	Unknown	Innovative	Unknown	Equipment not commercially available	Unknown	o Ž
Ultraviolet Oxidation	Applicable to PCBs in water. Not a specific treatment	Medium to high Very compound specific	Yes	Yes	Commercially available	Low Requires periodic maintenance of UV lamps High power requirement	No major impacts	Yes

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

PCBs	Chemical
Contaminant Group	Technology Group

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Ultraviolet Photolysis	Applicable to PCBs in water Not a specific treatment	Medium to high Very compound specific	Yes	Yes	Commercially available	Low Requires periodic maintenance of UV lamps High power requirement	No major impacts	Yes

Contaminant Group PCBs
Technology Group Biological

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Anaerobic Biological activated Carbon Process	Potentially applicable	Unknown	Unknown	Not demonstrated	Unknown	Equipment not commercially available	Unknown	, oN
Powdered Activated Carbon	Applicable to wide range of concentrations of PCBs in water	High	χ ₀ χ	Commercially available	Moderate	Equipment is commercially available	Produces PCB contaminated waste sludge requiring treatment/ disposal	Yes

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

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TABLE 4-2A PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER

Contaminant Group PCBs
Technology Group Thermal

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O&M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Solar	Applicable to PCBs and other chlorinated hydrocarbons	Unknown	Unknown	Under development	Unknown	Unknown	No major Impacts identified	, O
Supercritical Water Oxidation	Applicable to PCBs in water	99+% to PCBs achievable	, ≺es	Commercially available innovative in remediation of surface water and groundwater	High energy requirement High pressure operation	Equipment commercially available	No major impacts identified	Yes

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Contaminant Group Technology Group

Inorganics Physical

Detain	Yes/No	
Adverse	Impacts	-
	Implementability	
_	Requirements	
Technology	Maturity	
Potential to Meet	Cleanup Goal	
Bemoval	Efficiency	
	Applicability	
	Technology	(6

No additional technologies or new information on previous technologies identified

Contaminant Group Inorganics
Technology Group Chemical

Retaın Yes/No Adverse Impacts Implementability Requirements 0 & M Technology Maturity Potential to Meet Cleanup Goal Removal Efficiency Applicability Technology

Unknown Innovative

Unknown

Applicable to cyanide in water

Catalytic Oxidation

Unknown Not commercially available

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Unknown

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Inorganics	Biological
Contaminant Group	Technology Group

Technology	Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Biodenitrification	Applicable to nitrates in water	99+% achievable	Yes	Demonstrated	Requires addition of organic substrate Good process control required	Readily available	No major impacts identified	Yes

PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER **TABLE 4-2A**

Contaminant Group Technology Group

Inorganics

Adverse Impacts Implementability O & M Requirements Technology Maturity Potential to Meet Cleanup Goal Removal Efficiency Applicability Technology

Retain Yes/No

Contaminant Group Metals
Technology Group Physical

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O&M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Alternating Current Electro- coagulation	Applicable to most metals in water. Must be combined with solids removal	Unknown	Unknown	Innovative	Requires good process control	Equipment not commercially available	No major Impacts identified	- oZ
Hardwickia Bınata Bark Adsorptıon	Applicable to mercury (II) in water	Unknown	Unknown	Experimental	Unknown	Equipment not commercially available	No major impacts identified	
Ultrafiltration	Applicable to insoluble metal species in water or metals complexed with high molecular weight molecules	High Dependent on ability to precipitate or complex metals	Unknown	Commercially available	Frequent maintenance of filtration membranes	Readily implementable	No major impacts identified	Yes

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

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PRELIMINARY TECHNOLOGY SCREENING GROUNDWATER AND SURFACE WATER TABLE 4-2A

Contaminant Group Technology Group

Metals

Applicability Technology

Removal Efficiency

Potential to Meet Cleanup Goal

Technology Maturity

O & M Requirements

Implementability

Adverse Impacts

Retain Yes/No

Contaminant Group Metals
Technology Group Biological

Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Model hji	Moderate to high	Moderate	Activated sludge treatment commercially available	Moderate	Requires operation of activated sludge water treatment system	Solid sludge from process will contain metals removed, May be hazardous waste	- 2
Unknown	Ę	Low	Experimental	Unknown	Utilizes conventional equipment	Solid sludge from process will contain metals removed May be hazardous waste	, Q

See Table 4 4A for rejection rationale Technologies that have not been retained are shaded

Contaminant Group Technology Group

Metals Thermal

Technology Maturity Potential to Meet Cleanup Goal Removal Efficiency Applicability

Technology

Retain Yes/No

Adverse Impacts

Implementability

Requirements

⊗ ⊗ M

Contaminant Group Radionuciides
Technology Group Physical

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Alternating Current Electrocoagulation	Applicable to removal of uranium and transuranium elements from water Must be combined with solids removal treatment	Ę	Yes	Innovative	Requires good process control	Equipment available	No major impacts identified	Yes
Emulsion Liquid Membrane Extraction	Applicable to uranium contaminated water	Unknown	Unknown	Experimental	Unknown	Not commercially available	No major impacts identified	ţo Z
Hollow-Fiber Supported Liquid Membrane	Applicable to uranium-contaminated water	Unknown	Unknown	Experimental	Unknown	Not commercially available	No major impacts identified	No.

See Table 4-4A for rejection rationale. Technologies that have not been retained are shaded

Contaminant Group Radionucildes
Technology Group Chemical

Technology	Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Potassium Ferrate Precipitation (TRU Clear TM)	Applicable to removal of uranium and transuranium elements from water Must be combined with solids removal treatment	Į Po	se>	Innovative	Requires good process control	Equipment available	No major impacts identified	Yes

Contaminant Group Radionuclides
Technology Group

Technology	Applicability	Removal	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Biosorption (Bioaccumulation)	Potentially applicable to metallic radionuclides	Unknown	Unknown	Expenmental	Unknown	Not commercially available	Produces a solid waste containing radionuclides	, S
Enzymatic Microbial Reduction	Applicable to uranium dissolved in water	Unknown	Unknown	Experimental	Unknown	Not commercially available	No major impacts identified	, o

See Table 4-4A for rejection rationale Technologies that have not been retained are shaded

Radionuciides Thermal Contaminant Group Technology Group Applicability Technology

Technology Maturity Potential to Meet Cleanup Goal Removal Efficiency

Retain Yes/No

Adverse Impacts

Implementability

O & M Requirements

TABLE 4-2B

Contaminant Group PCBs
Technology Group Biological

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O&M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Aerobic	Applicable to PCB-	Highly variable,	Unknown	Innovative	Unknown	Not commercially	Unknown	, S
Biodegradation	contaminated soils	10 to 50% typical				available		
Anaerobio Biological Activated Carbon Process	Potentrally applicable	Unknown	Unknown	Not demonstrated	Unknown	Not commercially available	Unknown	- 9
Anaerobic Dechlorination	Applicable to PCB contaminated soils	Unknown	Unknown	Experimental	Unknown	Not commercially available	Únknown	No.
Slurry Phase Bioreactor	Applicable to PCB/PCE-contaminated soils	Highly variable	Unknown	Innovative	High materials handling	Uses conventional equipment	Produces liquid waste stream	Yes

1 See Table 4-4B for rejection rationale. Technologies that have not been retained are shaded

PRELIMINARY TECHNOLOGY SCREENING SOIL AND SEDIMENTS TABLE 4-2B

Retain Yes/No

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Contaminent Group Technology Group	PCBs Physical/Chemical Process	Process					
Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts
BEST, Process	Applicable to sludges and sediments containing organic contaminants	Low to Medium	ТОМ	Innovative	High matenals handling	Equipment avaliable	Produces waste stream containing contaminants removed
CF Systems Organic Extraction System	Applicable to sludges and sediments containing organic containing organic	%02	Moderate	Innovative	High materials handling	Equipment available	Produces waste stream containing containing fromoved produces large volume of residues
Fenton's Reagent Decomposition	Applicable to PCB/PCE.	77% for PCBs	Moderate	Experimental	Unknown	Unknown	No major impacts identified
Glycolate Dechlornation	Applicable to soils containing PCBs or highly concentrated chlorinated organics	Variabie	Moderate	Innovative	High matenals handling	Equipment available	Produces waste stream

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Produces waste stream containing contaminants removed

Uses readily available equipment

High materials handling

Innovative

₹

Low to Medium

Applicable to PCB contaminated soils

Surfactant Washing

1 See Table 4-4B for rejection rationale Technologies that have not been retained are shaded

Contaminant Group PCBs
Technology Group Thermal

Technology	Applicability	Removal Poten Efficiency Clea	Potential to Meet Cleanup Goal	Technology Maturity	O&M Requirements	Implementability	Adverse Impacts	Retain Yes/No
Fluidized Bed Incineration	Applicable to PCBs and a wide range of VOCs	Eg.	Hgħ	Commercially available	Requires supplemental fuel	Requires off-gas treatment, mobile units available Excavation required	No major impacts identified	Yes
Infrared Thermal Treatment	Applicable to PCB, VOC and semi- volatile contaminated soils	Moderate to High	High	Commercially available	Requires supplemental fuel, moving parts in thermal zone	Requires off-gas and afterburner treatment, mobile units available Excavation required	No major impacts identified	Yes
Rotary Kiln Incineration	Applicable to PCBs and a wide range of VOCs	Hgħ	H FB	Commercially available	Requires supplemental fuel	Requires off-gas treatment, mobile units available Excavation required	No major impacts identified	XeX
Solar	Applicable to PCB/PCE-contaminated soils	Unknown	Unknown	Innovative	Unknown	Not commercially available	No major impacts identified	, oN
Wet Air Oxidation	Applicable to PCB, volatile and semi-volatiles	Vanable	Moderate	Pilot scale	Complex process, high femperature and pressure	Equipment not readily available	Produces off-gas	Ç O Z

¹ See Table 4-4B for rejection rationale Technologies that have not been retained are shaded

PCBs	Solidification/Stabilizatio
Contaminant Group	Technology Group

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Matunty	O & M Requirements	implementability	Adverse Impacts	Retain Yes/No
Chemical	Applicable to soil	V/N	N/A*	Innovative	Unknown	Unknown	Unknown	- 2
Stabilization	containing PCBs and creosote and incinerator ash containing heavy metals							
In Situ Virnfication	Applicable to semivolatile organics, metals, radionuclides and PCBs in soil	HgH	Hgh	Demonstrated on pilot scale	Complex field activity required	Currently withdrawn from market due to operational problems	Off-gas may need treatment	- Ž
Vitrification	Applicable to semivolatile organics, metals, radionuclides and PCBs in soil	High	Hgh	Demonstrated	High	Commercial capacity unknown	Off-gas may need treatment	-oX

[&]quot; N/A refers to fact that these technologies do not remove or destroy contaminants. However, passing EP Tox or TCLP may achieve clean-up goals

¹ See Table 4-4B for rejection rationale Technologies that have not been retained are shaded

Metals	Biological
Contaminant Group	Technology Group

		Removal	Potential to Meet	Technology	& ⊗ O		Adverse	Retain
Technology	Applicability	Efficiency	Cleanup Goal	Maturity	Requirements	Implementability	Impacts	Yes/No

Metals	Thermal
Contaminant Group	Technology Group

ntaminant Group	chnotogy Group
ပိ	۴

Metals Physical/Chemical

Applicability Technology

Removal Efficiency

Requirements No new technologies or new information on previously identified technologies in Final TSP

Retain Yes/No

Adverse Impacts

Implementability

ಶ ಶ

Technology Maturity

Potential to Meet Cleanup Goal

Metals	Solidification/Stabilization
Contaminant Group	Technology Group

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
In Situ Vitrification	Applicable to most metals in soil	N/A.	N/A*	Developing	High energy use Labor intensive	Currently withdrawn from commercial availability due to operational problems	Potential for toxic emissions May not be implementable near building foundations or areas of buried utilities	- 2

N/A refers to the fact that these technologies do not remove or destroy contaminants However, passing EP Tox or TCLP may achieve cleanup goals

¹ See Table 4-4B for rejection rationale Technologies that have not been retained are shaded

Radionuciide	Biological
Contaminant Group	Technology Group

Retain	Yes/No
Adverse	Impacts
	Implementability
№	Requirements
Technology	Maturity
Potential to Meet	Cleanup Goal
Removal	Efficiency
	Applicability
	Technology

Metals	Physical/Chemical
Contaminant Group	Technology Group

		Removal	Potential to Meet	Technology	& O ⊗		Adverse	Retain
Technology	Applicability	Efficiency	Cleanup Goal	Maturity	Requirements	Implementability	Impacts	Yes/No

Metals	Thermal
Contaminant Group	Technology Group

		Removal	Potential to Meet	Technology	№ & O		Adverse	Retain
Technology	Applicability	Efficiency	Cleanup Goal	Maturity	Requirements	Implementability	Impacts	Yes/No

Metals	Solidification/Stabilization	
Contaminant Group	Technology Group	

Technology	Applicability	Removal Efficiency	Potential to Meet Cleanup Goal	Technology Maturity	O & M Requirements	Implementability	Adverse Impacts	Retain Yes/No
In Situ Vitrification	Applicable to most radionucildes in soils	.v\	A\./A	Developing	High energy use Labor intensive	Currently withdrawn from commercial availability due to operational	Potential for toxic emissions May not be implementable near building foundations or areas with burled utilities	" Ž
Polymerization- Polyethylene	Low level radioactive wastes	N/A*	N/A*	innovative	HgH.	Equipment available	increased waste volume	No.

N/A refers to the fact that these technologies do not remove or destory contaminants. However, passing EP Tox or TCLP may achieve cleanup goals

See Table 4-4B for rejection rationale Technologies that have not been retained are shaded

TABLE 4-3A

SUMMARY OF GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES RETAINED AFTER PRELIMINARY SCREENING

Contaminant Group	Physical Treatments	Chemical Treatments	Biological Treatments	Thermal Treatments
Volatile Organics	Aqua Detox (Low Vacuum Steam Stripping) In Situ Air Stripping		Aerobic Biological Reactors	
Semivolatile Organics	Activated Carbon (1) Aqua Detox (Low Vacuum Steam Stripping) Freeze Crystallization (1) Steam Stripping (1)	Catalytic Dechlorination (1) Gamma Irradiation (1) Ozonation (1) Peroxide Oxidation (1) Ultraviolet Oxidation (1) Ultraviolet Photolysis (1)	Contact Stabilization Extended Aeration Powdered Activated Carbon (1) Pure Oxygen Activated Sludge Submerged Aerobic Fixed Film Reactor (1)	Steam Stripping/Catalytic or Thermal Oxidation (1) Supercritical Water Oxidation
PCBs	Activated Carbon Freeze Crystallization	Ozonation Peroxide Oxidation Ultraviolet Oxidation Ultraviolet Photolysis	Powdered Activated Carbon	Supercritical Water Oxidation
Inorganics			Biodenitrification	
Metals	Ultrafiltration			
Radionuclides		Potassium Ferrate Precipitation		

(1) Technology retained in preliminary screening for semivolatiles in the Final TSP were not subjected to final screening

TABLE 4-3B

SUMMARY OF SOIL/SEDIMENT TREATMENT TECHNOLOGIES RETAINED AFTER PRELIMINARY SCREENING

Contaminant Group	Contaminant Group Biological Treatments	Physical/Chemical Treatments	Thermal Treatments	Solidification/Stabilization Treatments
PCBs	Slurry Phase Bioreactor	A N	Fluidized Bed Incineration Infrared Thermal Treatment Rotary Kiln Incineration	A
Metals	¥2	Ā	NA	Ą Z
Radionuclides	NA	NA	NA	NA

NA - No Additional technologies

TABLE 4-4A

Technology	Reason Rejected from Consideration at This Time
Volatile Organics - Chemical Treatments	
Catalytic Oxidation	Unknown effectiveness and ability to meet cleanup goals Technology not sufficiently developed
Solar Photocatalytic	Unknown potential to meet cleanup goals Technology in experimental stage and not sufficiently developed
Volatile Organics - Biological Treatments	
Aerobic Reductive Dechlorination	Unknown effectiveness, implementability and economics Process in early development stage
Cometabolism Biological Process	Low potential to meet cleanup goal Technology not sufficiently developed
Semivolatile Organics - Physical Treatments	
Carbon Dioxide Extraction	Effective on limited number of constituents Unknown potential to meet cleanup goals
Semivolatile Organics - Chemical Treatments	
Catalytic Oxidation	Unknown potential to meet cleanup goals Technology is in the experimental stage and not sufficiently developed
Solar Photocatalytic	Unknown potential to meet cleanup goals Technology in experimental stage and not sufficiently developed

TABLE 4-4A

Technology	Reason Rejected from Consideration at This Time
Semivolatile Organics - Biological Treatments	
Anaerobic Biological Activated Carbon Process	Low potential to meet cleanup goals Technology not sufficiently developed Additional treatment systems would be required
Anaerobic Reductive Dechlorination	Unknown effectiveness, implementability and economics Process in early development stage
Cometabolism Biological Process	Low potential to meet cleanup goals Technology is in the experimental stage and not sufficiently developed Process is sensitive to influent containment concentrations
In Situ Bioremediation	Low potential to meet cleanup goals Difficult to control and treat broad mixture compounds
PCBs - Physical Treatments	
Solvent Extraction	Low potential to meet cleanup goals at low PCB concentrations Recovered contaminants require treatment
PCBs - Chemical Treatments	
Catalytic Oxidation	Unknown ability to meet cleanup goals Technology is in the experimental stage and not sufficiently developed for PCBs
Solar Photocatalytic	Unknown potential to meet cleanup goals Technology not sufficiently developed for PCBs

TABLE 4-4A

Technology	Reason Rejected from Consideration at This Time
PCBs - Biological Treatments Anaerobic Biological Activated Carbon Process	Unknown potential to meet cleanup goals Additional data needs to be developed to assess effectiveness implementability and O&M requirements
PCBs - Thermal Treatments Solar	Unknown potential to meet cleanup goals Technology not sufficiently developed water matrix with low concentrations of contaminants
Inorganics - Chemical Treatments Catalytic Oxidation	Unknown ability to meet cleanup goals Technology not sufficiently developed for inorganic treatment
<u>Metals - Physical Treatments</u> Hardwicka Binata Bark Adsorption	Unknown ability to meet cleanup goals Technology is in the experimental stage and not sufficiently developed

TABLE 4-4A

Technology	Reason Rejected from Consideration at This Time
Metals - Biological Treatments	
Activated Sludge	Questionable potential to meet cleanup goals. Low potential for application at RFP Produces large volumes of potentially hazardous waste.
Biosorption (Bioaccumulation)	Unknown ability to meet cleanup goals Technology not sufficiently developed Inadequate data has been developed to date on this technology, produces waste sludge
Radionuclides - Physical Treatments	
Alternating Current Electrocoagulation	Unknown potential to meet cleanup goals Technology not sufficiently developed for treatment of radionuclides
Emulsion Liquid Membrane Extraction	Unknown potential to meet cleanup goals Unknown O&M requirements and problems with implementability Inadequate data has been developed on this technology to date
Hollow-Fiber Supported Liquid Membrane	Unknown potential to meet cleanup goals Technology not sufficiently developed
Radionuclides - Biological Treatments	
Enzymatic Microbial Reduction	Unknown potential to meet cleanup goals Unknown O&M requirements and implementability
Biosorption (Bioaccumulation)	 Unknown potential to meet cleanup goals Technology not sufficiently developed Produces large volume of radioactive solid waste

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TABLE 4-4B

SOIL/SEDIMENT TREATMENT TECHNOLOGIES NOT PASSING PRELIMINARY SCREENING

Technology	Reason Rejected from Consideration at This Time
PCBs - Biological Treatments	
Aerobic Biodegradation	Low potential to meet cleanup goals Technology not sufficiently developed for PCBs
Anaerobic Biological Activated Carbon Process	Unknown potential to meet cleanup goals Technology not sufficiently developed for PCBs
Anaerobic Dechlorination	Unknown ability to meet cleanup goals Technology is in the early development stage and more research is required
PCBs - Physical/Chemical Treatments	
BEST Process	Low potential to meet cleanup goals Production of wastes
CF Systems Organic Extraction Systems	Low potential to meet cleanup goals Production of wastes
Fenton's Reagent Decomposition	Low potential to meet cleanup goals Technology not sufficiently developed Fenton's reagent decomposition can produce intermediate products that need treatment
Glycolate Dechlorination	Sultable for high concentrations of PCBs Questionable potential to meet cleanup goals Produces a liquid waste
Surfactant Washing	Unknown potential to meet cleanup goals Technology is still in the experimental stage and not sufficiently developed

TABLE 4-4B

SOIL/SEDIMENT TREATMENT TECHNOLOGIES NOT PASSING PRELIMINARY SCREENING

Technology	Reason Rejected from Consideration at This Time
PCBs - Thermal Treatments	
Solar	Unknown potential to meet cleanup goals Technology not sufficiently developed
Wet Air Oxidation	Questionable ability to meet cleanup goals Suitable for wastes with high organic concentrations Produces offgas and liquid waste
PCBs - Solidification/Stabilization Treatments	
Chemical Stabilization	Unknown potential to meet cleanup goals Technology not sufficiently developed
In Situ Vitrification	Currently not available Withdrawn from market by vendor due to operational problems
Vitrification	Unavailability of commercial capacity
Metals - Solidification/Stabilization Treatments	
In Situ Vitrification	Currently not available Withdrawn from market by vendor due to operational problems
Radionuclides - Solidification/Stabilization Treatments	
In Situ Vitrification	Currently not available Withdrawn from market by vendor due to operational problems
Polymerization - Polyethylene	High O&M requirements Increase in waste volume

TABLE 4-5A

GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES FINAL TECHNOLOGY SCREENING

Technology	Additional Data from Laboratory, Bench or Pilot Bench Testing Needed for Selection	Offers Advantages over Other Available Technologies*	Amenable to Testing at Bench/Lab Scale	Test at Bench/Lab Scale	Amenable to Testing at Pilot Scale	Anticipated EPA, State, and/or Community Acceptance	Test** at Pilot Scale
Volatile Organics - Physical Treatments							
In Situ Ar Stripping	ON.	Yes	<u>8</u>	Š	Yes	No problems anticipated	Š
Aqua Detox (Low Vacuum Steam Stripping)	S S	Yes	2	Š	Yes	No problems anticipated	Š
Volatile Organics - Chemical Treatments							
Ozonation	Yes	Yes	2	Š	Yes	No problems anticipated	Yes
Peroxide Oxidation¹	No ²	Yes	2	Š	Yes	No problems anticipated	Š
Ultraviolet Oxidation¹	No ²	Yes	8	2	Yes	No problems anticipated	8 8
Ultraviolet Photolysis	Yes	Yes	2	2	≺es	No problems anticipated	Yes
Volatile Organics - Biological Treatments							
Aerobic Biological Reactors	Yes	<u>8</u>	Yes	2	Yes	No problems anticipated	8 N
Semivolatile Organics - Physical Treatments							
Aqua Detox (Low vacuum steam stripping)	Š	Yes	2	8	Yes	No problems anticipated	8 8
Activated Carbon	o _N	Yes	Yes	2	Yes	No problems anticipated	8
Freeze Crystallization	N _O	Yes	Yes	2	Yes	No problems anticipated	8
Steam Stripping	8	Yes	Yes	Š	Yes	No problems anticipated	Š

¹ Subjected to final screening in Final TSP New information from treatability testing warrants reexamination

² OU specific bench test and IRA program at OU1 will provide adequate information

TABLE 4-5A

GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES FINAL TECHNOLOGY SCREENING

Technology	Additional Data from Laboratory, Bench or Pilot Bench Testing Needed for Selection	Offers Advantages over Other Available Technologies*	Amenable to Testing at Bench/Lab Scale	Test at Bench/Lab Scale	Amenable to Testing at Pilot Scale	Anticipated EPA, State, and/or Community Acceptance	Test** at Pilot Scale
Semivolatile Organics - Chemical Treatments							
Catalytic Dechlorination	Yes	8	Yes	8	Yes	No problems anticipated	8
Gamma Irradiation	Yes	<u>8</u>	S	8	Yes	No problems anticipated	8
Ozonation	Yes	Yes	2	8	Yes	No problems anticipated	Yes
Peroxide Oxidation	No.	Yes	2	8	Yes	No problems anticipated	8
Ultraviolet Oxidation	ÇON V	Yes	Š	Š	Yes	No problems anticipated	2
Ultraviolet Photolysis	Yes	Yes	£	8	Yes	No problems anticipated	Yes
Semivolatile Organics - Biological Treatments							
Contact Stabilization	Yes	o N	Yes	2	Yes	No problems anticipated	2
Extended Aeration	Yes	Š	Yes	S	Yes	No problems anticipated	2
Powdered Activated Carbon	No No	Yes	Yes	8	Yes	No problems anticipated	2
Pure Oxygen Actuated Sludge	Yes	o N	Yes	8	Yes	No problems anticipated	2
Submerged Aerobic Fixed Film Reactor	Yes	<u>8</u>	Š	8	Yes	No problems anticipated	S _o

 $^{\mathrm{1}}$ OU specific bench test and IRA program at OU1 will provide adequate information

TABLE 4-5A

GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES FINAL TECHNOLOGY SCREENING

Technology	Additional Data from Laboratory, Bench or Pilot Bench Testing Needed for Selection	Offers Advantages over Other Available Technologies*	Amenable to Testing at Bench/Lab Scale	Test at Bench/Lab Scale	Amenable to Testing at Pilot Scale	Anticipated EPA, State, and/or Community Acceptance	Test** at Pilot Scale
Semivolatile Organics - Thermal Treatments							
Steam Stripping/Catalytic or Thermal Oxidation	9	Yes	8	S S	Yes	Problems expected	2
Supercritical Water Oxidation	Yes	o N	2	8	Yes	Problems expected	2
PCBs - Physical Treatments							
Activated Carbon	%	Yes	Yes	Š	Yes	No problems anticipated	ž
Freeze Crystallization	8	o _N	Yes	Š	Yes	No problems anticipated	2
PCBs - Chemical Treatments							
Ozonation	Yes	Yes	Yes	Yes	Yes	No problems anticipated	8
Peroxide Oxidation	Yes	Yes	Yes	Yes	Yes	No problems anticipated	2
Ultraviolet Oxidation	Yes	Yes	Yes	Yes	Yes	No problems anticipated	8
Ultraviolet Photolysis	Yes	Yes	Yes	Yes	Yes	No problems anticipated	Š
PCBs - Biological Treatments							
Powdered Activated Carbon	8	Yes	Š	8	Yes	No problems anticipated	8
PCBs Thermal Treatments							
Supercritical Water Oxidation	Yes	<u>0</u>	8	2	Yes	Problems expected	Š
Inorganics - Biological Treatments							
Biodenitrification	o Z	Yes	8	2	Yes	No problems anticipated	o N

TABLE 4-5A

GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES FINAL TECHNOLOGY SCREENING

Technology	Additional Data from Laboratory, Bench or Pilot Bench Testing Needed for Selection	Offers Advantages over Other Available Technologies*	Amenable to Testing at Bench/Lab Scale	Test at Bench/Lab Scale	Amenable to Testing at Pilot Scale	Anticipated EPA, State, and/or Community Acceptance	Test** at Pitot Scale
Metals - Physical Treatments							
Ultrafiltration	Yes	Yes	Yes	Yes	Yes	No problems anticipated	Š
Radionuclides - Chemical Treatments							
Potassium Ferrate Precipitation (TRU Clear™)	Yes	Yes	Yes	Yes	Yes	No problems anticipated	8

Includes one or more advantages pertaining to cost effectiveness, O&M requirements, or fewer adverse impacts relative to applicable technologies
 ** Need for pilot testing will be reviewed in future annual reports. Review will be based on results achieved during bench/lab tests (if conducted) and an additional review of site characterization, ARARs, technology data, cost of pilot testing and full scale implementation.

TABLE 4-5B

SOIL/SEDIMENT WATER TREATMENT TECHNOLOGIES FINAL TECHNOLOGY SCREENING

	Additional Data from Laboratory, Bench or	Offers Advantages over Other	Amenable to Testing at	Test at	Amenable to Testing	Anticipated EPA, State,	Test**
Technology	Pilot Bench Testing Needed for Selection	Available Technologies*	Bench/Lab Scale	Bench/Lab Scale	at Pilot Scale	and/or Community Acceptance	at Pilot Scale
PCBs - Biological Treatments							
Slurry Phase Bioreactor	Yes	Yes	8	Š	Yes	No problems anticipated	Yes
PCBS - Thermal Treatments							
Fluidized Bed incineration	N _o	Yes	Yes	8	Yes	Problems Expected	<u>8</u>
Rotary Klin Incineration	o _N	Yes	Yes	8	Yes	Problems Expected	Š
Infrared Thermal Treatment	Yes	Yes	S _N	Š	Yes	Problems Expected	S _S

* Includes one or more advantages pertaining to cost effectiveness, O&M requirements, or fewer adverse impacts relative to applicable technologies
** Need for pilot testing will be reviewed in annual reports. Review will be based on results achieved during bench/lab tests (if conducted) and an additional review of site characterization, ARARs, technology data, cost of pilot testing and full scale implementation, and EPA/CDH input

TABLE 4-6A

SUMMARY OF GROUNDWATER/SURFACE WATER TREATMENT TECHNOLOGIES SELECTED FOR BENCH OR LABORATORY SCALE TREATABILITY STUDIES

Technology	Contaminant	Appendix B Page Number for Technology Data Sheet
Adsorption ¹	Metals/Radionuclides	B-5
Ion Exchange ¹	Metals/Radionuclides	B-37
Oxidation/Reduction ¹	Metals/Radionculides	B-39
Ozonation	PCBs	B-63
Peroxide Oxidation	PCBs	B-63
Potassium Ferrate¹ Precipitation (TRU-Clear™)	Metals/Radionuclides	B-44
Ultrafiltration/1 Microfiltration	Metals/Radionuclides	B-62
Ultraviolet Oxidation	PCBs	B-63
Ultraviolet Photolysis	PCBs	B-63

¹ Technologies previously selected for testing in the Final TSP

TABLE 4-6B

SUMMARY OF SOIL/SEDIMENT TREATMENT TECHNOLOGIES SELECTED FOR BENCH OR LABORATORY SCALE TREATABILITY STUDIES

Technology	Contaminant	Appendix C Page Number for Technology Data Sheet
Magnetic Separation ¹	Radionuclides	C-22
Physical Separation ¹	Metals/Radionuclides	C-25
Soil Washing ¹	Metals/Radionuclides	C-32
Solidification/Stabilization	Metals/Radionuclides	C-37
Polymerization-Epoxy ¹		
Polymerization-Polyester ¹		
Portland Cement ¹		
Masonry Cement ¹		
Gravimetric Physical Separation (TRU Clean™)¹	Metals/Radionuclides	C-17

¹ Technologies previously selected for testing in the Final TSP

TABLE 4-7
TREATMENT TECHNOLOGIES SELECTED FOR PILOT SCALE TREATABILITY TESTING

Soil/Sediment Treatment Technology	Estimated Cost of Pilot Study	Appendix B or C Page Number for Technology Data Sheet
Ozonation for VOCs/Semivolatiles	\$250,000	B-59
Slurry Phase Bioreactor for PCBs	\$300,000	C-31
Ultraviolet Photolysis for VOCs/Semivolatiles	\$250,000	B-59

/R TS 22 2 RP*

APPENDIX A POTENTIAL APPLICABLE OR RELEVANT AND APPROPRIATE REQUIREMENTS FOR THE SITEWIDE TREATABILITY STUDIES PROGRAM

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A-1 1

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TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/1)

						FED	FEDERAL STANDARDS	RDS			STA	STATE STANDARDS (TBCs)	URDS (TBC)	-			
					Γ	SDWA		SDWA			CDH W	QCC Grounk	Swater Quality	CDH WQCC Groundwater Quality Standards (d)	Ð		
					Maximum	Maximum		Maximum		Statowide		Site-Specific (g)	3)				
	*	5				Contaminant	뇓	minent			Table 1	Table 2	Table 3	Table 4	Table 5	Table 6	
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TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/l)

TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/l)

						FED	FEDERAL STANDARDS	KRDS			STA	STATE STANDARDS (TBCs)	ARDS (TBC)	•		
					SDWA	SDWA	SDWA	SDWA			CDH W	OCC Gross	Jwater Quali	CDH WQCC Groundwater Quality Standards (d)	5	
					Maximum	Maximum	Maximum	Maximum		Statewide		She-Specif	(8)			
		5			Contaminant	Contaminant	Contaminant	Contaminant		Teble	ı	Table 2 Table		Table 4	Table 5	Table 6
		MDF		,	Lovei	Lovel	Lovel	Level	Subpart F	<	Hamen	Secondary	Secondary Agriculture TDS	SQT.	Chronic	Radioneclides
Purameter	<u> </u>		CDH	Method (6)	TBC.	rBCs	Coals TBCs (a)	Goel TBCs (8)	Limt (c)	<u> </u>	Howith	Drinking				Woman Walnu
2,4 5-TP Silvex	<u>.</u>		0.5	P	01	S		S	2	ጽ						
2,4-Dichlorophenoxyacetic Acid	<u>a</u>		_	-	100	70		8	<u>8</u>	92						
(2 4-D)	_															
Acrolein	_		2													
Aldicart	_		으			3(e)		1 (e)		2						_
Aldrin		900		ව						0 002					0 000074	
Bromacil	<u>a</u>															
Carbofuran	<u>~</u>			70		\$		\$		36						
Chloranii	_							-								_
Chlordene (Alpha)	_	0.5	_	ච		2		0		0 03					0 00046	
Chlordene (Gamma)	_	0.5	_	ق		2		0		0 03					0 00046	
Chlorpyrifos	۵.			E619												
DDT	_		-	<u>ඩ</u>						0 1					0 000024	
DDT Metabolite (DDD)	_	-0		ರಿ												
DDT Metabolite (DDE)	<u>.</u>	- 0	0 1	ಕಿ						-0						
Demeton	_															
Diazimon	۵.															
Dicidrin	<u>a</u>	- 0	0 1	Đ						0 002					0 000071	
Endosuifan I	<u>.</u>	8		චි												
Endosulfan II	۰.	-		G												
Endosulfan sulfate	_	-		C _P												
Endrin	_		-	ಕ್ರಿ	0 2				0 2	0 2						
Endrin Aldehyde	_		0 1					_		0 2						
Endrin Ketone	_	0.1		ਰੂ												
Guthion	_															
Heptachlor	ے	90 0		G		0.4		0		900 0					0 00028	
		98	0 05	ಕ್ರಿ		0.2		0		600						
Hexachlorocyclohexane, Alpha	<u>_</u>	0 05		G						900 0					0 0092	

TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/l)

				lidos	Velnut	Creek																						,	S		2	:	: 2
			Table 6	Radionaclidos	Woman Walnut	Creek																							<u> </u>		08		
	9		Table 5	Chronic			0.0163			0.0173	0.0125	2				0,000070	4										_m						
€	CDH WQCC Groundwater Quality Standards (d)		Table 4	SOT																													
ARDS (TBC	adwater Qual	(g)	Table 3	Secondary Agriculture TDS																													
STATE STANDARDS (TBCs)	VQCC Groun	Site-Specific (g)	Table 2	Secondary	Drinking	·																											
ST.	CDH		Table 1	Human	Health								8					<u>~</u>														15(8)	4 mrcm/yr
		Statewide	Table	<	<u>6</u>						0 2		\$			0 005		0 03	!											6	<u> </u>		
			RCRA	Subpart F	Limit	<u> </u>		_			0 4		8					5.0															
URDS	SDWA	Maximum	Contaminant	Level	Goal	TBC. (b)					0.2		5			0		0															
FEDERAL STANDARDS	SDWA	Maximum	Contaminant	Lovel	Goels	TBCs (a)																											
FED	SDWA	Maximum	Conteminent	Lovel	TBCs	(0)					0.2		40			0.5		3									9						
	SDWA	Meximum	Contaminant	Lovel	TBC	(0)					4		100																			15 (8)	50 (4 mrem/yr)
					Method	9	a		ਰੈ	•	පි		ਹੈ			a	•	දී		-	c C	<u>ئ</u>	a	ਹੈ	ට්	ਹੈ	v						
						8		0 05		0 5(9)	0 00		0.5			_		5									<u>6</u>						
			₹	MDI.		Æ	0 05		0 05		900		0.5			0.5		-		0.5	0 \$	0 5	0.5	0.5	_	_			100		_	2	4
					2	6	_	_	_			_	<u> </u>	<u> </u>	_		۵.	۵.	_				2			£	2	ســـــــــــــــــــــــــــــــــــــ			~		~
							Hexachlorocyclohexane Beta	Hexachlorocyclohexane BHC	Hexachlorocyclohexane Delta	Hexachlorocyclohexane Tech	Hexachlorocyclohexane, Lindane P	Malathion	Methoxychlor		5						Aroclor 1221	Aroclor 1232				Arodor 1260	Atrazine	Americium (pCi/l)	S			_	Gross Beta (pCi/l)

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TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/l)

						FEI	FEDERAL STANDARDS	ARDS			STA	TE STAND	STATE STANDARDS (TBCs)	•			
					SDWA	SDWA	SDWA	SDWA			CDH W	ACC Grown	dwater Quali	CDH WQCC Groundwater Quafty Standards (d)	9		
					Maximum	Meximum	Maximum	Maximum		Statewide	1	Site-Specific (g)	k (g)				
		₹			Contaminant	Contaminant	Contaminant	Contaminant	RCRA	Table	Table 1	Table 2	Table 3	Table 4	Table 5	Table 6	
		MDL			Lovel	Level	Lovel	Level	Subpart F	<	Human	Secondary	Secondary Agriculture TDS	SOT	Chronic	Radion	Radiomedides
	2 4	Ē	- {	Method	TBCs	TBC	Confe	Goe Goe	Comit	<u>@</u>	Houlth	Drinking			-	Women	Welmu
738173010404010101010101010101010101010101010		100	5	(2)	(8)	(a)	19(4)	1 BCs (0)	(6)	60,0						10	Creek
		0 5/1 0 (4)			_,v					(7) (7)							
		1			1					(4)							
	~				8(3)					8(2)						60	•
Thorium 230+232 (pCi/l)	~									(2) 09						·	
Tritium (pCI/I)	~				20 000 (3)					20 000 (2)						80	200
Uranium 233+234 (pCi/l)	_																
Uranium 235 (pCi/l)	=	90				_											
Uranium 238 (pCi/l)	~	90															
Uranium (Total) (pCi/l)	~															اد.	2
	-																
cone	Sv		2	<u>.</u>						7							
	_	2		೮													
Yrtho)		2		బ		009		90		029							
				عـ						0 05							
_		2	_	೮						970							
(Para)		9	_	೮	75		25			72					_		
		S		S						700							
TOE	SV	2	8	೮						7					1 2		
		으	S	S						21							
2 4-Dimethylphenol		2		CS													
		S	8	೮						7							
2 4-Dinitrotoluene		2		ಜ													
2 6-Dinitrotoluene		2		బ													
lene		2		೮			_									_	_
2-Chlorophenol	S¢	2		CS													
2-Methylnaphthalene		2		CS													
		2		೮													
2-Nitrounlline S	SV	S		S													

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TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/1)

Property						75C	FEDERAL STANDARDS	ARDS			ST.	ITE STAND	STATE STANDARDS (TBCs)	<u>-</u>			
POLY					SDWA	SDWA	SDWA	SDWA			CDH	ACC Gross	dwater Quali	ity Standards	Ð		
POL					Meximum	Maximum	Maximum	Maximum		Statewide		Site-Specif	(g)				
Type MDL			<u>\$</u>		Contaminant	Contaminant	Contaminant	Contaminant	RCRA	Table	Table 1	Table 2	Table 3	Table 4	Table 5	1	Table 6
17 yes 18 18 18 18 18 18 18 1			Æ.		Love	Love	Love	Level	Subpart F	<	Human	Secondary	Agriculture	SE.	Chronic		Radiomeclides
Column C		2		 Method	TBC	TBCs	Gords	Goel	Limit	<u>€</u>	Health	Drinking					Woman Walnut
10 10 CS	Parameter	(2)	RFP	(9)	(•)	②	TBCs (a)	TBCs (b)	<u> </u>								Crock
Styliable Styl	2-Nitrophenol	SV	01	CS													_
SY SO CS	3 3-Dichlorobenzidine	SV	2	S													
Phenylphenol SY SO CS	3-Nitroeniline	SV	ક્ર	 S													
Pleasy Edder SV 10 CS Elemy Edder SV 10 CS hylphanol SV 10 CS SV 10 CS CS SV 10 CS CS SV 10 CS CS Above SV 10 CS Above SV 10 CS Above SV 10 CS Above SV 10 CS Application	t 6-Dinatro-2-methylphenol	SV	જ	 S													
SV 10 CS thylphenol SV 10 CS SV 10 CS CS SV 10 CS CS SV 10 CS CS SV 10 CS CS SN 10 CS CS three SV 10 CS three SV 10 CS ory)median SV 10 CS ory)median SV 10 CS ory)median SV 10 CS ory)median SV 10 CS sylphthate SV 10 CS sylphthate SV 10 CS sylphthate SV 10 CS sylphthate SV 10 CS	4-Bromophenyl Phenylether	SV	2	cs													
Phenry Ether SV 10 CS thylphenol SV 10 CS SV 10 CS CS SV 10 CS CS ene SV 10 C SV 10 CS C chance SV 10 C Abert SV 10 CS chance SV 10 CS chance SV 10 CS chance SV 10 CS chylphthate SV 10 CS sylphthate SV 10 CS sylphthate SV 10 CS sylphthate SV 10 CS	6-Chloroaniline	SV	2	cs													
htyphenol SV 10 CS SV 50 CS SV 50 CS SV 60 CS SV	4-Chlorophenyl Phenyl Ether	SV	2	 cs													
SV 10 CS CS CS CS CS CS CS C	4-Chloro-3-methylphenol	SV	으	 CS													
SV 50 CS SV 10 CS SV 10 d SV 10 d cores SV 10 d e SV 10 CS o CS 0 CS or rithere SV 10 CS i CS 0 CS i CS 0 CS operopylybehar SV 10 CS j/jabhhalate SV 10 CS sy 10 CS inidate SV 10 CS	(-Methylphenol	SV	2	 S													
SV SO CS CS CS CS CS CS CS	4-Nitroaniline	S	S	 cs													
00000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6-Nitrophenol	SV	S	 బ													
00000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Accesphthene	SV	2	 బ													
SX 50 0 SX 50 0 SX 10 0 <td< td=""><th>Anthracene</th><td>SV</td><td>2</td><td> S</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	Anthracene	SV	2	 S													
3V 5V 3V 10 4V 10 5V 10 6V 10 8V 10	Benzidine	SV		 70			-			0 0002	0.1				0 00012		
\$V 10	Benzoic Acid	SV	S	 S													
5V 10 CS SV	Beazo(a)anthracene	SV	<u> </u>	 S													
SV 10 CS SV	Bcazo(a)pyrene	SV	으	 S													
\$V 10	Benzo(b)fluoranthene	SV	으	 CS													
SV 10 CS	Benzo(g h i)perylene	S S	2	ಬ													-
5V 10 SV 10	Benzo(k)fluoranthene	25	<u> </u>	S													
3V 10 CS 3V 10 CS 3V 10 CS 5V 10 CS 5V 10 CS 5V 10 CS	Benzyl Alcohol	S	으	S		1841											
SV 10 CS SV	bis(2-Chloroethoxy)methane	SV	2	 S													
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	bis(2-Chloroethyl)ether	SV	9	 S						0 03					00000	33	37
01 AS	bis(2-Chlorosopropyf)ether	S	2	 CS													
01 AS	bis(2-Ethythexyl)phthalate	SV	2	 CS													
SV 10	Butadiene	SV															
	Butylbeazylphthalate	SV	2	 cs													
	Chlormated Ethers	S															

TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/1)

Parameter Chloronikylchers Chlorophenol Chrywene Dibenzofuran Dibenzofuran Dibenzofuran Dibenzofuran Dibenzofuran Dibenzofuran Diethylophthalate Di-n-chwylphthalate Di-n-chylphthalate Di-n-chylphthalate Diethylphthalate Diethylphthalate Diethylphthalate Halorbenzene Halorbenzene Hancehlorobenzene Herachlorobenzene Herachlorochtadiene Herachlorochtadiene Herachlorochtadiene Herachlorochtadiene Herachlorochtadiene Herachlorochtadiene Hydrazine Indeno(1 2 3-cd)pyrene Indeno(1 2 3-cd)pyrene	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	M M M M M M M M M M M M M M M M M M M	1009) 1009) 1009) 1009) 1009) 1009)	** © S S S S S S S S S S S S S S S S S S	SDWA Maximum Contaminant Lovel (a)	SDWA Maximum Contaminant TBCs (b)	Maximum Contaminant Lovel Goals TBCs (a)	SDWA Maximum Contaminant Level Goal TBCs (b)	RCRA Subpart F Limit (c)	Statewride A A (d) (7) 7 000 7 1000 1 050 3 5	CDH Wy Table 1 Human Health 1	Sine-Specific (g) Table 2 Table Secondary Agric Driething	H WQCC Groundwater Quality Sta. Star-Specific (g) 1 Table 2 Table 3 Table an Secondary Agriculture TDS brinking Drinking	CDH WQCC Groundwater Quality Standards (d) Sine-Specific (g) Sine-Sp	(d) Table 5 Chromic 0 01 0 01 1 9	Table 6 Rathorocitics Women Walest Creek Creek
Nitrophenois Nitrosemines Nitrosodibutylamise	2 2 2		9	<u>م</u>						·					2	

TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/l)

						FEDI	FEDERAL STANDARDS	KDS			STA	TE STAND	STATE STANDARDS (TBCs)				
					SDWA	SDWA	SDWA	SDWA			CDH W	QCC Ground	CDH WQCC Groundwater Quality Standards (d)	y Standards (9		
					Meximum	Maximum	Meximum	Maximum		Statowide		Site-Specifi	300				
		<u>\$</u>			Contaminant	Contaminant	Contaminant	Contaminant	RCRA	Table	Table 1	Table 2 Table		Table 4	Table 5	Table 6	
		MDI.			Lovel				Subpart F	<	Homen	Secondary	Secondary Agriculture TDS	TDS .	Chronic	Radione	Radionuclides
	2			Method	TBCs	បី			Limit	<u>6</u>	Health	Drinking				Women	Walnut
	3	E.	EDH H	9	(3)	<u>@</u>	TBCs (a)	TBCs (b)	(c)							Creek	Crook
ile	26		9	٩											0 0014		
	2		2	٩											9100		
N-Nkrosodiphenylamine	SV	2	(6)	CSP			_								4 9		
N-Nitroso-di-n-dipropylamine	SV	으		CSF													
Pentachiorinated Ethanes	sv			مر													
Pentachlorobenzene	S		2	a.						60							
Pentachlorophenol	SV	S	ક્ષ	బ		<u>@</u>		(e) 0		200							
Phenanthrene	SV	2		బ													
Phenol	S	2		cs							_						
Phthalate Esters	SV																
Polynuclear Aromatic Hydrocarb SV	- As		<u>.</u>	عـ											0 0028		
Vinyl Chloride	S.	02	2	رد رد	2		•			2							
				į						-							
}		, <u>.</u>		i i	89		200			700							
1 2 2-1 ecraconormane		ח ע	2	ځ ځ											0 17		
			-	ح د											90		
		_•^		ું ક	7		7			7							
	>	S	_=	رد	2		. 0			0.4							
i 2-Dichloroethene (cis)	>		_	•		92	-2-	۶		2							
	 >	S		ડ													
rams)			_	•		100	=	001		<u>8</u>							
		ν.	_	C C		8	<u>.</u>	_		0 56							
		so i		ا ح													
opropene (trans)		v :		ું દ													
	> ;	2 9		<u>.</u>													
4-Methyl-2-nentanone	> >	2 2		ح د													
	· >	2 2		ე გ			-										
_	-		_		-	_	_	_		-	_	_	_	-	_	_	_

TABLE A-1 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
GROUNDWATER QUALITY STANDARDS (ug/1)

				SDWA	SDWA	SDWA	AWGS			3 10		dumber Orests	C) spectrum with a section of the Control of the Co	5		
				=	9		Meximum		Statewide		Sile Specifi	(6)	d control of	2		
	ğ			*	Contaminant	*	ŧ	RCRA	Table	Table 1	Table 2 Table	50	Table 4	Table 5	Table 6	
	MDE					Lovel	Level	12.	<		Secondary	alture	TDS	Chronic	Radionechdes	sclydes
			Pod	ő	TBCs				6	Health	Drinking				Women	Woman Walnut
Pernander (5)	RFP		(9)	(e)	②	TBCs (a)	TBCs (b)	(c)							Creek	Creek
Acrylontrile		15(9)												0 058	_	
Benzene	×	_		S		•			_							
Bromodichloromethane V	'n	_	C.						03							
Bromoform	s	_	C						-							
Bromomethane	2		C.													
Carbon Disulfide V	S		رد													
Carbon Tetrachloride V	×	_		2		•			03					~~		
Chlorinated Benzenes V	으		CV/CS													
Chlorobenzene	s.	_	CV/CS		81		8		8							
Chloroethane	으		CV													
Chloroform	S	_	رد د	Tot THM					9					0 19		
				<100**												
	2		C C													
Dibromochloromethane	S	_	C C						14							
Dichloroethenes																
Ethyl Benzene V	×		C4		700		200		089							
Ethylene Dibromide V			- P		0 05				0 0004							
Ethylene Oxide																
Halomethanes V		<u>ව</u>		81					<u>8</u>					61 0		
Methylene Chloride V	S		C C													
Pyrene	오		S													
Styrene	S.		Ç		100		8								_	
Tetrachlorocthanes V	S		c.													
proethene	S		ડ		5		0		S					80		
Toluene	2	_	C¢		000		000		000							
Trichloroethanes	<u>~</u>		C4													
Trichloroethene	S	_	CV	2		•										
Vinyl Acetate V	2		C													
Xylenes (total)	5		CV		10 000	•	10 000									

EXPLANATION OF TABLE

- = secondary maximum contaminant level TBCs
- ** = total trihaiomethanes chloroform bromoform, bromodichloromethane dibromochloromethane
- = Colorado Department of Health
- = Contract Laboratory Program
- = Environmental Protection Ageacy
- = Minimum Detection Limit for radionuclides (pCi/l) MDL
 - = picocuries per liter PC SE
- = polychlorinated biphenyl
- = Practical Quantitation Limit
- = Resource Conservation and Recovery Act PQL RCRA RFP SDWA
 - = Rocky Flats Plant
- = Safe Drinking Water Act
 - = Target Analyte List Ţ¥Ľ
- THM . = Total Tribalomethanes
- = Tentatively Identified Compound
- = micrograms per litter 11C VOA
- WQCC = Water Quality Control Commission = Volatile Organic Analysis
- (1) TDS standard see Table 4 in (6) standard is 400 mg/l or 1.25 times the background level whichever is least restrictive
 - (2) radionuclide standards see sec 3 11 5(c)2 in (d)
- (3) If both strontium-90 and tratium are present the sum of their annual dose equivalents to bone marrow shall not exceed 4 mrem/yr
 - (4) MDL for Radium 226 is 0 5 MDL for radium 228 is 1
- (5) type abbreviations are A=anion B=bacteria C=cation, D=dioxin E=element FP=field parameter 1=indicator M=motal P=pesticide PP=pesticide/PCB
 - R=radionaclide SV=semi-volatile V=volatile
- (6) method abbreviations are CT=CLP-TAL NC=non-CLP CV=CLP-VOA CS=CLP-SEMI EP=EPA-PEST CP=CLP-PEST E=EPA, a = detected as total in CV, b = detected as TICs in CS c = detected as TICs in CV
 - d = not routinely monitored e = monitored in discharge ponds f = mixture-individual isomers detected
 - (7) Where standard is below (more stringent than) PQL (CDH), PQL is standard

 - (3) Value for gross alpha excludes uranium (9) Value is CDH detection level (PQL not available)
- (a) EPA National Primary and Secondary Drinking Water Regulations 40 CFR 141 and 40 CFR 143 (as of 5/1990)
 (b) EPA National Primary and Secondary Drinking Water Regulations 40 CFR Parts 141 142 143 Final Rule Effective July 30 1992 (56 Federal Register 3526 1/30/1991)
 - (c) NCP 40 CFR 300, NCP Preamble 55 FR 8764 CERCLA Compliance with Other Laws Manual EPA/540/G-89/1006 August 1988 40 CFR 264 94
- (d) CDH/Water Quality Control Commission, The Basic Standards for Ground Water 3 11 0 (5 CCR 1002-8) 1/5/1987 amended 11/30/1991 statewide radioactive standards listed in 3 11 5(c)(2) (e) EPA National Primary and Secondary Drinking Water Regulations 40 CFR Parts 141 142 143 Final Rule Effective January 1 1993 (56 FR 30266 7/1/1991)
 - - (f) EPA Maximum Contaminant Level Gouls and National Primary Drinking Water Regulations for Lead and Copper 40 CFR 141 and 142 (56 FR 26460 6/7/91) effective 12/7/92 (g) CDH/Water Quality Control Commission Classifications and Water Quality Standards for Ground Water 3 12 0 (9/19/1991)

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

					SDWA	SDWA	SDWA	SDWA	CWA		CWA	
					Maximum	Meximum	Maximom	Maximum	AWOC for Proteotion of	oction of	AWOC for Protection of	ction of
		至			Contaminant	Contaminant	Contaminant	Contaminant	Aquatic Life (c)		Human Health (c	
		MDL			Lord	Lovel	Lovel	Level		Chronic	Water and F	Fit
	4		Ē	Method	3	TBC	Goals	Confe	Value	Value	Tie.	Consumption
Parameter		RFP	CDH	<u>@</u>		€	3	TBCs (b)			Ingestion	Only
Bicarbonate	٧	10 000	_	E310 1								
Carbonate	<	10 000		E310 1								
Chloride	<	2 000		E325	250 000*				860,000(e)	230 000(e)		
Chlorine		000		E4500					61	11		
Flouride		2 000		E340	4 000 2 000*		4 000		·			4 000
es Nitrato		2 000		E353 1	10 000			10 000			10,000	
N as Nitrate+Nitrite		2 000		E353 I		10 000	·	10 000				
N as Nkrite		2 000		E354 1		000		1 000				
Sulfate	<	2,000		E375 4	250 000*							
Sulfide	<											
									•			
Coliform (Fecal)				SM9221C	1/100 mg							
Ammonia as N	υ	2 000		E350					Criteria are pH	and temperature	Criteria are pH and temperature dependent - see criteria document	riteria docume
Dioxin	۵			₽					0 01	0 00001	0 000000013	0 000000014
Sulfor		000 001		E600								
Dissolved Oxygen		200		SM4500					2 000			
Hd	Ē	0 1		E150 1	65-85+					6.5-9		
Specific Conductance	교			E120 1								٠
Temperature									ss	SS		
Boron	_	2 000		E6010								
Total Dissolved Solids		10 000		E160 1	\$00 000				S	SS	250 000	
Aluminum		200		ธ		50 to 200*			750	87		
Antimony		8		๖					000 6	1 600	146	45 000
Arsenic		으		ד	S						0 0022	0 0175
Arrente III	Σ								360	190		
Arsenic V	Σ								850	48		
Barium		200		<u>5</u>	000	2 000 (f)		2 000 (f)			000	
Beryllium		2		ฮ					130	53	**8900	117**
Cadmium		S		t	0	5		5	39(3)	(3)	01	
Calcium	Σ	2 000	_	ธ					_			

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992) FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

	L		I		4.000	1	,,,,,					
					VACC	VAC.	SDWA		CWA		CWA	
					Maximum	Maximum			AWQC for Protection of	bection of	AWQC for Protection of	tion of
		<u>\$</u>			Continuing	Contaminant	minage	Contaminant	Aquatic Life (c)		Human Health (c)	
		MDL			Level	<u>Fore</u>	Level	Level		Chronic	Water and	Fish
	2	_		Method	3	TBCs	Goals	Goals	Velue	Value	Fish	Consumption
Permaneter	3	RFP FP	CDH (8)	(8)		(p)	•	TBCs (b)			tion	Only
Cesium	Σ	000		NC								
Chromium	Σ	2		CT	S	100		90				
Chromium III	X	S		SW8467196					002 1	210	170 000	3 433 000
Chromium VI	Σ	2		E218 5					91	11		
Cobalt	Σ	8		را							•	
Copper	Σ	22		כל	1 000•			1 300 (g)	18 (3)	12 (3)		
Cyanide	×	2		تا تا					. 22	5.2	200	
Iron	Σ	8		ָל	300 +					000	300	
Lead	×	8		ن	S			0 (2)	82 (3)	32(3)	S	
Lithium	Σ	8		NC					,			
Magnesium	Σ	2000		تا تا								
Manganese	Σ	15		ט	\$0\$						S	٤
Mercury	Σ	0 2		ל	2	2			7.	0.012	771	0 146
Molyhdenn	2	90,		. L	ı	<u> </u>						2
Nickel	: ≥	Ş		<u> </u>						6	7.5	8
Determina	2	5		; t					(c)	(5) 701	* 0	3
- Consession 1	Ε :	3 .				8					į	
Scientific	Σ	<u></u>		ָל בּ	2	8		S.		S (d)	9	
Silver	Σ	2		<u>ნ</u>	20	* 8			1 ල	0 12	S	
Sodium	Σ	200		ธ								
Strontium	Σ	200		NC								
Thellium	Σ	으		บ					1 400 (1)	40 (1)	13	48
Tin	Σ	200		NC.								
Titanium	≆	2		E6010								
Tungsten	Σ	2		E6010								
Vanadium	Σ	S		ט								
Zinc	Σ	8		ל	s 000 s				120 (3)	110 (3)		
10 to 4 7 7 7												
7 4 3-1 L Silver	a. (ç .		<u>e</u> !	S 1		8				
2 4-Dichlorophenoxyacetic Acid (2 4-D)	<u></u>		_ 5	•	8	ę.		R R				
Aldiest	۰ ۵		2 5			9		_	08(1)	(1)	920	780
	<u>-</u>	_	<u> </u>		_	(i) cl		- -				

TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

	L				KDWA	SDWA.	SDW/A	ehw.	A/MA/		V.(13).		_
					N-		1		A DOLLAR		· ·	•	
		<u>\$</u>			Contaminant	Contaminant	Contaminant	Maximum	Awardic Life (c)	loction of	AWQC for Protection of Human Health (c)	Hos of	
					Level				Acute	Chronic	Water and	Fish	_
	178		_	Method	③	TBCs		Goals	Value	Value	Figh	Consumption	_
Į.	e	RFP	HQ:	(8)		(6)	①	TBCs (b)				Only	
	Δ.	0 05	<u>-</u>	ð					3.0		0 000074	6,0000 0	_
	۵,										-		
5	۵.		_	70		6		8					
Chloranil													
Chlordane (Alpha)	_	0.5	_	C		2				0 0043	0 00046	0 00048	
Chlordene (Gemme)	۵.	0.5		G C		2		0	24		0 00046	0 00048	
Chlorpyrifos	۵.		-	E619							!		
DDT	_	0 1	-	G C						1100 0	0 000024	0 000024	
DDT metabolite (DDD)	_	10	-	å									
DDT metabolite (DDE)	_	0.1	=	ů	<u></u>				1 050				
Demeton	_		=							0.1			
Diazinon	_												
Dieldrin	۵.	-	-	<u>ඩ</u> ට						0 0019		9/0000 0	
Endosulfan I	_	0 05	5	a Ü					0 22		7.	159	_
Endosulfan II	۵	5	5	ຍ									
Endosulfan Sulfate	<u>~</u>	<u>-</u>	<u>-</u>	වී									
Endrin	<u>.</u>	-	<u>-</u>	0	0.2				0 18	0 0023	-		
Endrin Aldehyde	۵.		-										
Endrin Ketone	_	-		ð									
Guthion	~ ~	ξ.	- s	ě		7			S	0 01	• 0000		
Heptachlor Epoxide	. م	0 05	0 00			0 0					0 00028	67000 0	
Hexachlorocyclohexane Alpha	۵.	0 05	0 0		<u> </u>							0 031	
Hexachlorocyclohexane, Beta	_	0 05	0.05	d)							0 0163	0.0547	
Hexachlorocyclohexase BHC	_	0 05	0 05										
Hexachlorocyclohexane Delta	<u> </u>	0 05		CP									
Hexachlorocyclohexane Technical	_		0 2								0 0123	0 0414	
Hexachlorocyclohexane (Lindane) Gama P	A 6	0 05	000	Đ	4	0.2		0.2	20				
lor		0.5	0 2	ŧ	8	\$		\$		003	8		
Mirex	_		<u>=</u>			_				100 0			

TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992) FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

	Γ		\vdash		SDWA	SDWA	VMQS	SDWA	CWA		CWA	
					Maximum	Meximum	Maximum	Meximum	AWOC for Protection of	tection of	AWOC for Protection of	tion of
		Š			Contaminant	Contaminant	Contaminant	ä	Aquatic Life (c)		Human Health (c)	
,		MDL			Level	Lovel	Level	Level	Acute	Chronic	Water and F	T.
	3		*	thod to	€	TBC	Coeds	Goals	Value	Value	Fish	Consumption
Parameter	9	RFP	CDH (3)			(b)	(e)	TBCs (b)			Ingestion	Only
Parathron	Ь		_						90 0	0 013		
PCBs	<u>.</u>	0.5	<u>ප</u> 			0.5		0	2.0	0 014	0 000079**	0 000079**
Simazine	_		v									-
Toxaphene	۵.	_	SCP			3		0	0 73	0 0002	0 00071**	0 00073**
Vaponite 2	_											
Aroclor 1016	£	0.5	ਹੈ									
	£	0.5	ਹੈ									
Aroclor 1232	£	0.5	<u>ਹੈ</u>									
	£	0.5	ਹੈ									
	£	0.5	ਹੈ									
Aroclor 1254	£	_	ਹੈ	_								
Aroclor 1260	£		ਹੈ									-
Atrazine	2		0			E		m				
Americium (pCi/I)	~											
Americium 241 (pCi/I)	~	100										
Costum 134 (pCi/l)	~	_										
Conturn 137 (pCi/l)	*			•								
Gross Alpha (pCI/I)	~	2			15 (10)							15
Gross Beta (pCM)	~	-			50 (4 mrem/yr)		-					
Photonium (pCM)	~											
Plotonium 238+239+240 (pCi/l)	~	100										
Radium 226+228 (pCI/I)	~	0 5/0 1 (9)	-		S							
Strontium 89+90 (pCi/l)	~											
Strontium 90 (pCi/l)	æ				8 (6)							•
Thorium 230+232 (pCi/l)	~											
Tritium (pCM)	~				20 000 (6)	_						
Uranium 233+234 (pCi/l)	~		_									
Urenium 235 (pCv/l)	~	90										
Uranium 238 (pCVI)	æ	90										
Uramium (total) (pCi/l)	~		_			_				_		

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

					SDWA	l	SDWA	SDWA	CWA		CWA	
					Maximum		Maximum	Maximum	AWQC for Protection of	tection of	AWQC for Protection of	etion of
		<u></u>			Contaminant	minant	Contaminant	Contaminant	Contaminant Contaminant Aquatic Life (c)		AH (C	()
····		MDL		•	Leve		Level	Level	Acute	Chronic		# # # # # # # # # # # # # # # # # # #
Parameter	6	EFP.	3 ¥	Method (3)	<u>•</u>	2 E			✓		Fish	Consumption Out:
	ł					(2)	i,	(2)			The Section	Cany
1 2 4 5-Tetrachlorobenzene	S		2	ء							38	48
1 2 4-Trichlorobenzene	S	9		ಬ								!
1 2-Dichlorobenzene (Ortho)	δV	10	2	బ		909		009				
1 2-Diphonylhydrazme	sv			a					270 (1)			
1 3-Dichlorobenzene (Meta)	sv	10	_	S					;			
1 4-Dichlorobenzene (Para)	SV	0	_	S	75		75					
2 4 5-Trichlorophenol	SV	8		CS							2 800	
2 4,6-Trichlorophenol	SV	2	ଛ	S						970 CE)	112**	36**
2 4-Dichlorophenol	SV	2	S	೮					2.020 (1)	365 (1)	3 090	
2 4-Dimethylphenol	SV	2	S	ಬ					2 120 (1)	;		
2 4-Dinitrophenol	S	S	જ	బ								
2 4-Dintrotoluene	SV	9	2	೮							: :: 0	*
2 6-Dinitrotoluene	SV	2	2	ಬ					330 (1)	230 (1)	8	14 300
2-Chloronaphthalene	SV	2		೮					•	,		· · · · · · · · · · · · · · · · · · ·
2-Chlorophenol	S	2	ક્ષ	ಬ					4 360 (1)	2,000 (1)		
2-Methylnaphthalone	SV.	2		ಬ								
2-Methylphenol	S	2		೮								
2-Nitrogniline	S	S		CS								
2-Nitrophenol	SV	2		ಬ								
3 3-Dichlorobenzidine	25	8	2	బ							100	0 02
3-Nitroantiine	>	8		೮							_	
4 6-Dinitro-2-methylphenol	2	S	S	బ								
4-Bromophenyl Phenylether	SV	2		ಬ								
4-Chloroaniline	S	2		S							•	
4-Chlorophenyl Phenyl Ether	SV	2		బ								
4-Chloro-3-methylphenoi	SV	2	જ	ಬ	-				30 (1)			
4-Methytphenol	SV	2		CS								
4-Nikroundine	SV	S		బ								
4-Nitrophenol	SV	8		బ					230 (1)	150(1)		
Acenaphthene	SV	2	2	೮					1 700 (1)	(1) 025		

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)	FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)
---	--

			ſ				Ī					
				<u>`</u>	SDWA	SDWA			CWA		CWA	
					Maximum	Maximum			AWQC for Proteotion of	tection of	AWQC for Protection of	ction of
		<u></u>			Contaminant	Contaminant	minent	minent	Aquetic Life (c)		Human Health (c))
		MDI.			Level	Lovel				Chromic	Water and	Fish
	34			po d	€	TBC	-	Goals	Value	Value	1	Consumption
Parameter	0	RFP	CDH (3)	Ð		Ð	②	TBCs (b)			Ingestion	Only
Anthracene	SV	10		cs								
Benzidine	SV		_	9					2,500		0 00012	0 00053
Benzoic Acid	SV	ક્ર		S								
Benzo(a)anthracene	SV	2	2	CS								
	sv	2		CS								
thene	SV	9		S								
Benzo(g h i)perylene	SV	9		CS								
	SV	2		S								
Benzyl Alcohol	SV.	9		8								
bis(2-Chloroethoxy)methane	SV	9		cs			_					
	SV	9	2	5							0.03**	1 36 64
ther) N	2		8 5							2.7	96 1
	>	: 9	2							_	15,000	96.4
	3	2		3							000 5	90000
1-1-1-1	3	9		ę						_		
	> 2	2		ß								
	۸ ا		_									
valence	SV.								1 600 (1)			
hers	SV	2		S					238 000 (1)			
Chilorophenol	SV		S									
Chrysene	SV	9	2	CS								
Dibenzofuran	SV	2		S								
Dibenz(a h)anthracene	SV	2	2	CS								
Dichlorobenzenes	SV								1 120 (1)	763 (1)	400	2 600
Dichlorobenzidine	SV	82		cs					,	;		0 02
Diethylphthalate	SV	9		S							350 000	1 800 000
Dimethylphthalate	SV	0	9	S							313 000	2 900 000
Di-n-butylphthalate	SV	2		S								
Di-n-octyfphthalate	sv	9		CS								
Ethylene Glycol	sv			9								
ane		2		S					3 980 (1)		42	*
Fluorene	SV	2	2	CS								

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992)
FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

	L				SDWA	SDWA	SDWA	SDWA	CWA		CWA		_
					Maximum	Meximum	Mariana	1	A WAY OF THE PARTY	A	Aumor for British of	40 10	
		\$			Contaminant	Contentinant	nineet	12	Aquetic Life (c)		Human Health (c.	caron or	
		MDL			Lovel	Lovel	Level	E ST	Acuste	Chronic	Water and	捏工	1
	2			Method	3	TBCs		Goels	Value	Value	Fig.	Constantion	_
Perimeter	ε	RFP	CDH (3)	(8)		(e)	(TBCs (b)			Ingestion	Only	
Formaldehyde	S												
Haloethers	S S								380 (1)	122 (1)			_
Hexachlorobenzene	S S	2	<u> </u>	೮							0 00072**	0 00074**	
Hexachlorobutadiene	SV	2	9	S					(I)	93(1)	0 45**	* 9S	
Hexachlorocyclopentadiene	SV	2	2	CS						5 2 (1)	206		_
Hexachloroethane	SV	2	2	cs					_	540 (1)	61	8 74	_
Hydrazine	S									· •			
Indeno(1 2 3-cd)pyrene	S	2	2	S									
Bophorone	SV	2	<u> </u>	S					117 000 (1)		5 200	520 000	
Nephthelene	SV	으	2	CS					2 300 (1)	620 (1)			
Nitrobenzene	34	2	9	CS					27 000 (1)		19 800		
Nitrophenols	SV								230 (1)	150 (1)			
Nitrosamines	SV								5 850 (1)	•			
Nitrosodibutylamine	SV		2	٩							1900 0	0 587	
Nitrosodiethylamise	SV		2	ء							8000 0	1 24	
Ntrosodimethylamise	SV		2	<u>ھ</u>							0 0014	91	
Nkrosopyrrolidise	S		으	٩							0 0 1 6	919	
N-Nitrosodiphenylamine	S	2	2	عد							49**	16 1 **	
N-Nitroso-di-a-dipropylamine	24	2	2	<u>a</u>	ų.								
Pentachlorinated Ethanes	25			ے					7 240 (1)	1 100 (1)			
Pentachlorobenzene	S		<u>e</u>	٩							74	85	
Pentachlorophenol	25	ଞ	8	೮		.		€0	20 (4)	13 (€)	010,1		
Phenanthrene	2	<u>e</u>	<u>e</u>	S									_
Presio	>>	≘	8	S					10 200 (I)	2 560 (1)	3 500		
Phthalate Esters	≥			0						3(1)			
Polynuclear Aromatic Hydrocarbons	2		<u>e</u>	<u>a</u>							0 0028**	0 031100	
Vinyl Chloride	<u>s</u>	2	7	<u>ح</u>	2						2 **	525 ***	
1 1 1-Trichlornethans	>	v	=	2	Ę		900				\$		
1 1 2 2-Tetrachloroethane	<u> </u>	<u>, </u>	<u></u>	<u> </u>	3		3			7.400	18 400	030 000	
1 1 2-Trichlomethane	· >			3 2						400		* 6 6 7 1	
	<u>.</u>	<u>.</u>	<u>.</u>	<u>;</u>	_	_	_	_	-	3		: o :	_

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

							,			\)		
					SDWA	SDWA	SDWA	SDWA	CWA		CWA	
					Maximum	Meximum		Maximum	AWQC for Protection of	ection of	AWQC for Protection of	tion of
		Š,			Contaminant	Contaminant	Contaminent	Contaminant	Aquatic Life (c)		Human Health (c)	
	·	MDL			Level			Level	Acute	Chronic	Water and	Figh
	<u>2</u>			Method	€	8	4	Goals	Value	Value	Fish	Consumption
Persactor	ε	西	(<u>Q</u>	②		②	②	TBCs (b)			Ingestion	Only
1 1-Dichloroethane	>	S.		رد								
1, f-Dichloroethene	>	S	_	C.	7		7					
1 2-Dichloroethane	>	S	_	C.	\$		•		118 000	20 000	0 24**	243 **
1,2-Dichloroethene (cis)	>		_	•		٤		20				
1,2-Dichloroethene (total)	>	2		ბ								
1,2-Dichloroethene (trans)	>	S		•		100		001				
1,2-Dichloropropene	>	5	_	C.		s				s 700		
1 3-Dichloropropene (cis)	>	8	_	C C						244 (1)		14 100
1 3-Dichloropropene (trans)	>	S	_	رد					90 9	244 (1)	87	14 100
2-Butanone	>	01		CA								
2-Hexanone	>	2		C C								
4-Methyl-2-pentanone	>	2		C.								
Acetone	>	2		CΛ								
Acrylonitrile	>		s	U					7 500	2,600	950 0	0 65
Benzene	>	2	_	ડ	5		•		s 300		**990	40 **
Bromodichloromethane	>	2		C								
Bromoform	>	S	_	ر ر								
Bromomethane	>_	2	_	رد								
Carbon Dissiffide	>_	S		رد								
Carbon Tetrachioride	>	2	_	C.	×		0		35 200 (1)		0 4**	** #\$ 9
Chiorinated Benzenes	>	9		CV/CS					250 (1)	SO(I)		•
Chlorobenzene	>	2	_	cv/cs		8		8				
Chloroethane	>	2		رد								
Chloroform	<u>></u>	S	_	رد	Tot THM<100 (2)				28 900 (1)	1 240 (1)	** 61 0	157**
Chloromethane	>	2	_	C.								
Dibromochloromethane	>	2	_	C								
Dichloroethenes	>_		_						(1) 000 (1)		0 033**	1 85 **
Ethyl Benzene	>	s	_	Ç.		700		700	32 000 (1)		1 400	3 280
Ethylene Dibromide	>			-		0 05		0				
Ethylene Oxide	>											
Halomethanes	<u>></u>		_		8		_		11 000 (1)		**6I 0	15 7 **

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TABLE A-2 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992) FEDERAL SURFACE WATER QUALITY STANDARDS (ug/l)

												-
					VMQS	SDWA	SDWA	SDWA	CWA		CWA	
					Maximum	Maximum	Meximum Meximum	Meximum	AWQC for Pro	tection of	AWQC for Prote	ection of
		<u>\$</u>				Contaminant	Contaminant	Contaminant	Aquatic Life (c.		Human Health (c	•
		MDL			Level	Lovel	Level	Level	Acute	Level Level Level Acute Chroade Wa	Water and Figh	重
	5			Method		TBCs	Goals	Goals	Value	Value	Fire	Consumption
Purameter	ε	RF	CDH (3)	9		Ð	3	TBCs (b)			Ingestion	Only
Methylene Chloride	>			CV								
Pyrene	>	2	0	CS								
Styrene	>	2		c		<u>8</u>		8				
Tetrachloroethanea	>	s	-	C					9 320 (1)			
Tetrachloroethene	>	2	_	cv		2			5 280 (1)	84 0 (1)	0 80**	8 85 **
Toluene	>	Ş		CV		1 000		000	17 500 (1)		14 300	424 000
Trichloroethanes	>	2	_	C C					18 000 (1)			
Trichloroethene	>	S	_	CV	2		0		45 000 (1)	21 900 (1)	27**	80 7 **
Vinyl Acetate	>	2		C								
Xylenes (total)	>	5		Ç		000 01		10 000				

EXPLANATION OF TABLE

* = secondary maximum contaminant level TBCs

** = Human health criteria for carcinogens reported for three risk levels Value presented is the 10-5 risk level

AWQC = Ambient Water Quality Criteria

= Contract Laboratory Program

= Clean Water Act

= Environmental Protection Agency

= Minimum Detection Limit for radionuclides (pCi/l) MOL

= picocaries per liter Ş

= polychlorinated biphenyl

= Practical Quantitation Level

= Safe Drinking Water Act PQL SDWA

= Target Analyte List = Species Specific T.Y. SS

= Total Trihalomethanes THM

= Tentatively Identified Compound

= micrograms per liter

= Volatile Organic Analysis

(1) criteria not developed, value presented is lowest observed effects level (LOEL)

(2) total tribalomethanes chloroform bromoform, bromodichloromethane, dibromochloromethane

(3) hardness dependent criteria

 (4) pH dependent criteria (7 8 pH used)
 (5) standard is not adequately protective when chloride is associated with potassium calcium or magnesium rather than sodium
 (6) if both stroatium-90 and tritium are present, the sum of their anawal dose equivalents to bone marrow shall not exceed 4 mrem/yr
 (7) type abbreviations are A=sation B=bacteria C=cation D=dioxin E=clement I=undicator FP=field parameter M=metal P=posticide PP=posticide/PCB, R=radionaclide SV=semi-volatile, V=volatile

(8) method abbreviations are CT=CLP-TAL, NC=non-CLP CV=CLP-VOA CS=CLP-SEMI EP=EPA-PEST CP=CLP-PEST E=EPA, a = detected as total in CV b = detected as TIC in CS

c = detected as TIC in CV d = not routinely monitored e = monitored in discharge ponds f = mixture-individual isomers detected

(9) MDL for radium 226 is 0 5 MDL for radium 228 is 1 0

(10) Value for gross alpha excludes uranium

(a) EPA National Primary and Secondary Drinking Water Regulations, 40 CFR 141 and 40 CFR 143 (as of May 1990) Segment 4 MCLs are ARAR Segment 5 MCLs are TBC all MCLGs are TBC (b) EPA National Primary and Secondary Drinking Water Regulations 40 CFR Parts 141 142 and 143 Final Rule effective July 30 1992 (56 Federal Register 3526 1/30/1991)

(c) EPA, Quality Criteria for Protection of Aquatic Life, 1986

(d) EPA National Ambient Water Quality Criteria for Scientum - 1987 (e) EPA, National Ambient Water Quality Criteria for Chloride - 1988 (f) EPA National Primary and Secondary Drinking Water Regulations 40 CFR Parts 141 142 and 143 Final Rule (56 FR 30266 7/1/1991) effective 1/1/1993 (g) EPA Maximum Contaminant Level Goals and National Primary Drinking Water Regulations for Lead and Copper 40 CFR 141 and 142 (56 FR 26460 67/1991) effective 12/7/91

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E160 1

otal Dissolved Solids

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Dissolved Oxygen

Coliform (Fecal) Ammonia as N

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2 8 2

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Aquatic Water Life Supply Basin Standards (b) E 2000/100 ml 500 STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l) 2 000 10 000 10 000 1 000 250 000 50 3 000 250 000 Support (E) 100,000 100 000 10 000 3 000 82 Tables I II III (1) Chronic Value (2) \$ 000 6 5-9 0 Aquetic Life
Acute Chro
Value Value
(2) (2) Statewide Standards (a) 5 000 6 5-9 0 620 0 00001 Chronic Acute Chronic Value Value 0 00000022 0 000000013 0 01 Weter and Fish Noncarcinogene Human Health Carcinogens/ (Z) (S) Water Supply SM9221C E350 SM4500 E150 1 E120 1 E4500 E4500 E340 E353 1 E353 1 E354 1 E354 1 E310 1 (6) E310 1 E600 色 100 000 500 0 1 10 000 10 000 10 000 5 000 5 000 5,000 5 000 MDE REP 900 **1 y 6**

as Nitrate

TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)

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A-3.3

2286//LITA-3 WK! 13 Feb-92/RPT

TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992) STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

								Statewad	Statewide Standards (a)	3			Bests	
													Standards (b)	.
	L				Human Health	_			T.	Tables (1)	5			
					Carcinogena/		Aquetic Life (8)	.He (8)	Aquetic Life	ife			Organics	
					Noncarcinogena		Acute	2		Chronic	Agricul-	Agricul. Doubortic	ε	
		5			(2)		Value	Velvo	2		turnal	Water	Aquetic Weter	Water
1	£.	MDL		Method	Weter	Water and			ନ	ନ	Standard Supply	Supply	9	Supply
Partition	6	RFP	8	CDH (6)	Supply	Fish					6	€		
2 4-D	۵.		_	Ð	20									100
Acrolein			2			320	53	21		_				
Aldicarb	۸.		2		10									
Aldrin	۵	9 02	<u>-</u>	G.	0 002 (8)	0 00013	1.5						0 003	
Bromacil	_													
Carbofuran	_			70	36									
Chloranil	<u>_</u>			E619										
Chlordane (Alpha)	۵.	0.5	_	Ĝ	0 03 (8)		12	0 0043						
Chlordane (Gamma)	ے	0.5	_	ď	0 03 (8)	0 00058	1 2	0 0043						
Chlorpyrifos	<u>_</u>		<u>-</u>				0 083	98						
DDT	۵.	0	-	G	0 1	65000 0	0 55	0 00					000	
DDT Metabolite (DDD)	_	-	5	Ğ		8000 0	90						100 0	
DDT Metabolite (DDE)	_	-	5	C _B	0.1	0 00059	1 050						<u>100</u> 0	
Demeton	<u>a</u>		=					=					0.1	
Diezhon	Δ.													
Dieldrin	_	-	<u>-</u>	ڻ ت	0 002	0 00014	13	0 0019					0 003	
Endosuifen I	_	0 05	<u>.</u>	රි		0 93	= 0	950 0					0 003	
Endoculfan II	۵.	-	<u>-</u>	ಶಿ										
Endosuifan Sulfate	_	-	5	å		0 93								
Endrin	_	=	<u>-</u>	ਹੈ	0 2		6 0 0	0 0023					900	
Endrin Aldehyde	۵.		<u>-</u>		0.2	0 2				_				
Endrin Ketone	<u>ه</u>	<u>.</u>		g										
Guthion	<u>~</u>		1 5	_				100					0 01	
Heptachlor	ρ.	900	0 05		800 0	0 00021	0 26	0 0038						0 2
Heptachlor Epoxide	<u>م</u>	0 05	0 05	å	60 0	1000 0	0 26	0 0038						
Hexachlorocyclohexane Alpha	_	0 05	0 05		900 0		0 0039			_				
Hexachlorocyclohexane Beta	<u>a</u>	0 05	0 S	G C		0 014								
Hexachiorocyclohexane BHC	<u>.</u>	9 05	0 05				8							
Hexachlorocyclohexane Delta	۸.	8		ů										
Hexachlorocyclohexane Tech	<u>a</u>		0 2	<u>_</u>	_	0 012	_		_				_	

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TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

								Statewa	Statewide Standards (a)	(3)			Besm	3
													Surgarus (0)	(O)
					Human Health	.e			F	Tables 1,11 III (1)	Φ			
					Carcinogens/		Aquatic Life (8)	ife (8)	Aquetic Life	Life			Organica	
-					Noncarcinogena			Chronic	Acute	Chronic	Agricul-	Domestic	9	,
		<u>%</u>			(2) (8)		Value	Value	Value	Value	Frat	Water	Aquetic	Water
	£			Method	Water	Water and			Ð	8	Standard Supply	Supply	Life	Supply
Persenter	ଚ		ĺ	(9)	Supply	Fush					ච	€		
Hexachlorocyclohexane, Lindane	۵	0 05	0 05	CP	0.2	610 0	1.0	80 0					100	0
Malathion	<u>a.</u>		0 2					0.1					-	
Methoxychlor	<u>~</u>	0.5	0.5	C	5			0 03					0 03	8
Mirex	_		-					0001					000	
Parathion	<u>a</u>					-							8	
PCBs	<u>a</u>	0.5	=	ಕಿ	0000	0 000044	2.0	0 014					0 00	
Simazine	<u>a</u>			•										
Toxaphene	۵.		s	C _P	0 03	0 00073	0 73	0 0002					0 005	20
Vaponite 2	<u>_</u>													
Aroclor 1016	운	0 5		ਹੈ										
Aroclor 1221	윮	0 5		ද										
Aroclor 1232	ድ	0.5		Đ										
Aroclor 1242	£	0.5		a										
Aroclor 1248	ድ	0 8		G										
Arodor 1254	웊	_		G		•								
Aroctor 1260	8:			C.										
Atrazine	£			•										
Americium (pCi/l)	24													
Americium 241 (pCi/l)	æ	10 0												
Cesium 134 (pCi/l)	<u>«</u>	_=			(01)									
Cesism 137 (pCi/l)	~	_												
Gross Alpha (pCi/l)	æ	2											<u>.</u>	
Gross Beta (pCi/l)	æ	4												
Plutonium (pCs/l)	~													
Plutonium 238+239+240 (pCi/I)	~	100			15 (10)								_	
Radium 226+228 (pCi/l)	<u>~</u>	0 5/1 (9)			2 (10)									
Strontium 89+90 (pCi/l)	×	_												
Strontium 90 (pCi/l)	~				8 (10)									
Thorium 230+232 (pCt/l)	<u>«</u>	_	_		60 (10)		_			_				

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TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (Rebruary 1, 1992)
STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

								Stateway	Statewide Standards (a)	€			Benin Standards (b)	3
					Unance Unable				-	far ber ber	4			
					Homen House			•	-	1 ables 1,111,1111 (1)				
					Carcinogena		Aquetic Life (8)	,ife (8)	Aquetic Life	Je			Organica	
					Noncarcinogena		Acute	Chronic	Acute	Chronic	Agricul-	Agricul- Domestic	E	
		3			(2)		Value	Value	Value	Value	teral	Weter	Aquetic Water	Water
	2	MDL.		Method	Weter	Weter and			8	2	Standard Supply	Supply	1.16	Supply
	<u>છ</u>	RFP	(9) HQ	9)	Supply	Fish					<u>©</u>	€		
	æ				20 000 (10)									
Uranium 233+234 (pCi/l)	~											,		
Uranium 235 (pCi/l)	~	90												
Uranium 238 (pCi/l)	~	90												
Uranium (Total) (pCi/l)	~								TVS	TVS				
1 2 4 5-Tetrachlorobenzeae	S			ع	2 (8)									
1 2 4-Trichlorobenzene	S	9		೮	,									
1 2-Dichlorobenzene (Ortho)	SV	9	-	ಬ	079	620								
	SV			عـ	0 05	3 0 0	270							
		2	_	ខ	620	400								
Parra)		2	_	బ	22	75								
		S		೮										
loi	S	9	S	೮	2	2		026			•			
		_	R	S	21	21	2 020	365						
76		2	S	ಬ			2 120							
		8	ଞ	೮	4	7								
		2	2	S		= 0								
		<u> </u>	2	೮			330	230						
plene		2		S										
		<u>0</u>	୫	బ			4,380	2 000						
alene	SV	2		బ							•			
		2		S										
		ક્ષ		ខ										
2-Nitrophenol		9		ន										
3 3-Dichlorobenzidine		20	2	ຽ		0 039								
3-Nikroandine		જ		CS										
4 6-Dinatro-2-methylphenol		S	৪	S		13								
4-Bromophenyi Phenyiether		2		೮										
4-Chloroanilme	<u>s</u>	2		<u>წ</u>	_						_			

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TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

									State Statement (a)	È			Standards (h)	3
	H				,	-					,			
					Human Health	€ .			-	Tables I II III (1)	3		_	
				_	Carcinogens/	>	Aquatic Life (8)	(8) (8)	Aquetic Life	Life			Organica	_
					Notestremogent	Cours	Acute	Chronic	Acute	Chromic	Agricul-	Agricul- Domestic	3	
		5			(2) (g)		Value	Value	Value	Value	tural	Water	Aquetic Water	Water
	7	MDL		Method	Water	Water and			2	8	derd	Supply	Life	Supply
Parameter	<u>S</u>	RFP	ទិ	(9) HCD	Supply	Fish					ච	€		
4-Chlorophenyl Phenyl Ether	SV	<u>e</u>		cs										
4-Chioro-3-methylphenol	\$	2	S	S			93							
4-Methylphenol	>5	9	_	S									_	
4-Nitrounline	S	: S	_	8 8										
4-Nitropheaol	SV	S		S										
Accasphthene	25	9	2	S			1 700	220						
Anthracene	SV	2	_	S		0 0028								
Benzidine	S		2	•	0 0002	0 00012(8)	2 500						10	0 01
Benzoic Acid	S	ક્ષ		CS										_
Benzo(a)anthracene	3	9	2	CS		0 0028								
Benzo(a)pyreae	SV.	2	2	CS	1.	0 0028								
Benzo(b)fluoranthene	S	9	2	CS		0 0028								
Benzo(g h i)perylene	SV	<u>e</u>	2	S		0 0028								
Benzo(k)fluoranthene	S	2	2	S		0 0028								
Benzyl Alcohol	S	<u>e</u>		S										
bis(2-Chloroethoxy)methane	S	2		S										
bis(2-Chloroethyf)ether	SV	2	2	S	0 03 (8)	0 03 (8)								
bis(2-Chloroisopropy!)ether	S	유	2	బ		1 400								
bis(2-Ethylhexyl)phthalate	S	2	2	S		18(8)								
Butadiene	S						_							
Butyl Beazylphthalate	S	92	2	S		3 000								
Chlorinated Ethers	S		_											
Cistorinated Napthalenes	S													
Chloroelkylethers	S	으		S										
Chlorophenol	20		S										0	0
Chrysene	SV	으	2	CS		0 0028	_			_				
Dibenzofurun	SV	9		CS										
Dibenz(a h)aarthracene	S	2	2	CS		0 0028								
Dichlorobeazenes	SV		_											
Dichlorobenzadane	SV	8	2	S		0 039								

A-3.7

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TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (Pebruary 1, 1992)
STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

								Statewid	Statewide Standards (a)	≆		_	Bestin	;
													Mandards (b)	ē
					Human Health	_			-	Tables I II III (1)	3			
					Carcinogens/		Aquetic Life (8)	.ife (8)	Aquetic Life	Life			Organica	
					Noncarcinogena	100	Acute	Chronic	Acute	Chromic	Agricul-	28	E	
		Ž,			(2) (g)		Value	Velue	Value	Value	tural		Aquetic Water	Water
	2	MDL		Method	Water	Water and			8	9	Standard Supply		Life	Supply
Parameter	ତ	RFP	CDH	9	Supply	Fuh					ච	€		
Dicthylphthalate	λS	01	10	CS		23 000								Ī
Directhylphthelate	δ	2	9	CS		313 000								
Di-n-butylphthelate	2	2	9	cs		2 700								
Di-n-octylphthelete	25	2		S										
Ethylene Glycol	S			7										
Fluoranthene	S	2	2	S		42	3 980							
Fluorene	SV	으	2	S		0 0028								
Formaldehyde	S													
Haloethers	S													
Hexachlorobenzene	S	2	9	ಬ	٠	0 00072								
Hexachlorobutadiese	S	2	2	S		0.45	8	93						
Hexachlorocyclopentadiene	S	으	2	S		240	7	2						
Hexachloroethane	ટ્ડ	2	으	ន		6-	980	240						
Hydrazine	SV.													
Indeno(1 2 3-cd)pyrene	λS	으	2	CS		0 0028								
Isophorone	25	으	2	S	1 050	**	117 000							
Naphthalone	S	<u> </u>	2	ಬ		0 0028	2 300	620						
Nitrobenzene	25	으	<u>e</u>	cs	3.5	3.5	27 000							
Nitrophenois	S													
Nitrosamines	≳													
Nitrosodibutylamine	ટ		으	عـ		0 0064								
Nitrosodiethylamine	25		2	م		9000 0								
Nkrosodimethylamine	S		2	٩		69000 0							•	
Nitrosopyrrolidine	8		2	<u>م</u>		9100								
N-Nitrosodiphenylamme	25	2	2	CSP		64								
N-Nkroso-di-n-dipropylamine	25	2	2	CS		0 005								
Pentachlorunated Ethanes	S<			٩										
Pentachlorobeazene	S		2	<u>a</u>	(8)									
Pentachlorophenol	ટ્ડ	S	8	S	200		6	57						
Phenanthrene	25	<u> </u>	<u> </u>	<u>ა</u>		0 0028								

Agricul-tural Tables I II III (1) Chronic Value (2) Aquetic Life Acute Chr Statewide Standards (a) Value (2) Chronic 20 000 Aquetic Life (8) Value 2 560 2 400 2 600 5 700 2 2 2 118 000 23,000 6,060 6 060 Acute Value 7 550 5 300 \$ Water and Flah 21 000 0 0028 0 057 0 17 90 98 4 Carcinogena/ Noncarcinogena 2 2 Human Health 0 Se (8) (2) (8) Water Supply **\$** 6 <u>. 6666666.6.</u>6.666666 වෙහි 8 S **5 5 6 6** Parameter (5) RI
Phenol SV II
Phthalate Esters SV
Polynaciear Aromatic Hydrocarbon SV
III
SV III
SV III
SV III
SV III 3-Dichloropropene (trans) 1 2-Dichloroethene (total) 1 2-Dichloroothene (trans) 1,3-Dichloropropene (cis) 1 1 2 2-Tetrachiorocthane 1 2-Dichloroethene (cis) I, I, 1-Trichloroethane i, i 2-Trichloroethane 2-Dichloropropune

1, 1-Dichlorocthane 1,2-Dichlorocthane 1,1-Dichloroethene

Supply Aquatic Water

Weder Suppty (4)

€

Basin Standards (b)

STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)

A-3 6

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Carbon Tetrachloride Chlorinated Benzenes Chlorobenzene

Carbon Disulfide

-Methyl-2-pent

35 200

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TABLE A-3 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992)
STATEWIDE AND BASIN (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

								Statewid	Statewide Standards (a)	€			Regin	
													Standards (b)	ૄ
	_				Human Health	_			2	Tables I,II III (f)	(2)	ì		
					Carcinogens/		Aquatic Life (8)	ife (8)	Aquatic Life	Life			Organica	_
					Noncarcinogena		Acute		Acute	Chronic	Agricul	Agricul- Domestic	E	
		\$			(S) (B)		Value		Value	Value	Trans.	Water	Aquetic Weter	Water
	T.	MDL		Method	Water	Wetor and			2	2	Standard Supply	Supply	Life Life	Supply
Parameter	ଚ	RFP	(9) HQD	9	Supply	Fush					ල	€		:
Chloroethane	>	2	L	رد										
Chloroform	>	S	_	<u>ر</u>	و	9.	28,900	1 240						
Chloromethane	>	2	_	C C		5.7								
Dibromochloromethane	>	'n	_	ડ	4	9								
Dichloroethenes	>													
Ethyl Benzene	<u>></u>	s	_	C C	089	3 100	32 000							
Ethylene Dibromide	>			9										
Ethylene Oxide	>													
Halomethanes	>				92									
Methylene Chloride	>	'n	_	رد		47								
Pyrene	>	2	으	S		0 0028								
Styrene	>	S		رد										
Tetrachloroethanes	>	s	_	C C										
Tetrachioroethene	>	<u>.v</u>	=	CV CV	2	80	5 280	3						
Toluene	>	S	-	<u>ડ</u>	000	000	17 500							
Trichloroethanes	>	S.	=	C4										
Trichloroethene	>	'n	_	C.	8	2.7	45 000	21 900						
Vinyl Acetate	>	2	_	C.										
Xylenes (Total)	>	S		۲										

EXPLANATION OF TABLE

- = Contract Laboratory Program
- = Colorado Department of Health
 - = dissolved
- = Environmental Protection Agency
- = Minimum Detection Limit for radionuclides (pCi/l)
 - = picocuries per liter E PC
- = polychlorinated biphenyl
- = Practical Quantitation Level
 - = species specific
 - = Target Analyte List SS ZAT TAL
- = Total Trihalomethanes
- = Table Value Standard (hardness dependent), see Table III in (a) = Tentatively Identified Compound
 - = micrograms per liter
- = Voletile Organic Analysis
- WQCC = Weter Quality Control Commission

Table I = physical and biological parameters

Table II = inorganic parameters

Table III = metal parameters

Values in Tables I II and III for recreational uses cold water blots and domestic water supply are not included

- (2) In the absence of specific, numeric standards for non-naturally occurring organics the narrative standard is interpreted as zero with enforcement based on practical quantification levels (PQLs) as defined by CDH/WQCC or EPA
 - (3) All are 30-day standards except for nitrato-intrite

- (4) Anamonia, suifide, chloride, suifate copper, iron, manganese, and zinc are 30-day standards all others are 1-day standards

 (5) type abbreviations are A=mion B=bacteria C=cation T=indicator FP=field parameter M=metal P= peaticide PP=peaticide/PCB R=radionuclide SV=semi-volatile V=volatile

 (6) method abbreviations are CT=CLP-TAL NC=son-CLP CV=CLP-VOA CS=CLP-SEMI EP=EPA-PEST CP=CLP-PEST E=EPA, a = detected as total in CV

 b = detected as TICs in CS c = detected as TIC in CV d = not routinely monitored in discharge pends, f = mixture-individual isomers detected
 - (7) See Section 3 8 5 (2)(a) in (b)
- (8) Where standard is below (more stringent than) PQL (CDH), PQL is standard
 - (9) MDL for Radium 226 is 0 5 MDL for Radium 228 is 1 0
 - (10) See section 3 1 11 (f) (2) in (a)
- (a) CDH/WQCC Colorado Water Quality Standards 3 1 0 (5 CCR 1002-8) 1/15/1974 amended 10/17/1991 (ARAR)
 - (Envrionmental Reporter 726 1001-1020 6/1990)
- (b) CDH/WQCC Classifications and Numeric Standards for S Platte River Basin Laramie River Basin Republican River Basin

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	Segment 4 & 5 Stream Classification and Water Quality Standards (b)(4)	sification a	od Water Q	nelity Standards	(P)(4)	
						Table C		Stream So	Stream Segment Table	Table 2	
		1			Tables	Figh &	Table D	ଚ		Radiomuclides	clides
	į	<u> </u>		Method	¥ €	Water	Radio-	Acute	Chronic	Woman Walnut	Walnut
Parameter	<u>.</u>	Z E	CDH	6	Ξ_	Ingestion	nuclide	Value	Value	Creek Creek	Crock
Bicarbonate	<	10 000	Т	Fito i							
Carbonate		000 01		E310 I							
Chloride		2 000		E325				30,000	360 000		
Chlorine		000,1		E4500				20,000	220,000		
Fluoride	<	2 000		E340				•	1		
N as Nitrate	<	2 000		E353 1				9	200		
N as Nitrato+Nitrite	<	2 000		E353 1				30'01	200		
N as Nitrite	<	2 000		E354 1				8			
Sulfato		2 000	_	E375 4					200		
Sulfide	<								200 000		
Coliform (Fecal)	B	_		SM9221C							
Aramonia as N	υ	2 000		E350				620	5		
Dioxin	۵			70	0 00000022	0 000000013			0 000000013		
Califar											
Disabled Original	u f	80 80		E600				20	20		
The state of the s	2 (8 3		SM4500				2 000	2 000		
Sneeific Conductance	<u>.</u> 6	-		E130 I				6.5.9	6.5-9		
Temperature	£	•	-,.	1 07 1							
Boron		2 000		E6010				750	5	•	
Total Dissolved Solids	_	10 000		1 0913					3		
Aleminum	Σ_	200		1							
Antimony	Σ	8		כו			_				
	Z	01		t t				Ş			
	Σ							₹			
>	× :										
	Σ ;	. 20g		t							
begyinum	Σ	2	<u>-</u>	1							

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	Segment 4 & 5 Stream Classification and Water Quality Standards (b)(4)	sification a	nd Water Q	uality Standards	(b)(4)	
								Strong Seq	Stream Sogment Table	Table 2	
					Tables	Fish &	Table D	©		Radiomaclides	ides
		<u>Š</u>		Method	Y.B		Redio	Acute	Chronic	Woman Walnut	Walnut
	<u> </u>	MDL	SH		<u> </u>	Ingestion	nuclide	N	0 m m	Creek	Creek
Cadmin	2	v	1	Į				176	TVe		T
	<u> </u>	2 000		<u> </u>	,,,,,			2	2		
	Σ	1 000		NC							•
Chromium	Σ	2		כו							
Chromium III	Σ	S.		SW8467196				S			
Chromium VI	Σ	2		E218 5				TVS	TVS		
Cobalt	Σ	ક્ર		ರ							
Copper	Σ	22		ե				TVS	TVS		
Cyanide	Σ	2		t				~	2		
Iron	Σ	8		ל					300 (3)		
	∡	s		៦				TVS	TVS		
Lithium	Σ	8		NC							
Magnesium	Σ	2000		<u>চ</u>							
Manganese	Σ	15		<u>च</u>					50 (3)		
Mercury	Σ	0 2		ש					10 0		
Molybdenum	Σ	200		NC.							
Nickel	Σ	2		ַל				TVS	TVS		
Potessium	Σ_	2005		ಕ							•
Seleniem	Σ	S		ե				2			
Silver	Σ	2		<u></u> ច				TVS	TVS		
Sodium	Σ	2000		<u>៦</u>							
Strontien	×	200		SC SC							
Thefliem	Σ	2		<u>5</u>					-		
Tin	Σ	200		SC.							
Titanium	Σ	2		E6010							_
Tungsten	Σ	으		E6010							
Vanadium	Σ	S		<u>ნ</u>							
2 mc	Σ	8		t ₃				TVS	TVS		
2 4 5-TP Silvex			0.5	-0							
	_	_	<u>.</u>	<u>.</u>	<u>.</u>	_	_	_	_	_	-

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	Segment 4 & 5 Stream Classification and Water Quality Standards (b)(4)	sification as	od Weter Qu	sality Standards	(b)(4)	
					Tebles	Table C Fish &	Table D	Stram Sog	Stream Segment Table	Tuble 2 Redigmedidae	-
		<u>5</u>		Method	A.B	Wester	Radio		Chronic		Walnut
Purameter	. ତ	F	COH	<u> </u>	3	uonesitus	2007			¥	E
2 4-D	<u>a</u>		_	P	001						
Acrolein	<u>a.</u>		2								
Aldicarb	_	_	2		10						
Adrin	<u>.</u>	0 05	0	C	0 002 (6)	0 000074			0 000074		
Bromacil	<u>۵</u>				;						
Carbofunan	_			•	36						
Chloranii	_			E619							
Chlordene (Alpha)	<u>a</u>	0.5	_	G	0 03 (6)	0 00046			0 00046		
Chlordane (Gamma)	<u>a</u>	0.5	_	Ç	0 03 (6)	0 00046			0 00046		
Chlorpyrifos	۵.		0		,						
DDT	۰	-	0	ď	910	0 000024			0 000024		
DDT Metabolite (DDD)	<u>a</u>	0.	0	Đ	;						
DDT Metabolite (DDE)	۵.	<u>-</u>	-	c b							
Demeton	<u>a.</u>		-								_
Diazinon	<u>α.</u>										
Dieldrin	<u>a</u>	<u>-</u>	-0	0	0 000 (6)	0 000071			0 000071		
Endosuifun I	<u>a.</u>	0 05	0	චි							
Endosulfan II	۵	-	<u>.</u>	ð							
Endosulfan Sulfate	<u>a</u>	5	0	G							
Endrin	<u>م</u>	<u>-</u>	-	පි	0 2	,					
Endrin Aldehyde	Δ.		-								
Endrin Ketone	<u>~</u>	=		CB							_
Guthion	<u>م</u>		15								
Heptachlor	۵.	0 05	8	ರಿ	(9) 800 0	0 00028			0 00028		
Heptachlor Epoxide	<u>~</u>	0 05	0 05	G	0 004 (6)						
Hezachlorocyclohezane, Alpha	<u>a</u>	0 05	0 05	G		0 0092			0 0092		
Hexachlorocyclohexane Beta	<u>a</u>	0 03	0 05	c		0 0163			0 0163		
Hexachlorocyclohexane BHC	<u>a</u>	0 05	0 05								
Hexachlorocyclohexane Delta	۵.	0 05		G							
Hexachlorocyclohexane Tech	<u>a</u>		0 2	<u></u>		0 0123			0 0123		
								•	_	_	-

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (Rebruary 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

Political Poli						****						
Political Character							Table C		Stream So	gment Table	Tuble 2	
Type POL Method A.B Weter Radio- Actes Chronic						Tables	Fish &	Table D	ଚ		Radioms	clides
Cayloberane Lindens		Į.	<u> </u>		Wethod	₽ €	Water	Redio	Acade		Woman	Walnu
Ocycloherane Lindune P 0 05 CP 4 0 0166 0 01	Permeter	6	RFP	1	2	<u> </u>	an and an	Morrison				
100 100	Hexachlorocyclohexane Lindane	4	0 05	0 05	85	4	0 0186			0 0186		
100 100	Malathion	<u> </u>		0.2								
P 0.1 P 0.5	Methoxychlor	۵	0.5	0.5	ಕಿ	<u>8</u>						
P 0.5 1 CP 0.005 (6) 0.000079	Mires	<u>a</u>		0								
P 0.5 1 CP 0.00079 0.000	Parathion	<u>Α</u>					_					
P	PCBs	<u>~</u>	0.5	_	8	0 000 (9)	0.000079			0.00000		
1 5 CP 5 5 5 5 5 5 5 5 5	Simazine	<u>a</u>			v		4			4		
PP 05 CP	Тохартыя	<u>a.</u>		'n	Ĉ	'n						
PP 05 CP	Vaponite 2	Δ.										
PP 05 CP	Aroclor 1016	<u>&</u>	0.5		ð							
PP 05 CP	Aroclor 1221	£	0.5		Đ							
PP 05 CP CP CP 1 CP 1 CP 1 CP 1 CP 1 CP 20	Aroclor 1232	<u>&</u>	0.5		ಕಿ							
PP 05 OF CP 1 CP 1 CP 2 RR 001 RR 1 1 80 80 80 80 80 80 80 80 80 80 80 80 80 8	Aroclor 1242	2	0.5		<u>ප</u>							
PP 11 CP 30 005	Aroclor 1248	운	0.5		<u>8</u>							
PP 1 CP 30 005	Aroclor 1254	£			ච							
PP	Aroclor 1260	<u>&</u>	_		ð							
ж 001 ж 11 ж 12 ж 4 ж 6001 ж 6001 ж 65/10(7)	Atrazine	<u>a</u>			u		<u>e</u>			6		
RR 001 RR 1 1 80 80 80 80 80 80 80 80 80 80	Americiam (pCi/l)	æ									50 05	0 05
80 80 80 80 80 80 80 80 80 80 80 80 80 8	Americium 241 (pCi/l)	~	0 01					æ				
7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Cestum 134 (pCi/l)	~	_			8		2			2	8
7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Cesium 137 (pCi/l)	æ	_									
5 15 000 S/10(7) S 8 8 8 8	Gross Alpha (pCM)	æ	2			-	····				7	=
15 000 S/10(7) S S S S S S S S S S S S S S S S S S S	Gross Beta (pCi/l)	~	4								s	<u>6</u>
001	Mutonium (pCv/l)	<u>~</u>									0 05	0 05
0 5/1 0(7)	Natonium 238+239+240 (pCs/l)	æ	10 0					15				
50 50	Radium 226+228 (pCi/l)	~	0 2/1 0 (7)					s				
50 SO	Strontrum 89+90 (pCu/l)	æ	_									
	Strontium 90 (pCi/l)	<u>æ</u> .						••			50	80

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992)
STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	k 5 Stream Cla	effication a	Weter O	Segment 4 & 5 Stream Classification and Water Quality Standards (b)(4)	(6)(4)	
						Table C		Stream So	Stream Segment Table	Table 2	
					Tables	五十二	Table D	<u>ල</u>		Radiomedidos	lides
	8	<u>5</u> 3		Method	¥.8	Water	Redio	Acute	Chronic	Woman Walnut	Walnut
Peremeter	ଚ	EF.	COH		<u> </u>	Town Our			3		1
Tritlum (pCi/l)	æ						20 000			2005	905
Uranium 233+234 (pCi/l)	~										}
Uranium 235 (pCs/l)	~	90									
Uranium 238 (pCi/l)	~	90									
Uranium (Total) (pCi/l)	<u>~</u>						\$			S	9
1 2,4 5-Tetrachlorobenzene	SV		2	٠	2 (6)						
1 2 4-Trichlorobenzone	S	01		CS							
1 2-Dichlorobenzene (Ortho)	SV	10	_	S	620						
1 2-Dipheaythydrazine	SV			ء .	0 05 (6)						
1 3-Dichlorobenzene (Meta)	S	0	_	S	620						
1 4-Dichlorobenzene (Para)	SV	2	_	cs	75						
2 4,5-Trichlorophenol	SV	S		CS	700						
2 4 6-Trichlorophenoi	SV	2	જ	CS	20(6)	12			12		
2 4-Dichlorophenol	SV	2	S	CS	21 (6)						
2 4-Dimethylphenoi	SV	2	ક્ર	CS							
2 4-Dinitrophenol	SV	S	S	CS							
2 4-Dintrotoluene	sv	2	2	CS							
2 6-Dinstrotoluene	S	2	2	CS							
2-Chloronaphthalone	SV	2		S							
2-Chlorophenol	sv	2	8	ಬ							
2-Methylmaphthalene	SV	9		CS							
2-Methylphenol	SV	2		CS							•
2-Natroaniline	SV	ş		CS							_
2-Nitrophenol	SV	2		CS							
3 3-Dichlorobenzidine	SV	8	2	CS		0 01			0 01		
3-Nkroaniline	SV	S		ಬ							
4 6-Dinitro-2-methylphenol	SV	S	S	CS							
4-Bromophenyl Phenylether	SV	2		S							
4-Chloroanline	sv	2		CS							

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARS/TBCs (February 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

						Table C		Stream Seg	Stream Segment Table	Table 2	
						Fuch &	_	(3)		Radiomaclidos	Hidos
		2		Method	A.B.	Weter			Chronic	Woman Walnut	Walnu
	R.	MDC		<u></u>		Ingostion	nuclide		Value	Creek	<u>8</u>
Parameter	6	RFP	HOO								
4-Chlorophenyl Phenyl Ether	SV	<u>0</u>		S							
-Chloro-3-methylphenol	SV	2	8	S							
6-Methylphenol	SV	2		cs							
4-Nitroaniline	SV	S		S							
4-Nitrophenol	SV	S		cs							
Acenaphthene	SV	2	2	cs	~~~						
Authracene	SV	2	_	CS							
Benzidine	S.		2	•	0 0002 (6)	0 00012			0 00012		
Benzoic Acid	SV	S		S							
Benzo(a)enthracene	SV	2	2	cs							
Benzo(a)pyreae	S	2	2	ಬ							
Benzo(b)fluoranthene	S	2	<u>e</u>	క							
Benzo(g h i)perylene	S	9	으	S					_		
Benzo(k)fluoranthene	S	2	2	ខ							
Benzyl Alcohol	S	2		೮							
is(2-Chloroethoxy)methane	SV	2		S							
bis(2-Chloroethyl)cther	sv	<u>e</u>	으	CS	0 03 (6)	0 0000037			0 00000037		
ia(2-Chloroiaopropyl)ether	2	2	2	CS							
da(2-Ethylhexyl)phthalate	S	2	2	S							
Butadiene	SV										
Butyl Benzylphthalate	SV	2		S						_	
Chlorinated Ethers	SV										
Chlorinated Napthalenes	SV										
Chloroalkylethers	SV	2	_	S							
Chlorophenol	SV		S								
Chrysene	S	오	2	S							
Dibenzofuran	SV	2		CS							
Dibeaz(a h)anthracene	S.	2	2	cs							
Dichlorobenzenes	SV		_								
Dathankanidia	20	ç	2	٥		-			5		

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARARs/TBCs (February 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/I)

					Segment 4	Segment 4 et 3 Stream Classification and Water Quality Standards (D(4)	rificacion as	A Market	miky Standards	(\$	
					,	Table C		Stream Sog	Stream Sogment Table	Table 2	
					Tables	Fish &	Table D			Redioneclides	e p
	į	\$ \$ 10 10 10 10 10 10 10 10 10 10 10 10 10		Method (6)	# 6	Water	Radio	Acute	Chronic	Woman Walnut	Walnut
Persuector	ଚ	RFP	СОН	Ē	3	Topos Sun					<u> </u>
Diethyiphthalate	SV	<u>e</u>	2	CS							
Dimethylphthalate	SV	2	2	CS							
Di-n-butylphthalate	SV	9	2	S							
Di-n-octylphthalate	SV	2		S							
Ethylene Glycol	SV			7							
Fluoranthene	SV	2	9	CS							
Fluorene	SV	2	2	S			,				•
Formaldchyde	SV										
Haloethers	SV										
Hexachiorobenzene	SV	2	2	S	0 02 (6)	0 00072			0 00072		
Hexachlorobutadiene	SV	2	유	ಬ	4	0 45			0.45		
Hexachlorocyclopentadiene	SV	으	으	S	49						
Hexachlorochane	SV	2	2	S		19			61		
Hydrazine	SV										
Indeno(1 2,3-cd)pyrene	SV	으	으	ខ							
Isophorone	SV	<u>e</u>	2	S	1 050						
Naphthalene	S	으	2	S							
Narobenzene	S	<u> </u>	2	S	3 5 (6)						
Nitrophenois	SV										
Nitrosamines	SV										
Nitrosodibutylamine	SV		으	عـ		0 0064			1900 0		
Nitrosodiethylamme	SV		으	عـ		0 0008			9000 0		
Nitrosodimethylamine	SV		2	م		0 0014			0 0014		
Nitrosopyrrolidine	SV		2	ع		0 016			9100		
N-Nitrosodiphenylamine	25	2	으	CSP		49			49		
N-Nitroso-di-n-dipropylamine	SV	<u> </u>	9	CSP							
Pentachlorinated Ethanes	S			_م_							
Pentachlorobenzene	SV.		<u>e</u>	عـ	(9) 9						
Pentachlorophenol	SV.	<u>s</u>	S :	ខ	200						
remaine	<u>}</u>	2_	2	<u>s</u>	_	_				_	

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	Segment 4 & 5 Stream Classification and Water Quality Standards (b)(4)	ification en	d Water Qu	ality Standards	(b)(4)	
	<u></u>					Table C		Stream Soc	Stream Segment Table	Table 2	
					Tables	Fish &	Table D	ଚ		Radiomec	ides
		호		Method	A.8	Weter		8	e e	1	Walnut
Peremeter	6	REP.	CDH	(e) _	€	Ingestion	macingo	9 2	Veluc Veluc	# 25 25	B
Phenol	SV	2	જ	CS							T
te Esters	SV										
Polynuclear Aromatic Hydrocarbons	SV		9	_ھ_		0 0028			0 0028		·
Vinyl Chloride	SV	2	7	CV	2						
1.1 1-Trichioroethane	_>	~		CA	200						
1 1,2 2-Tetrachlorocthane	>	S	_	CV		0 17			0 17		
1 1,2-Trichloroethane	>	25	_	CV	28	090			090		
1 1-Dichloroethane	>	s		CV							
1,1-Dichloroethene	>	s	_	co	7						
1,2-Dichloroethane	>	s	_	CV	<u>8</u>						
1,2-Dichloroethene (cis)	>			•	۶						
1,2-Dichloroethene (total)	>_	S		C					-		
1 2-Dichloroethene (trans)	>_	S	_	.	۶						
1 2-Dichloropropane	>_	S	_	CV	0 26 (6)						
1,3-Dichloropropene (cis)	>	S	_	cv							
1,3-Dichloropropene (trans)	>	2	_	C							
2-Butanone	>_	2		C4							
2-Hexanone	>	<u> </u>		C v							
4-Methyl-2-pentanone	>_	2		CV							
Acetone	>	<u>e</u>		ડ							
Acrylonitrile	>		ĸ	v		0 058			0 058		
Benzene	>	S		C4	2						
Bromodichloromethane	>	×	_	<u>ر</u>							
Bromoform	>	×	_	CV							
Bromomethane	>	9	_	CV.							
Carbon Disuffide	>	2		C4							
Carbon Tetrachloride	>			C.	2		•				
Chlorinated Benzenes	>	으		CV/CS							
Chlorobenzene	>_	s	_	CV/CVS	300						

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TABLE A-4 POTENTIAL CHEMICAL-SPECIFIC ARAR&/TBCs (February 1, 1992) STREAM SEGMENT (CDH/WQCC) SURFACE WATER QUALITY STANDARDS (ug/l)

					Segment 4	t 5 Stroam Clas	elfication as	ad Water Qu	Segment 4 & 5 Stream Classification and Water (bullty Standards (b)(4)	(P)(4)	
						Table C		Stream Sog	Stream Segment Table	Table 2	
						Finh &		ଚ		Radiomechdes	Holes
		5		Method	A,B	Water	Radio	Acute	IJ	Women Walnut	Waler
	Type of	MDL		9		Ingestion	maclide			Crock	Crock
Parameter	ଚ	RFP	НСЭ								
Chloroethane	۸	10		ΛO							
Chloroform	>	2	_	CV	Tot THM	61 0			61 0		
					1001						
Chloromethane	>	2	_	CV							
Dibromochloromethane	>	5	-	cv							
Dichloroethenes	>		_								
Ethyl Benzene	>	2	_	CA CA	089						
Ethylene Dibromide	>_			-							
Ethylene Oxide	<u>></u>										
Halomethanes	>				<u>8</u>	61 0			0 19		
Methylene Chloride	>	S	_	CA CA							
Pyrone	>	01	2	೮							
Styrene	>	S		Ç ¢							
Tetrachloroethanes	>	s	_	رم		80			80		
Tetrachlorocthene	>	S	_	رد در	01						
Toluene	>	s	_	ر د	2 420						
Trichloroethanes	>	8	_	<u>ح</u>							
Trichloroethene	>	s	_	رج	2						
Vinyl Acetate	>	01		<u>₹</u>							
Xylenes (Total)	>	2		<u>ر</u>							

EXPLANATION OF TABLE

- = Total trihalomethanes chloroform bromoform bromodichloromethane dibromochloromethane
- = Contract Laboratory Program
 - = Colorado Department of Health
 - = dissolved
- = Environmental Protection Agency
- = Manimum Detection Limit for radionuclides (pCi/l) MDL

 - # picocuries per liter PCM RFP PCM
- = polychlorinated biphenyl = Practical Quantitation Level

 - = Rocky Flats Plant

 - = species specific SS TAL
- = Target Analyte List
- = Total Trihalomethanes THM
- = Table Value Standard (hardness dependent) see Table III in (a) = Tentatively Identified Compound 되 TVS
 - Ìn
 - = micrograms per liter
- = Water Quality Control Commission = Volatile Organic Analysis
- (1) In the absence of specific, numeric standards for non-naturally occurring organics the narrative standard is interpreted as zero with enforcement based on practical quantification levels (PQLs) as defined by CDH/WQCC or EPA
 - (2) Ammonia sulfide, chloride sulfate, copper, iron manganese, and zinc are 30-day standards all others are 1-day standards

- (3) Lowest value given dissolved or total recoverable
 (4) Segment S standards are goals
 (5) Includes Table 1 Additional Organic Chemical Standards (chronic only)
 (6) Standard is below (more stringent than) PQL, therefore PQL is standard
 (7) MDL for Radium 226 is 0 5 MDL for Radium 228 is 1 0
- (a) CDH/WQCC, Colorado Water Quality Standards 3 1 0 (5 CCR 1002-8) 1/15/1974 amended 9/30/1989 (ARAR)
- (Euvrionmental Reporter 726 1001-1020 6/1990)

 (b) CDH/WQCC Classifications and Numeric Standards for S Platte River Basin Larame River Basin Republican River Basin

APPENDIX B TECHNOLOGY DATA SUMMARIES FOR GROUNDWATER/SURFACE WATER TECHNOLOGIES REVIEWED IN THE ANNUAL REPORT

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ACTIVATED CARBON

Description

Granular Activated Carbon (GAC) adsorption is based on the attraction of organic molecules in solution to the surface of the activated carbon. The adsorption process is dependent on the strength of the molecular attraction between the carbon and the organic contaminant, the type and characteristics of the carbon, and the pH and temperature of the solution. Nonpolar organic compounds of low water solubility are most easily adsorbed (U.S. EPA 1986a)

GAC adsorption is one of the most frequently used techniques for treating aqueous streams contaminated with organics. The carbon is placed in columns that are operated until the effluent concentration reaches unacceptable levels. At this point the carbon has become saturated with the contaminants and must be regenerated for reuse. The carbon is generally regenerated thermally Pretreatment is typically required for removal of oil, grease, and suspended solids.

Applications

GAC adsorption is an effective process for removing a variety of organics from water. It has been successful for carbon tetrachloride, chloroform, DDT, benzene, acetone, methylene chloride, phenol, trichloroethylene, and xylene among others (U S EPA 1985). In general, GAC can reduce these contaminants from mg/L concentrations to low ug/L concentrations.

The Rocky Mountain Arsenal has used GAC adsorption extensively for treatment of groundwater (PMSO 1987a, 1987b) Contaminants removed include trichloroethylene, dibromochloropropane, disopropylmethyl phosphonate, dicyclopentadiene, and various pesticides such as dieldrin and aldrin

Advantages and Disadvantages

GAC adsorption is a well known and developed technique for removing organic contaminants from water. The adsorbability varies between different classes of organics, but most of them can be removed by this method. The major disadvantage of GAC adsorption is that it requires energy-intensive regeneration or disposal of the carbon, and large amounts of carbon are required for poorly adsorbable compounds, such as chlorinated volatile organics. Residuals include spent carbon, and/or waste streams from the regeneration process.

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ACTIVATED SLUDGE

Description

The activated sludge process uses microorganisms to remove organic contaminants from water. The microorganisms use the organics as a substrate for growth and as an energy source. Adequate nutrients, nitrogen, and phosphorus are required for microbial activity. As the microorganisms proliferate, they form a biomass which is referred to as the "activated sludge." This material is kept in close contact with the wastewater by air agitation, which also provides the oxygen needed to sustain the process. The biomass has the ability to adsorb particulate and dissolved metals and radionuclides.

The biologically treated wastewater is sent to a clarifier where the biomass is removed by settling. Some of this settled sludge is returned to the process. The remainder of the sludge must be dewatered and digested or disposed.

Applications

Most organic compounds can be biologically degraded by the appropriate microorganisms. Some compounds, such as large, complex chlorinated organics and some volatile chlorinated organics, are more easily degraded anaerobically than aerobically. High concentrations of organics or the presence of metals may be toxic to the organisms, and pretreatment may be required.

Advantages and Disadvantages

The major advantage of biodegradation is that it is a natural process that will generally reduce the toxicity of the contaminant. Disadvantages of biological reactors include generation of large amounts of sludge (especially in aerobic processes), possible formation of toxic by-products, and relatively low removal efficiencies that make additional treatment necessary. Emissions of volatile organics may also be a problem. It is also generally difficult to treat very low levels of organics. High or varying concentrations of organics or metals may have a toxic effect on the microorganisms.

References

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Nyer, Evan K 1985 Groundwater Treatment Von Nosfrand Reinhold Company, NY

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ADSORPTION

Description

Adsorption is a term commonly used to refer to both adsorption and absorption. Adsorption is the physical adhesion of molecules or particles to the surface of a solid adsorbent without chemical reaction. Absorption involves the transfer of the molecules or particles from one phase to the other so that they actually become a part of the other phase (medium). Absorption may be physical or chemical in nature.

A number of different adsorption processes exist for treatment of metals and radionuclide contaminants in water. These include activated alumina, a ferrite process, and other processes (U.S. EPA 1985, 1986a, Schweitzer 1979)

Activated Alumina
Activated alumina is a porous form of aluminum oxide with a large surface area
it will adsorb liquids, vapors, and gases
For removal of aqueous contaminants, activated alumina is
typically used in a column similar to that for ion exchange
It has proven to be successful in the
removal of arsenic and fluoride from groundwater (Rubel 1980, Frankel and Juergens 1980)
Adsorbed
species can be removed by flushing the column with a suitable chemical solution, generating a
concentrated side stream

Ferrite Process This process involves the introduction of ferrite particles into a waste stream. Inorganic contaminants present in the waste stream will sorb to the particles which are then removed by physical separation. The ferrite process also has the capability of being used in a column similar to ion exchange.

Applications

Activated alumina is used to remove small amounts of fluoride and arsenic from potable water and wastewater (Rubel 1980, Frankel and Juergens 1980) The fluoride adsorption process is pH dependent with optimal removal occurring at pH 5 Research indicates that selenium can also be removed using activated alumina (Yuan et al. 1983)

Advantages and Disadvantages

Adsorption of metals and radionuclides is a standard technique for removal and concentration of these contaminants. The major disadvantage to adsorption processes is that they produce a concentrated liquid side stream resulting from regeneration. If not regenerated, the sorbent must be disposed as a solid waste.

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AEROBIC BIOLOGICAL REACTOR

Description

The aerobic biological reactor is a biodegradation system used for destruction of organic compounds in aqueous media. The process uses a bioreactor packed with plastic media which acts as a support for a film of bacterial growth. The packing is completely submerged in the bioreactor. Air or oxygen is pumped into the bioreactor to maintain aerobic conditions. In addition to oxygen, it may be necessary to add nutrients to the bioreactor for some applications. The submerged aerobic fixed film reactor requires less space than an aeration basin. This is due to the greater surface area provided by the bacterial film, and to the higher oxygen loading provided to the microorganisms.

Applications

The process is applicable to aqueous media contaminated with organic constituents which are amenable to biodegradation. The submerged aerobic fixed film reactor has been shown to be effective for relatively low concentrations in the influent stream. This is an advantage over other bioreactors, such as rotating biological contractors or aeration basins, which are not effective for low concentrations of organic contaminants. It may be necessary to combine the process with treatment of the bioreactor effluent by granular activated carbon for adsorption of non-biodegradable organic constituents.

Submerged aerobic fixed film technology is not applicable to radionuclides or heavy metals. Some metals have a toxic effect on the bacterial growth and must be avoided. Certain halogenated organic compounds are not readily destroyed by strictly aerobic biodegradation and are not amenable to treatment by this technology.

Advantages and Disadvantages

The primary advantages of the aerobic biological reactor are applicability to a broad range of organic constituents, effectiveness for treatment of relatively low contaminant concentrations, and relatively low capital and operating costs

The technology is not effective for all organic contaminants, it may be necessary to combine the process with a treatment technology for the bioreactor effluent

References

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- Yare, Bruce S Winter 1991/92 Semivolatile Organic Decay Rates in Pilot-Scale Solid and Slurry Phase Bioreactors Remediation, V 2, No 7

ALTERNATING CURRENT ELECTROCOAGULATION

Description

In this technology, an alternating (A-C) current electrocoagulator imposes an electric field on stable suspensions and emulsions and rearranges surface charges, which in turn facilitates particle flocculation and separation. Production separation is accomplished in conventional gravity separation and/or decant vessels. After the product separation step, each phase (oil, water, solid) is removed for reuse, recycling, further treatment or disposal. The technology can be employed in conjunction with conventional water treatment systems, including those relying on metal precipitation, membrane separation technologies, mobile dewatering and incineration units, and soil extraction systems.

Applications

The A-C electrocoagulation technology can be applied to a variety of aqueous-based suspensions and emulsions typically generated from contaminated groundwater surface runoff, landfill leachate, truck wash, scrubber solutions, treated effluents, and extract solutions. The suspensions include solids such as inorganic and organic pigments, clays, metallic powders, metal ores, and natural colloidal mater. The emulsions include an array of organic solid and liquid contaminants, including petroleum-based by-products.

Advantages and Disadvantages

Liquid/liquid and solid/liquid phase separations are achieved without the use of expensive polyelectrolytes. Generally, the rate of separation is faster than with methods that employ chemical flocculants, and the solids are often more dense than those resulting from chemical treatment. The process is also free of the excess waste solids attributed to chemical aids.

References

Electrocoagulation Found Effective in Removing Metals from Slurries 1991, May 2 HAZTECH News V 6, no 9

Farrell, Clifton W Alternating Current Electrocoagulation for Superfund Site Remediation Remedial Action, Treatment and Disposal of Hazardous Waste EPA/600/9-91/002 April, 1991

AEROBIC REDUCTIVE DECHLORINATION

Description

Most of the environmental contamination by chlorinated organics is in the form of complex commercial mixtures containing numerous compounds with varying degrees of chlorination. Biodegradation of this large number of distinct compounds therefore requires broad enzymatic specificity. Additionally, chlorinated organic materials frequently resist microbial degradation. Although these complex chlorinated mixtures are difficult to degrade, the aerobic bacterial degradation of chlorinated organics has been demonstrated in the laboratory.

Applications

This process is applicable to soils, sediments, and aqueous streams contaminated with chlorinated solvents

Advantages and Disadvantages

This process would completely destroy the chlorinated organic compounds, converting them to cell material, carbon dioxide, and water

This process is currently in the early development stage, and more research is required to evaluate effectiveness, implementability, and economics

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ANAEROBIC BIOLOGICAL ACTIVATED CARBON PROCESS

Description

The anaerobic biological activated carbon (AnBAC) technology is being developed to treat wastes containing high concentrations of organics. The process uses a granular activated carbon bed operated under anaerobic conditions. The carbon serves to both adsorb and immobilize organic contaminants and support the microorganisms that feed on the contaminants. The process has been demonstrated at the bench scale and pilot scale for treating wastes containing high concentrations of phenol and formaldehyde.

Applications

This process is applicable to treating aqueous streams containing high concentrations of biodegradable organics

Advantages and Disadvantages

This technology destroys toxic organics, rendering them harmless to the environment. The process may offer an economic way to treat concentrated waste streams

The process is not commercially available and requires more study to assess effectiveness, implementability, and economics. Additional treatment would probably be required to meet stringent effluent quality criteria. This technology requires very long startup periods before the biological process begins to effectively degrade the contaminants.

- Goeddertz, John G, A Scott Weber, and Wei-Chi Ying May 1990 Startup and Operation of an Anaerobic Biological Activated Carbon (AnBAC) Process for Treatment of a High-Strength Multicomponent Inhibitory Wastewater Environmental Progress, V 9, no 2
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- Schroeder, AT Carbon-Assisted Anaerobic Treatment of Hazardous Leachates Remedial Action, Treatment and Disposal of Hazardous Waste EPA/600/9-91/002 April 1991

ANAEROBIC REDUCTIVE DECHLORINATION

Description

This is a biological treatment process that occurs in the absence of oxygen. The process was first observed to take place naturally in anaerobic environments such as river or lake sediments

The anaerobic dechlorination of Aroclor 1242 by microorganisms in Hudson River sediments has been demonstrated in the laboratory. Tests showed that the PCB mixture was dechlorinated so extensively that it was converted from 85% tri- and tetra-chlorinated products. The end result of this natural process is the conversion of the more highly chlorinated PCBs into compounds of low toxicity that can be further degraded aerobically.

Applications

The process is applicable to both in situ and conventional treatment of soils and sediments contaminated by PCBs. The process may also be applicable to aqueous streams

Advantages and Disadvantages

The process destroys the toxic PCB compounds However, the process is currently in the early stages of development, and minimal information on effectiveness, implementability, and economics is available

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- Wilson, JT, LE Leach, M Henson, and JN Jones 1986 In Situ Biorestoration as a Ground Water Remediation Technique Ground Water Monitoring Review, Fall 1986

AQUA DETOX (Low Vacuum Steam Stripping)

Description

This process simultaneously treats groundwater and soil contaminated with volatile organic compounds. The integrated system consists of two basic processes—a vacuum stripping tower that uses low pressure steam to treat contaminated groundwater, and a soil gas vapor extraction/reinjection (SVE) process to treat contaminated soil. The two processes form a closed loop system that provides simultaneous in situ remediation of contaminated groundwater and soil with no air emissions.

The SVE system uses a vacuum to treat a VOC-contaminated soil, inducing air flow through the soil to remove vapor phase VOCs with the extracted soil gas. Carbon beds then treat the soil gas to remove additional VOCs before reinjection into the ground. The vacuum stripping tower and SVE system share a granulated activated carbon (GAC) unit

A key component of the closed-loop system is a vent header unit. This unit collects the noncondensible gases extracted from the groundwater or air that may leak into the portion of the process operating below atmospheric pressure. The system condenses and treats the steam used to regenerate the carbon beds

By-products of the system include a free-phase product and treated water Occasional disposal of spent carbon will also be required

Applications

This technology removes VOCs, including chlorinated hydrocarbons, in groundwater and soil. Sites suitable for this technology include those with both contaminated groundwater and contaminated soil.

Advantages and Disadvantages

This technology may offer economic advantages when both soil and groundwater must be remediated. The process may produce a recyclable product that could offset some of the costs

Disadvantages relate primarily to system complexity and the need for highly trained operators

- CWPCA Bulletin Site Remediation Lockheed Aeronautical Systems Company Integrated Soil and Groundwater Treatment Winter 1992
- Lord, Arthur E Jr, Leonard J Sansone, and Robert M Koerner 1991 Vacuum-Assisted Steam Stripping to Remove Pollutants from Contaminated Soil A Laboratory Study Remedial Action Treatment and Disposal of Hazardous Waste EPA/600/9-91/002 April 1991
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- Stacy, Gregory L and Stephen C James 1991 The Superfund Innovative Technology Evaluation (SITE) Program Hazardous Materials Control, Jan /Feb 1991

BIODENITRIFICATION

Description

This is a biological process for removing nitrates from water. The process is accomplished anaerobically, with methanol added as a carbon source. The process can be carried out in plug-flow reactors, complete-mix reactors, and trickling filters.

Applications

This process is used to remove nitrates from aqueous wastes. It is frequently used as the second step of a two-stage process. In the first stage, termed the "nitrification" step, ammonia is converted aerobically into nitrate, which is then removed by biodenitrification.

Advantages and Disadvantages

The process offers an economic method for removing nitrates from water The process is sensitive of shock loadings and requires trained operators

- Eckenfelder, WW, Y Argaman, and E Miller 1989 Process Selection Criteria for the Biological Treatment of Industrial Wastewaters Environmental Progress, V 8, no 7 February 1989
- Givens, Silas W, Eric V Brown, Steven R Gelman, C P Leslie Grady, and Daniel A Skedsvold 1991 Biological Process Design and Pilot Testing for a Carbon Oxidation, Nitrification, and Denitrification System Environmental Progress, V 10, no 2 May 1991
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BIOSORPTION (BIOACCUMULATION)

Description

Biosorption (bioaccumulation) consists of both the accumulation of contaminants by bacteria, algae, and or plants, and the adsorption of contaminants to the cell wall. Several plant, bacteria, fungi, and algae species are effective at bioaccumulating/adsorbing metals. Of these, only plants are effective in soil matrices. Algasorb is an algae that has been immobilized in a silica gel polymer that acts much like an ion-exchange resin. The heavy metals will adsorb to the cell wall. In plants, the heavy metals are taken up through the root system.

Applications

This process is primarily applicable to groundwater and surface waters. It has been effective in removing heaving metals, and inorganics, including, but not limited to cadmium, silver, aluminum, chromium, cobalt, copper, gold, iron, lead, manganese, mercury, molybdenum, nickel, platinum, uranium, vanadium, zinc, and dissolved solids

Advantages and Disadvantages

This process may offer economic advantages over more conventional technologies. However, the technology is very new and much more information is required to assess its effectiveness and economics. The removed contaminants are transferred to a biomass that will require further treatment

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- Palmer, et al 1988 Metal/Cyanide Containing Wastes Treatment Technologies Noyes Data Corporation, Park Ridge, NJ
- Stacy, Gregory L and Stephen C James 1991 The Superfund Innovative Technology Evaluation (SITE) Program Hazardous Materials Control, Jan /Feb 1991
- U S EPA 1988 The Superfund Innovative Technology Evaluation Program Technology Profiles EPA/540/5-88/003 November 1988

CARBON DIOXIDE EXTRACTION

Description

In this process, carbon dioxide is used to remove organic constituents from water, soil, or sludge. The process is based on the fact that some organics are soluble in carbon dioxide when pressurized above its critical point. When the carbon dioxide and the waste are contacted, the contaminants of concern transfer from the waste matrix to the carbon dioxide. The carbon dioxide is then depressurized, and the waste and solvent are then separated. At this point, the waste matrix may be disposed or treated further, as appropriate. The carbon dioxide may be recompressed for reuse.

Applications

This process is applicable to a wide variety of constituents

Advantages and Disadvantages

The primary advantages of carbon dioxide extraction is its applicability to a wide range of contaminants

Costs of carbon dioxide extraction are higher than for adsorption or stripping methods. In most cases, extraction will be effective for a limited number of the constituents in the waste matrix, necessitating further treatment of the waste. Recovered contaminants will require treatment prior to disposal

Additionally, the system is fairly complex and requires highly trained operators

- Breton, M, et al 1988 Treatment Technologies for Solvent Containing Wastes Noyes Data Corporation, Park Ridge, NJ
- U S EPA 1988, September Technology Screening Guide for Treatment of CERCLA Soils and Sludges NTIS PB89-132674
- U S EPA 1988 The Superfund Innovative Technology Evaluation Program Technology Profiles EPA/540/5-88/003 November 1988

CATALYTIC OXIDATION

Description

Catalytic oxidation is used to destroy organic compounds in an aqueous medium. The catalyst lowers the activation energy of the oxidation reaction so that significant rates of destruction can be realized. An oxidizing chemical addition may be required.

Applications

Catalytic oxidation is potentially applicable to a wide range of organic compounds in water. The proper selection of catalyst and reaction temperature is critical.

Advantages and Disadvantages

Catalytic oxidation may produce complete destruction of dissolved organic compounds at low energy use and chemical use
The technology is still in the experimental stage of development

- Chemical Waste Management, Inc 1990 New Wastewater Treatment Technology for Hazardous Wastes Chemical Waste Management, Inc Geneva, IL
- Hagh, B F and D T Allen Catalytic Hydroprocessing of Chlorinated Organics Dept of Chemical Engineering, University of California, Los Angeles, CA
- Van der Vaart, D T, W M Vatvuk, and A H Wehe 1991, January Thermal Catalytic Incinerators for the Control of VOCs J Air Waste Management Association, V 41, no 1

COMETABOLISM BIOLOGICAL PROCESS

Description

This process involves the biological treatment of chlorinated organic compounds via cometabolism of the contaminant using methane or butane as the primary substrate. The hydrocarbon waste streams, which includes water or air, are remediated using a sand or soil bed containing bacteria capable of metabolizing the contaminants to water, carbon dioxide, and trace inorganic salts

Although chlorinated organic compounds are generally resistant to biodegradation, recent work has shown that bacteria that oxidize gaseous hydrocarbons such as methane or propane are also able to cometabolically oxidize trichloroethylene (TCE) and other low molecular weight halogenated compounds

Application

This process is applicable to aqueous streams containing low concentrations of chlorinated organics such as TCE and trichloroethane (TCA)

Advantages and Disadvantages

This process results in the destruction of the organic contaminants to form innocuous compounds

This process has been tested at bench scale only, and more information is required to determine potential effectiveness and costs. The process is very sensitive to influent contaminant concentration and may be difficult to control.

- Bradford, Michael L and Raj Krishnamoorthy 1991 Consider Bioremediation for Waste Site Cleanup Chemical Engineering Progress, February 1991
- Palumbo, A V, G W Strandberg, and W Eng 1990 Effects of Groundwater Chemistry on Cometabolism of Chlorinated Solvents by Methanotrophic Bacteria Oak Ridge National Lab, TN CONF-900402-15
- Wilson, JT, LE Leach, M Henson, and J Jones 1986 in Situ Biorestoration as a Ground Water Remediation Technique Ground Water Monitoring Review, Fall 1986

CONTACT STABILIZATION

Description

Contact stabilization is a form of the activated sludge where aeration is carried out in two phases. Two types of tanks are used. (1) the contact tank where contaminants are adsorbed and absorbed on the microbic masses, and (2) the stabilization tank where the microbial solids, which have been removed in a final settling tank, are partially stabilized by re-aeration before being recycled to the contact tank

Since most of the aeration is done on the relatively small volume of solids in the stabilization tank, the operating costs are reduced relative to conventional activated sludge processes. Additionally, smaller tank sizes are required, resulting in lower capital costs.

Applications

Applications are the same as for conventional activated sludge technology

Advantages and Disadvantages

Advantages and disadvantages are similar to activated sludge. However, this process may offer lower capital and operating costs in specific applications

References

Metcalf & Eddy, Inc Wastewater Engineering Collection, Treatment Disposal McGraw-Hill, Inc

Parker, Dr Homer W 1975 Wastewater Systems Engineering Prentice-Hall, Inc , Englewood Cliffs, NJ

EMULSION LIQUID MEMBRANE EXTRACTION

Description

Emulsion liquid membranes (ELMs) consist of emulsion globules that are mixed with a contaminant-containing waste stream. In a typical application, oil, which acts as the membrane medium, is mixed with a chemical extraction agent. The result is an emulsion in which the extraction agent is dispersed within oil globules. The oil acts as a membrane through which contaminants diffuse for subsequent reaction with the internal reagent. By mixing the oil/reagent emulsion with the waste stream, contaminants can be removed from the waste and concentrated in the emulsion globules. This process is sometimes referred to as double emulsion extraction because an emulsion is first made of oil and reagent, followed by emulsification of the oil and reagent globules with the waste stream.

The ELM system is potentially much more efficient than simple solvent/solvent extraction. If the internal phase is selected to react with the solute in the external phase, the driving force for solute removal is increased substantially. The extraction of uranium (VI) from weakly acidic aqueous solutions has been studied using emulsions containing benzylacetone or dibenzylmethane and tributylphosphate.

Applications

This technology is potentially applicable for extracting organics from aqueous waste streams. It can be used for treating wastewaters containing both high and low concentrations of contaminants

Advantages and Disadvantages

In addition to being less susceptible to problems with suspended solids, ELM treatment also requires much smaller quantities of chemical separating agents than do more conventional techniques. Besides the obvious savings in solvent costs due to reduced volumes, lowest capital expenditures are also possible because extraction vessels and pumping equipment can be smaller and fewer in number. Furthermore, solvent selection is much more flexible than with conventional extraction processes because a membrane-phase preference for the solute is not required. Consequently, solvents can be chosen based on factors like cost, availability, and physical properties, rather than partitioning performance.

This process has not been demonstrated in full-scale treatment applications. Therefore, an assessment of costs, implementability, and effectiveness cannot be made at this time

References

Two-Step Liquid Membrane Process Tested on Uranium, Other Contaminants in Ground Water 1991, May 2 HazTECH News V 6, no 9

ENZYMATIC MICROBIAL REDUCTION

Description

in this process, Fe (III)-reducing bacteria, GS-15 and Shewanella putrfaciens gain energy for growth by enzymatically coupling the oxidation of organic matter of H₂ to the reduction of U(VI) to U(IV). Since uranium is highly insoluble in its reduced state, microbial reduction can effectively remove dissolved uranium from surface waters and groundwaters.

Applications

Enzymatic microbial reduction is a potential means of removing dissolved uranium from contaminated water and waste streams. Other radionuclides, such as plutonium and technetium might also be removed in a similar manner.

Advantages and Disadvantages

Microbial reduction has been shown to oxidize organic contaminants such as U(VI)-reducing microorganisms which might be able to simultaneously convert the organic contaminants to carbon dioxide while precipitating the radioactive metal

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EXTENDED AERATION

Description

Extended aeration systems provide long-term aeration in a completely mixed activated sludge process. The system requires that microorganisms exist in the endogenous phase by maintaining a low food-to-microorganism ratio in the system. In the endogenous phase, the microorganisms are basically near starvation and are consuming each other. This results in the production of lower amounts of wasted sludge.

This process basically requires a steel or concrete tank fitted with air diffusers at the bottom. Systems are typically sized to provide approximately 24 hours of detention. The treated effluent then flows through a clarifier for removal of suspended solids. Additional treatment can be included as required to meet effluent criteria.

Applications

This process is used to process wastewaters containing high concentrations of biodegradable organics. Chlorinated hydrocarbons are not effectively biodegraded.

Advantages and Disadvantages

Advantages and disadvantages are the same as for conventional activated sludge However, extended aeration is better able to handle shock loadings or underloadings without detrimental effects on system performance

Additional treatment would likely be required to meet strict effluent quality requirements

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FREEZE CRYSTALLIZATION

Description

Freeze crystallization is a general separations process used to remove pure components from solutions by crystallizing the materials to be removed. This process has been used for applications as diverse as organic chemical refining and fruit juice concentration, and is also suited for treating hazardous wastes.

The basic operation involved is the production of crystals by removing heat from a solution. Crystals produced in this manner invariably have very high purities. Once small, uniform crystals have been produced, they must be washed to remove adhering brine. The brine is recycled to the crystallizer, so that as much solvent as desired can be recovered. The pure crystals are usually melted in a heat-pump cycle, which further improves the energy efficiency of the process.

When one or more of the solutes exceeds its solubility, additional crystal forms are produced, but they are formed separately from each other and from the solvent crystals. Since in most waste applications the solvent is water, and ice is always less dense than the solution and the solutes usually more dense, it is easy to separate these crystals by gravity.

Applications

The process works on aqueous streams containing heavy metals, all types of dissolved organics, and radioactive materials. This technology can also be used to process the liquid stream from soil washing operations.

The process is economically and technically competitive on very contaminated streams. For example, wastes with heavy metals require concentration of 1,000 to 10,000 mg/l to be economically recoverable with freezing

Advantages and Disadvantages

Freeze crystallization has several advantages for remediation and waste recovery applications. First, it is a very efficient volume reduction process, producing a concentrate that has no additional chemicals added to it - if disposal in a hazardous waste landfill, or incinerator destruction is required, this will reduce these costs substantially. When a large fraction of the solvent (usually water) is removed from a waste, the remaining impurities often begin to crystallize as well - they are often sufficiently pure to have by-product value for resale

The main disadvantage of this process is its relatively high cost for treating streams with low concentrations of contaminants. The process is also relatively complex, requiring numerous pieces of equipment, compressors, heat exchangers, and pumps

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GAMMA IRRADIATION

Description

This technology uses ionizing gamma radiation to decompose organic compounds. The media containing the organic constituents are exposed to a source of gamma radiation. The radiation excites the organic constituents to a higher energy state, which causes them to decompose. Gamma irradiation has been successfully applied to disinfection of sewage sludge. The process has been demonstrated to be effective for destruction of chlorinated hydrocarbons.

Applications

Gamma irradiation is applicable to disinfection of sewage sludge and destruction of organic constituents, particularly chlorinated hydrocarbons. Exposure of organic compounds to gamma radiation produces partially decomposed organic compounds as well as hydrogen, oxygen, and chlorine. Treatment of offgases produced by the technology would be required. It is possible that some of the partially decomposed organics may be more toxic than the original constituents.

Some organics are not amenable to treatment by gamma irradiation. Treatability testing would be required prior to application of the technology in the field. The process has no reported effect on heavy metals or radionuclides.

Advantages and Disadvantages

Gamma irradiation is a proven technology for disinfection of sewage sludge. The process has also been demonstrated to be effective for destruction of some organic constituents, particularly chlorinated hydrocarbons. The process seems well suited for application to sewage sludge contaminated with halogenated organics. The process may also be used for treatment of water or sludges contaminated with halogenated organics and which may foster unwanted biological activity. It is expected that bench testing should be available for this technology. The results of bench testing will probably be representative of the effectiveness of the process.

The process appears limited in the scope of its applicability. The gamma irradiation process produces off-gas which will require treatment. It is not clear what destruction efficiencies are achievable or what the costs of the process are

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HARDWICKIA BINATA BARK ADSORPTION

Description

Hardwickia binata bark was found to have good sorption capacity for mercury (II) Studies indicated that the sorption of Hg (II) increases as the pH increases and a contact time of two hours was found to be optimum

Applications

Hardwickia binata bark adsorption treats aqueous waste containing mercury (II)

Advantages and Disadvantages

The presence of light metal ions interferes with sorption of mercury

References

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HOLLOW-FIBER SUPPORTED LIQUID MEMBRANES

Description

This technology uses a liquid extractant supported on hollow polypropylene fibers to extract ionic radionuclides from water. The extractant is then regenerated by using an aqueous solution of a complexing agent. This results in the concentration of the radionuclides into a much smaller volume of liquid.

Applications

Laboratory tests on Hanford, Washington site groundwater demonstrated the removal of uranium using bis(2,4,4-trimethylpentyl)phosphonic acid contained in the commercial extractant Cyanex 272 as the extractant. The water-soluble complexing agent 1-hydroxyethane-1,1-diphosphoric acid was used as the stripping agent.

Advantages and Disadvantages

This technology has the potential for treating radionuclide-contaminated water to significantly reduce the volume of material

The technology has been demonstrated only on uranium under laboratory experiments

References

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IN SITU AIR STRIPPING

Description

This process uses horizontal air injection wells installed below the aquifer and extraction wells located either above or in the upper portion of the aquifer. In effect, an in situ diffused air stripping column is constructed. Air introduced at the bottom of the aquifer diffuses through the aquifer and is extracted at the top. While passing through the aquifer, the air strips and removes the volatile organics.

Applications

This process would be applicable to shallow aquifers containing volatile organic contaminants

Advantages and Disadvantages

This technology eliminates the need for an external air stripping tower. Additionally, the need for pumping the groundwater to the surface and disposing of the treated groundwater is eliminated.

The process produces a contaminated air stream that may require treatment. System costs are highly site-specific and the process may be difficult to control

References

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IN SITU BIOREMEDIATION OF GROUNDWATER

Description

In situ aerobic biological treatment of groundwater involves the stimulation of biological growth in the contaminated zone in order to reduce the contaminant concentrations. Microorganisms that can use some or all of the contaminants as substrate will normally exist in a contaminated environment. The microorganisms are stimulated to increase their biological growth and consumption of contaminants through addition of an oxygen source and essential nutrients and micronutrients. Anaerobic processes also exist.

The aerobic in situ treatment system generally consists of injection wells for injecting an oxygen source and required nutrients and extraction wells for monitoring and recovering by-products. The most common oxygen source is dilute hydrogen peroxide. Inocula of acclimatized bacteria may be added as needed. The treatment efficiency is measured in terms of contaminant reduction, dissolved oxygen, and bacterial growth.

In situ treatment may also be carried out as an anaerobic process. This requires that anaerobic conditions are established in the contaminated zone. The operation of such a system is essentially the same as for the aerobic, except that no oxygen addition is involved. The anaerobic and aerobic in situ processes may also be combined and operated in series.

Applications

In situ biodegradation has been used for various applications such as gasoline spills and wood-treating wastes containing semivolatile and nonvolatile organics (U S EPA 1986c, Litchfield 1986). While it was previously thought that trichloroethylene (TCE) was only anaerobically degradable, recent in situ studies have demonstrated that TCE can also be treated aerobically in situ (Roberts et al. 1989).

Even though most compounds can be biologically degraded, it should be noted that in situ treatment is dependent on other process-controlling factors such as geological and hydrological conditions

Advantages and Disadvantages

The major advantages of in situ biological treatment are

- Can be carried out in place
- No sidestreams generated
- Only environmentally safe compounds are added
- Relatively inexpensive operation

Disadvantages include

- Level of cleanup generally less than for aboveground treatment trains
- May be difficult to control
- Difficult to treat broad mixtures of compounds

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ION EXCHANGE

Description

Ion exchange can be used for the removal of undesirable anions and cations from a wastewater stream (Eckenfelder 1989) Cations are exchanged for hydrogen or sodium and anions for hydroxyl ions. Most ion-exchange resins used in wastewater treatment are synthetic resins made by the polymerization of organic compounds into a porous three-dimensional structure. Functional ionic groups are usually introduced by reacting the polymeric matrix with a chemical compound containing the desired group. Exchange capacity is determined then by the number of functional groups per unit mass of resin

Treatment of wastewater by ion exchange involves a sequence of operating steps. The wastewater is passed through the resin until the available exchange sites are filled and the contaminant appears in the effluent. At this point, the process is stopped and the bed is backwashed to remove dirt and to regenerate the resin

Applications

One of the major applications of ion exchange is the removal of chrome from industrial plating streams. Other anions or cations from wastewater streams can be removed. Macroreticular resins are used for the removal of specific organic compounds such as chlorinated pesticides and aromatic hydrocarbons. This technology has been used successfully for the remediation of heavy metals and uranium from wastewater and groundwater at the Hanford (Weiss 1990) and Savannah River Sites (Sferrazza 1990)

Advantages and Disadvantages

One of the advantages of ion exchange is that the removed product from the wastewater stream can be recovered and reused or concentrated for more controlled disposal

Other ions within a waste stream can compete with the ion of interest to remove in the exchange process thus reducing the capacity. For instance, iron in groundwater competes for the exchange of more hazardous ions like chromium or uranium.

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- Weiss, R L 1990 Westinghouse Hanford Company, personal communication May 8, 1990

OXIDATION/REDUCTION

Description

The chemical reduction-oxidation (redox) process involves a change of the oxidation state of the reactants, one is increased while that of the other reactant is reduced. Common oxidizing agents include ozone, hypochlorite, and chlorine. Common reducing agents include sodium borohydride, sulfur dioxide, and ferrous sulfamate (U.S. EPA 1985, 1986a).

The purpose of redox treatment of inorganic compounds (excluding heavy metals) in water is generally to break a compound into simpler, less toxic constituents. Examples are the conversion of sodium cyanide to carbon dioxide and nitrogen using alkaline chlorination and the conversion of ammonium to nitrogen and water using sodium nitrite (Marin et al. 1979).

The use of redox treatment of waste streams containing metals is typically required to enhance a subsequent precipitation step. The redox reaction is used to adjust the metal to an oxidation state that will result in the formation of an insoluble metal salt precipitate that can then be physically removed from the bulk of the aqueous waste stream

An example is the use of sulfur dioxide to reduce hexavalent chromium to trivalent chromium, which is then precipitated as chromous hydroxide. In general, the use of redox in conjunction with precipitation for the removal of heavy metals is a well established water treatment method.

Applications

A typical redox process for removal of cyanide involves conversion of cyanides to cyanates with a 15 percent solution of sodium hypochlorite at a pH >10 The cyanates are then further oxidized to N_2 and CO_2 with the sodium hypochlorite solution at pH 8.5 Complete oxidation takes approximately 10 minutes (Marin et al. 1979, EPA 1980). This type of process is common for treatment of electroplating rinse water.

Reduction of hexavalent chromium to its trivalent state followed by precipitation is a standard process step for treating chromium-bearing aqueous wastes. The solution pH is first adjusted to a pH of 2 to 3 by addition of hydrochloric or sulfuric acid. A reducing agent, typically sulfur dioxide or sodium metabisulfite, is then added. After the reaction is completed, the pH is adjusted to 7 5 to 8 5 using lime or caustic. At this pH, chromium hydroxide has its minimum solubility and precipitates (Lanouette 1977)

The use of redox reactions for the removal of trace quantities of uranium and transuranic elements from groundwater has not been demonstrated. Processes for recovery and purification of uranium and transuranic elements, however, rely heavily on adjustment of oxidation states. These processes include

precipitation as well as acid and solvent extraction. The separation of plutonium from cerium by extraction with tributyl phosphate (TBP) requires that the plutonium be oxidized to the tetravalent state without oxidation of cerium to its tetravalent state. Similarly, the separation of plutonium from uranium requires that the plutonium be trivalent and uranium hexavalent (Benedict et al. 1981). Process solutions typically contain transurance elements in concentrations orders of magnitude above those required to meet discharge limits.

The oxidation states and solubilities of uranium and transuranic elements at trace concentrations in groundwater have been studied by several researchers in recent years (Nitsche et al. 1988, Kim et al. 1988, Nash et al. 1988, Cleveland et al. 1985). In general, they found Pu(V) and Pu(VI) to be the oxidation states of the soluble plutonium species. Presumably, plutonium solubility could be reduced by reduction to Pu(III) or Pu(IV). The solubility is enhanced by the presence of carbonate and fluoride, which form complexes with the plutonium. Americium solubility is controlled mainly by the formation of radiocolloids.

Advantages and Disadvantages

The use of redox processes has the advantage that often inorganic contaminants may be transformed into less hazardous forms. The ability to adjust oxidation states of metals is advantageous and in some cases necessary for a subsequent treatment process, such as precipitation. A disadvantage of the use of chemical redox reactions is undesirable side reactions. These include the reduction or oxidation of organics and the production of chlorinated organics if the selected process is chlorination (Rice and Gomez-Taylor 1985). The process will also produce a sludge that requires further treatment or disposal

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- Versar, Inc 1986, September Mobile Treatment Technologies for Superfund Wastes Springfield, VA NTIS pp 4/2-4/6

Wagner, K, et al Remedial Action Technology for Waste Disposal Sites Second Edition Pollution Technology Review No 135 Noyes Data Corporation pp 489-493

POTASSIUM FERRATE PRECIPITATION (TRU CLEAR")

Description

This is a proprietary process being developed by Analytical Development Corporation The process is used for the removal of trace levels of alpha-emitting transuranic (TRU) elements from water

The technology is based on ferrate ion (FeO₄²) chemistry with TRU-removal accomplished by proprietary chemical additives into specific formulations for specific wastewaters. Ferrate chemistry has been studied for many years, but its commercial application has not occurred due to the inability to manufacture significant quantities of the material for large-scale use

The novel ferrate chemistry which is used by this technology operates via a degradation chemical reaction in which the strongly oxidizing ferrate ion reacts with water to form an insoluble hydrated ferric oxide, hydroxide ions, and oxygen gas

$$FeO_4^2 + 0.5 H_2O \rightarrow FeOOH + 2.0 OH + 0.75 O_2$$

The rate of this reaction is catalyzed by trace metal ions which may be present in solution. In the presence of organic or inorganic reducing agents, the rate of degradation and its stoichiometry can be influenced radically as well. The reaction mechanisms discovered to date during investigation of ferrate chemistry and application indicate a possible violation of equilibrium solubility behavior as it is understood today. The experimental results indicated that transuranic metal elements can be removed using this chemistry to lower concentrations in solution than can be predicated by equilibrium solubility constants which are empirically measured. It is believed that several mechanisms are operating simultaneously in the system which contribute to the overall removal characteristics of the technology, including localized, kinetically controlled reactions. These mechanisms are being investigated presently in conjunction with the engineering development of the technology. The precipitative removal of transuranic elements from wastewater to unprecedented low concentrations is the total effect of these mechanisms and is not predictable by standard analysis.

Applications

The process is used for removing uranium and transuranic elements such as plutonium and americium from wastewaters. The process uses conventional precipitation and clarification equipment

Advantages and Disadvantages

This technology may offer the ability to remove radionuclides to lower levels than achievable with conventional precipitation processes. It is also reported to produce much less sludge than conventional processes.

The primary disadvantage is that the process is based on a proprietary chemical, which would have to be purchased from a single supplier

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POWDERED ACTIVATED CARBON

Description

The powdered activated carbon treatment (PACT) process incorporates biodegradation and physical adsorption to remove organic constituents from an aqueous stream. The reaction is carried out in an aeration basin. Powdered activated carbon added to the aeration basin adsorbs organics from the wastewater stream and acts as a substrate for microorganism growth. Non-biodegradable components remain adsorbed on the powdered activated carbon. A clarifier is used to separate treated water from spent powdered activated carbon and biomass. The powdered carbon is regulated until its adsorptive capacity is reached after which it is either regenerated or disposed of

Applications

The process is applicable to aqueous streams with organic constituents concentrations ranging from 50 to 4,000 mg/l for large systems and up to 10,000 or 15,000 mg/l for small systems. Most organic constituents will be amenable to either biotreatment or adsorption onto the powdered activated carbon PACT has been shown to reduce chemical oxygen demand by 93 5% and biochemical oxygen demand by 99 5%. Bench testing will be required to determine whether similar reduction efficiencies can be achieved for specific applications.

PACT is not applicable to treatment of heavy metals or radionuclides. While PACT is not directly applicable to contaminated soils, it may be possible to combine the process with soil washing or similar technologies.

Advantages and Disadvantages

The primary advantage of PACT is its applicability to a broad variety of organic constituents. It is commercially proven technology and is readily available. Vendor equipment is available for on-site regeneration of the powdered activated carbon. Bench testing is expected to be readily obtainable.

One potential disadvantage of PACT is that it may not remove some organic constituents to the degree necessary to achieve ARARs

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PURE OXYGEN ACTIVATED SLUDGE

Description

This technology represents a modification of conventional activated sludge treatment in which pure oxygen is used instead of air. This requires the use of special equipment for extracting oxygen from ambient air. This technology offers potential advantages in performance and economics, which must be evaluated on a case-by-case basis.

Applications

This process is applicable to wastewaters containing high concentrations of biodegradable organics. However, chlorinated organics are not effectively treated.

Advantages and Disadvantages

Advantages and disadvantages are basically the same as for conventional activated sludge Additional treatment would still be required to achieve low levels of organics in the treated effluent

References

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SOLAR

Description

A system that uses solar energy to destroy hazardous organic wastes is being developed by VEDA Inc of Alexandria, Virginia The heart of this system is an array of sun-tracking mirrors as heliostats, referred to as a unified heliostat array Each heliostat concentrates and reflects the sun's radiant energy to a windowed reactor vessel. The heat and UV radiation provided by the unified heliostat array are used to destroy the organic contaminants.

A system for processing PCB or dioxin contaminated soil includes a desorption reactor, which heats the soil to 750°F. The high temperature vaporizes the organic contaminants from the soil. The heat for the desorption reactor is provided by cooling air from the windowed reactor.

The vaporized contaminants from the desorption reactor are injected into the windowed reactor where they are irradiated through a quartz window with concentrated solar energy from the unified heliostat array. The reactor temperature is maintained at 1,300°F (700°C) and is controlled by air flow around the reactor's ceramic liner. Inside the windowed reactor, organic compounds are decomposed by the high temperature and UV radiation. Some of the resulting exhaust gas is recirculated through the desorption reactor to provide additional heat needed to raise the temperature of the contaminated soil. The remainder of the exhaust gas is treated in a scrubber to remove hydrogen chloride, sulfur dioxide, and particulates before it is discharged to the atmosphere.

Applications

This process is applicable to soils and sediments that are contaminated with volatile and semivolatile organics. The process may also be applied to aqueous streams

Advantages and Disadvantages

The process offers high destruction efficiencies for organic contaminants Efficiencies as high as 99 9999% have been achieved

The system is not commercially available. However, a prototype system designed to process 500 pounds of contaminated soil per hour is being developed. Additional research is in progress to determine the temperature and condition necessary to volatilize and desorb PCBs and dioxins from soil

References

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SOLAR PHOTOCATALYTIC

Description

This is a proprietary process developed by Sandia National Laboratories and the Solar Energy Research Institute It provides solar-driven detoxification of contaminants using titanium dioxide as a catalyst

Applications

The process is used to destroy organics in contaminated groundwater and surface water Experiments have successfully demonstrated its effectiveness on trichloroethylene (TCE)

Advantages and Disadvantages

This process, when fully developed, may offer significant economic advantages due to its low power requirements

This process, however, is still in the developmental stage and more information is needed to evaluate effectiveness and economics for specific applications

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DOE Supports Effort to Develop Solar Process to Detoxify Organics 1991, May 2 HazTECH News V 6, no 9

SOLVENT EXTRACTION

Description

Solvent extraction is used to remove organic constituents and some heavy metals from water, soil, or sludge. A solvent is chosen in which the contaminants of concern are soluble. The chosen solvent and the matrix to be treated are mutually insoluble. When the solvent and the waste are contacted, the contaminants of concern transfer from the waste matrix to the solvent. The waste and solvent are then separated. At this point, the waste matrix may be disposed or treated further, as appropriate. The solvent may be regenerated for reuse.

Applications

Solvent extraction is applicable to a wide variety of constituents. However, most solvents will be effective for particular types of constituents and will not be effective for other types. In addition, it is possible that some constituents may not be amenable to solvent extraction. Each system must be tested to select appropriate solvents.

Solvents containing extracted constituents should be regenerated, if possible, to allow economical treatment. This process does not destroy the extracted constituents. Further treatment of extracted constituents may be required prior to ultimate disposal.

The process is not applicable to constituents which may not be removed from the solvent during regeneration. Matrix conditions, such as pH, or the presence of surfactants or emulsifiers, may alter the effectiveness of the process.

Advantages and Disadvantages

The primary advantages of solvent extraction are its applicability to a wide range of contaminants and the widespread use of solvent extraction in industrial applications. Solvent extraction may be readily bench tested

Costs of solvent extraction are higher than for absorption or stripping methods. In most cases, solvent extraction will be effective for a limited number of the constituents in the waste matrix, necessitating further treatment of the waste. Recovered contaminants will require treatment prior to disposal

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STEAM STRIPPING

Description

Steam stripping involves injection of steam into a solution to volatilize the organic compounds in the solution. It can be operated as a batch or continuous process

The batch process involves a batch still, an overhead vapor line, a condenser, a condensate receiver, and a gravity separator. Steam, injected through a perforated pipe in the still, provides the heat for vaporization of the waste. Vapor is condensed and collected as a liquid in the condensate receiver Liquids with similar boiling points and different densities may be separated by gravity separation in the condensate receiver (U.S. EPA, 1987c)

In continuous steam stripping, waste flows down the column while steam flows up as in air stripping. The column is designed to promote transfer of contaminants to the gas phase by causing effective heat transfer to the waste, by creating turbulence in the waste, and by providing a large waste surface area. Different liquid-vapor equilibria exist at various heights in the column, with the highest relative concentration of the most volatile component being on the top (Blaney, 1986), however, all volatiles are swept out together in steam stripping

Applications

Steam stripping is able to strip compounds with lower volatility than those removed by air stripping. The technology is reported to be effective for removal of high concentrations of organics, ranging from 1 to 20 percent (U S EPA, 1986a). Volatile organics, as well as semi-volatiles such as phenols, ketones, and phthalates, are good candidates for removal by steam stripping. Steam stripping is currently used at some commercial and industrial facilities to treat RCRA-spent solvent wastewaters (Turner, 1989). Hydrogen sulfide and ammonia can also be removed by this process (U S EPA, 1987c). Steam stripping is reported to be capable of removing over 99 percent of ammonia in high strength industrial wastes (Wickramanayake et al., 1989).

Advantages and Disadvantages

Steam stripping is a well demonstrated technology and commonly used in industry. As compared to air stripping, it may be used to treat less volatile compounds. However, the process generates a concentrate that requires treatment or disposal if recycling of the concentrate is not an option. This process is also expensive to operate, and is cost effective only when a source of waste heat or low cost fuel for producing steam is available.

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SUBMERGED AEROBIC FIXED FILM REACTOR

Description

The submerged aerobic fixed film reactor is a biodegradation system used for destruction of organic compounds in aqueous media. The process uses a bioreactor packed with plastic media which acts as a support for a film of bacterial growth. The packing is completely submerged in the bioreactor. Air or oxygen is pumped into the bioreactor to maintain aerobic conditions. In addition to oxygen, it may be necessary to add nutrients to the bioreactor for some applications. The submerged aerobic fixed film reactor requires less space than an aeration basin. This is due to the greater surface area provided by the bacterial film, and to the higher oxygen loading provided to the microorganisms.

Applications

The process is applicable to aqueous media contaminated with organic constituents which are amenable to biodegradation. The submerged aerobic fixed film reactor has been shown to be effective for relatively low concentrations in the influent stream. This is an advantage over other bioreactors, such as rotating biological contractors or aeration basins, which are not effective for low concentrations of organic contaminants. It may be necessary to combine the process with treatment of the bioreactor effluent by granular activated carbon for adsorption of non-biodegradable organic constituents.

Submerged aerobic fixed film technology is not applicable to radionuclides or heavy metals. Some metals have a toxic effect on the bacterial growth and must be avoided. Certain halogenated organic compounds are not readily destroyed by strictly aerobic biodegradation and are not amenable to treatment by this technology.

Advantages and Disadvantages

The primary advantages of the submerged aerobic fixed film reactor are applicability to a broad range of organic constituents, effectiveness for treatment of relatively low contaminant concentrations, and relatively low capital and operating costs

The technology is not effective for all organic contaminants, it may be necessary to combine the process with a treatment technology for the bioreactor effluent

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SUPERCRITICAL WATER OXIDATION

Description

Supercritical water oxidation uses oxygen dissolved in water above its critical point to oxidize organic compounds. Oxygen, from ambient air or from an oxygen source, is added to the water containing the organics to be treated. The water temperature and pressure are then raised above the critical point and rapid oxidation takes place. The heat released during oxidation is often sufficient to sustain the reaction if the heat release is not sufficient, energy in the form of supplemental heat or organic compounds may be added to the water. Salts formed in the oxidation process generally precipitate out of solution. After the treated water is cooled and the pressure is released, off-gases are released which may require treatment.

Applications

Supercritical water oxidation may be used to treat a variety of organic constituents, though it is less effective for halogenated compounds. Some work has been done with catalysts for treatment of halogenated compounds, however, the technology remains unproven for catalytic applications. The organics are partially oxidized to organic acids or completely oxidized to carbon dioxide and water Sulfur-containing compounds are oxidized to sulfate salts. Nitrogen-containing compounds are reduced to elemental nitrogen. Oxidation temperatures are not sufficient for generation of nitrogen oxides (NO_x)

For many compounds, oxidation is not complete. Organic and/or fatty acids will remain as by-products of the oxidation process. In most cases, it would be expected that the toxicity of the organic compounds will decrease. Aromatic compounds are less easily oxidized by the supercritical water oxidation process.

The technology is not applicable to or economically feasible for treatment of water containing organic compounds in low part per million concentrations. The process is not applicable to radionuclides or heavy metals

Advantages and Disadvantages

The primary advantage of supercritical water oxidation is that a variety of toxic organic constituents may be destroyed by low-temperature oxidation. Acid gases are easily controlled. The technology is proven at the commercial scale and equipment is readily available. Treatability testing may be conducted at the bench scale.

The primary disadvantages of supercritical water oxidation are that the technology does not effectively treat some organic constituents and it has high initial and operating costs. Some organic compounds

are not completely oxidized, partially oxidized compounds may be more toxic than the original compounds in some cases. The technology may not provide for sufficient removal of some compounds which may be present in low concentrations. The requirements to prevent corrosion of the system and pluging and plating out of metals is a also disadvantage. The system operates under high pressure which is a potential safety concern.

References

U S EPA 1988, September Technology Screening Guide for Treatment of CERCLA Soils and Sludges NTIS, PB89-132674

ULTRAFILTRATION

Description

This process uses special membrane material in equipment very similar to that used for reverse osmosis. The membrane material used has a much larger pore size than reverse osmosis membranes. Operating pressures are much lower, typically 50 to 100 psi versus 400 psi for reverse osmosis.

The most recent technology is based on a cross-flow element design. In this process, the influent, or feed stream is separated into two effluent streams—the "permeate" or clean stream, and the "concentrate" which retains all of the suspended solids rejected by the membrane. Only the permeate actually passes through the membrane. The feed and concentrate streams flow parallel to the membrane surface, resulting in the term "cross-flow". In this type of element, the solids are swept away with the concentrate, eliminating or greatly reducing the potential for the element to plug.

Applications

The process is applicable to wastewaters that contain contaminants in particulate form. For example, plutonium is often present as particulates that can be removed by this process.

Dissolved metals and radionuclides can also be removed by this process if they are first precipitated in a pretreatment process step

Advantages and Disadvantages

This process offers the advantage of improved removal efficiencies over conventional filtration. The process is easily automated, and pre-engineered package systems are readily available.

The primary disadvantage is relatively higher costs over conventional filtration

References

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U S EPA 1988 The Superfund Innovative Technology Evaluation Program Technology Profiles EPA/540/5-88/003 November 1988

UV/CHEMICAL OXIDATION OF ORGANICS

Description

Chemical oxidation is used to degrade hazardous organic materials to less toxic compounds. A number of different chemical oxidation processes exist for treatment of organic contaminants. These include chlorination, ozonation, and treatment by a combination of UV radiation, and ozone, and/or hydrogen peroxide (U. S. EPA 1985, 1986a, Wentz 1989)

Chlorination In this process chlorine is added to water to oxidize both organics and inorganics Chlorine, which is added in its elemental form (gas), chlorine dioxide gas, or hypochlorite salt, is a strong oxidizing agent in aqueous solutions. The primary use of chlorination has been for disinfection of drinking water. A potential disadvantage of this process is that the chlorine may form potentially toxic chlorinated by-products.

Ozone is a strong chemical oxidant that has been used for purification, disinfection, and odor control of drinking water. Ozone is generated from air or oxygen and is applied by bubbling the gas through the water being treated. Ozone efficiently breaks down some easily oxidizable organics, but has generally been shown to be an ineffective oxidant for halogenated organics at reaction times and concentrations normally used in drinking water treatment. Complete oxidation of organic species to carbon dioxide and water may require high ozone dosage and long contact times. If inorganics, such as iron, are present, their oxidation may inhibit the destruction of organics.

UV/Ozone/Hydrogen Peroxide The use of ultraviolet (UV) radiation in combination with ozonation has been found to catalyze the oxidation process and is now in common use. This form of treatment is accomplished by contacting the ozone and the contaminated water in a closed reactor in the presence of UV light. The combination of UV and ozone treatment makes it possible to oxidize compounds that would not be oxidized by ozone treatment only. UV radiation causes destruction or weakening of the chemical bonds in the organic compounds, thereby acting as a catalyst for the oxidation process. Hydrogen peroxide can be used in combination with UV light as an alternative to ozone, or all three may be combined.

Complete oxidation of organics results in the formation of carbon dioxide and water. In waste treatment, complete oxidation of all the contaminants is difficult and expensive to achieve, so a variety of low molecular weight organics are formed in the process. Since various degrees of oxidation occur in complex mixtures, it is important that the system be designed for removal of selected target contaminants. A thorough characterization of by-products is necessary

Applications

Chemical oxidation processes have been reported for dilute waste streams containing aldehyde, mercaptans, phenols, benzidine, unsaturated acids, and some pesticides (Kiang and Metry 1982)

The UV/Ozone/Peroxide system as marketed by ULTROX International has been used for pilot-scale and full-scale treatment of a variety of organic contaminants (Fletcher 1987, Barich 1990). In a pilot-scale test, the system was found to reduce trichloroethylene (TCE) from 200 ug/L to 2 6 ug/L and carbon tetrachloride from 10 ug/L to 2 9 ug/L. The ULTROX system has been used full-scale for treating 200,000 gallons of tetrahydrofuran-contaminated groundwater. The contaminant concentrations were reduced from 5,000 ug/L to nondetectable levels. Groundwater contaminated with TCE, tetrachloroethylene (PCE), and 1,1,1-trichloroethane at 470, 96, and 166 ug/L, respectively, was treated to below drinking water standards in pilot studies. Pilot studies were also conducted and demonstrated the reduction of polychlorinated biphenyl (PCB) concentrations from 50 ug/L to less than 1 ug/L.

Similar systems are manufactured by Solarchem (Ontario, Canada) and Peroxidation Systems, Inc (Gardenia, California)

Advantages and Disadvantages

Chemical oxidation of organic contaminants has the advantage that the contaminants are destroyed in the process. On a cost basis, UV/ozone/peroxide treatment is competitive with GAC treatment. Natural organics and inorganics may interfere with the oxidation process and increase the oxidant requirements. Undesirable organic by-products may also be formed.

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Advantages and Disadvantages

A primary advantage of this process is that it destroys the applicable contaminants rendering them harmless to the environment. It is effective on a wide range of contaminants and may offer economic advantages in specific cases

The process is complex and requires high operating temperatures and pressures Expensive equipment is required, as well as highly trained operators

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APPENDIX C TECHNOLOGY DATA SUMMARIES FOR SOIL/SEDIMENT TECHNOLOGIES REVIEWED IN THE ANNUAL REPORT

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AEROBIC BIOLOGICAL REACTOR

Description

The aerobic biological reactor is a biodegradation system used for destruction of organic compounds in an aqueous media. The process uses a bioreactor packed with plastic media which acts as a support for a film of bacterial growth. The packing is completely submerged in the bioreactor. Air or oxygen is pumped into the bioreactor to maintain aerobic conditions. In addition to oxygen, it may be necessary to add nutrients to the bioreactor for some applications. The submerged aerobic fixed film reactor requires less space than an aeration basin. This is due to the greater surface area provided by the bacterial film, and to the higher oxygen loading provided to the microorganisms.

Applications

The process is applicable to aqueous media contaminated with organic constituents which are amenable to biodegradation. The submerged aerobic fixed film reactor has been shown to be effective for relatively low concentrations in the influent stream. This is an advantage over other bioreactors, such as rotating biological contractors or aeration basins, which are not effective for low concentrations of organic contaminants. It may be necessary to combine the process with treatment of the bioreactor effluent by granular activated carbon for adsorption of non-biodegradable organic constituents.

Submerged aerobic fixed film technology is not applicable to radionuclides or heavy metals. Some metals have a toxic effect on the bacterial growth and must be avoided. Certain halogenated organic compounds are not readily destroyed by strictly aerobic biodegradation and are not amenable to treatment by this technology.

Advantages and Disadvantages

The primary advantages of the aerobic biological reactor are applicability to a broad range of organic constituents, effectiveness for treatment of relatively low contaminant concentrations, and relatively low capital and operating costs

The technology is not effective for all organic contaminants, it may be necessary to combine the process with a treatment technology for the bioreactor effluent

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ANAEROBIC REDUCTIVE DECHLORINATION

Description

Most of the environmental contamination by chlorinated organics is in the form of complex commercial mixtures containing numerous compounds with varying degrees of chlorination. Biodegradation of this large number of distinct compounds therefore requires broad enzymatic specificity. Additionally, chlorinated organic materials frequently resist microbial degradation. Although these complex chlorinated mixtures are difficult to degrade, the aerobic bacterial degradation of chlorinated organics has been demonstrated in the laboratory.

Applications

This process is applicable to soils, sediments, and aqueous streams contaminated with chlorinated solvents

Advantages and Disadvantages

This process would completely destroy the chlorinated organic compounds, converting them to cell material, carbon dioxide, and water

This process is currently in the early development stage, and more research is required to evaluate effectiveness, implementability, and economics

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ANAEROBIC BIOLOGICAL ACTIVATED CARBON PROCESS

Description

The anaerobic biological activated carbon (AnBAC) technology is being developed to treat wastes containing high concentrations of organics. The process uses a granular activated carbon bed operated under anaerobic conditions. The carbon serves to both adsorb and immobilize organic contaminants and support the microorganisms that feed on the contaminants. The process has been demonstrated at the bench scale and pilot scale for treating wastes containing high concentrations of phenol and formaldehyde.

Applications

This process is applicable to treating aqueous streams containing high concentrations of biodegradable organics

Advantages and Disadvantages

This technology destroys toxic organics, rendering them harmless to the environment. The process may offer an economic way to treat concentrated waste streams

The process is not commercially available and requires more study to assess effectiveness, implementability, and economics. Additional treatment would probably be required to meet stringent effluent quality criteria. This technology requires long startup periods before the biological process begins to effectively degrade the contaminants.

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BEST®PROCESS

Description

Resources Conservation Company's Basic Extractive Sludge Treatment (B E S T ®) process technology was invented during the 1960s by Boeing Company to process waste generated during the manned space flights. Since then, Resource Conservation Company (RCC) of Bellevue, Washington, owner of the B E S T ® patents, has developed the process from laboratory-scale testing through prototype full-scale operation. The process has been tested on municipal wastewater sludge, petroleum refinery wastes, PCB-contaminated soils and sediments, and oily hazardous wastes at regulated sites.

The process is configured to exploit the unique solvent properties of triethylamine (TEA). Triethylamine easily breaks the oil/water emulsions that cause major problems in some separation processes. At or below 20 °C, TEA is completely miscible. This "inverse miscibility" property is used by letting the oil and water components of a waste combined with the TEA to form a homogeneous, single-phase extraction mixture of oil/water/TEA. When oil/water emulsion is broken, bonded water is liberated and the bound particulates are released from the solution. The extraction efficiency of the system is enhanced because the amine solvent is able to achieve close contact with all components of the waste.

Before the extraction process is begun, feed material must be screened and pH adjusted to an alkaline condition. The feed is then introduced into a mixing tank and combined with TEA chilled to temperatures below the miscibility point (<20°C). At that temperature, a single liquid phase is formed and the solid material settles out. The mixture is agitate until equilibrium is reached, then the solids are removed from the solution either by filtration or centrifugation. Multiple extraction stages may be required to achieve contamination removal target levels.

The liquid fraction, a single-phase oil/water/TEA mixture, is heated to a temperature of 20°C and two distinct phases form an aqueous phase, and an organic phase made up of oil and TEA. The phases are separated by decantation into an oil/TEA phase and heavier water phase. The oil/TEA phase contains virtually all the oily material an organic contaminants. The TEA is recovered from the oil/TEA fraction by flash evaporation and steam stripping. Residual TEA is removed from the water layer by steam stripping. Recovered TEA is chilled and recycled for use in the process system.

The separated solids are returned to the feed tank for additional extraction with TEA. When extraction has been completed, solids are centrifuged or filtered and then dried to remove residual TEA and water

Oil, water, and solids are produced by the process Ideally, the product water can be conveyed to a water treatment facility for minimal treatment and discharged to the environment. The oil fraction may be reused as fuel, recycled, or destroyed if the organic contaminant levels in the oil are too high. The solids fraction may be returned to the site or sent to a disposal facility.

Applications

The B E S T® process can be used to treat soils and sediments contaminated by a wide range of organic compounds, including PCBs

Advantages and Disadvantages

The process can achieve removal efficiencies that exceed 98 percent for organic compounds. However, the process is complex and its capital and operating costs could be high

Processed material sizing requirements may limit processing applications or add significantly to processing costs since oversized material requires pretreatment

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CF SYSTEMS ORGANIC EXTRACTION

Description

CF Systems Corporation has developed a solvent extraction process that uses critical fluids and liquified gases such as carbon dioxide, propane, or other light hydrocarbons at high pressure to separate and recover oils from refinery sludges and to extract hazardous organic compounds from wastewater, sludge, sediment, and soil The process typically uses propane on contaminated soil and sludge and carbon dioxide to treat wastewater. These solvents provide high extraction efficiencies, evaporate readily from extracted organic material, and have high solubilities for most organic priority pollutants. They are inexpensive, readily available, nontoxic, and easily separated and retrieved from the process products.

The extraction process consists of four basic unit operations—solvent extraction, phase separation, solvent recovery, and filtration—Prior to processing, the particle size of the feed materials must be reduced, typically to at least 5 mm diameter, and the feedstock must be pumpable—To process hazardous soil or sludge, the waste is slurried and fed into the top of the extractor—The solvent (propane), condensed by compression, flows upward through the extractor—The condensed solvent contacts the waste slurry, rapidly dissolves the oils, and extracts most of the organic contaminants from the water—When extraction is complete, the clean water/solids mixture is withdrawn from the bottom of the extractor—The contaminated solvent is discharged from the top of the extractor and passed through a pressure reduction valve to a separator. In the separator, the extraction solvent is vaporized, recompressed, and recycled to the process as fresh solvent—The extracted organic contaminants are recovered from the separator for treatment in a separate process—Several stages of extraction and decanting may be required to attain a given cleanup level—Reportedly, up to 90 percent of the solvent is recycled in the system, the remaining 10 percent retains the extracted contaminants

Applications

The process can be used to remove a wide variety of organics from soils and sediments. The process was demonstrated at pilot scale for the EPA's SITE program and shown to be capable of removing PCBs from contaminated sediments. A commercial-size unit has been constructed to treat refinery sludges from a refinery in Texas.

Advantages and Disadvantages

The process offers low operating costs due to the use of inexpensive recoverable solvents. The process does not require high operating temperatures

The primary disadvantage relates to materials handling. Since the waste must be slurried before process, the process may be applicable to wastes with too broad a range of particle sizes. If larger particles are screened out prior to processing, disposal of the untreated reject material may add to process costs. Also, the process equipment may be costly because of the high operating pressures required and the design safety features needed when using a flammable solvent. In addition, uncontrolled solvent losses raise safety concerns, and controlled solvent release by flaring may require a permit.

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- US EPA September 1989 Forum on Innovative Hazardous Waste Technologies Domestic and International Atlanta, Georgia June 19-21, 1989 EPA/540/2-89/055

CHEMICAL STABILIZATION

Description

Stabilization usually involves the addition of a chemical reagent to react with the contaminant producing a less mobile or less toxic compound. It is generally used with a solidification process to immobilize a waste. Two major forms of solidification/stabilization, pozzolanic-based and cement-based, have been used extensively to treat hazardous waste (U.S. EPA 1985, 1986d).

Pozzolanic-Based This solidification method used materials that form a solid mass when mixed with hydrated lime Pozzolanic materials include diatomaceous earth, blast-furnace slag, ground brick, and some fly ashes. After mixing of the waste and pozzolan, hydrated lime is blended into the mixture. The resulting moist mixture is packed into a mold and allowed to cure.

Cement-Based Cements are often used as binding agents, along with pozzolanic materials, to improve the strength and chemical resistance of solidified waste. The types of cement used for solidification can be selected to emphasize a particular cementing reaction.

Applications

Solidification/stabilization is being used for low-level radioactive and RCRA mixed wastes at the Hanford nuclear reservation (Sferrazza 1990). After mixing the wastes with portland cement, fly ash, and clay, the cemented wastes are poured into specially constructed near-surface concrete vaults that isolate the cement product from the environment (Collins 1988). The combination of waste solidification and placement in concrete vaults is designed to contain the waste materials for at least 10,000 years.

Record of Decision (ROD) documents for at least seven Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) sites have identified solidification/stabilization as the remedial technology of choice for immobilization of heavy metal contaminants. These sites include the Selma Pressure Treating Company, CA, Flowood, MS, York Oil, NY, Chemtronics, NC, Bailey Waste Disposal, TX, Mid-State Disposal Landfill, WI, and Love Canal, NY

Various solidification/stabilization techniques have been used at DOE sites throughout the United States The 513 Solidification Unit at Lawrence Livermore National Laboratory uses cement, Envirostone[™], Petroset[™], and Aquaset[™] to solidify liquid wastes. The Los Alamos National Laboratory uses an in-drum solidification technique for immobilization of TRU solid and liquid wastes. Plutonium precipitation sludge is immobilization in-drum at Mound using portland cement. The Oak Ridge Facility uses a fly ash cement to immobilize a treatment pond sludge containing uranium, chromium, nickel, cadmium, and technetium. Portland cement is used to immobilize waste sludge in Rocky Flats pondcrete and saltcrete processes (Sferrazza 1990).

Advantages and Disadvantages

Solidification/stabilization is a well established process for reducing the mobility and toxicity of hazardous waste. Solid wastes containing radioactive contaminants are well suited for this process as it contains and reduces the mobility of the radioactive materials. Organic compounds, if present, often interfere with the desired solidification and stabilization process.

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FENTON'S REAGENT DECOMPOSITION

Description

Fenton's reagent has the ability to decompose varieties of organic compounds. Fenton's oxidation involves reaction of ferrous iron with hydrogen peroxide to generate hydroxyl radicals. The value of the reaction rate constant k is 76 L/mol-sec.

Applications

Fenton's reagent has been to shown to be effective for the remediation of PCBs/PCE-contaminated soils

Advantages and Disadvantages

A disadvantage of Fenton's reagent decomposition is the possibility of the formation of intermediate products that may need treatment

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FLUIDIZED BED INCINERATION

Description

Fluidized bed incineration uses air blown upward through the combustion zone of the incinerator to fluidize a bed of sand or other granular media. The result is a highly turbulent combustion zone with a large heat capacity. Waste material, including solids, liquids, sludges or gases, is injected directly into the fluidized bed. Volatiles are driven out of the waste and oxidized. Inerts accumulate in the fluidized bed. Bed material is occasionally drained from the fluidized bed to maintain an acceptable pressure drop across the bed. The operating temperature of the fluidized bed is limited by the softening point of the inerts in the feed material. If the operating temperature exceeds the softening point, agglomeration of bed media into particles too large to fluidized may occur. Combustion efficiency suffers when bed agglomeration occurs to an appreciable degree.

Applications

Fluidized bed incineration may be applied to organics and some inorganics in water, sludges, solids or gases. Treatment of off-gases for control of emissions is required. Wastes containing metals may require treatment of drained bed media to immobilize the metals.

The process is not applicable to wastes with low softening points. Fluidized bed incineration has a neutral effect on metals and non-volatile radionuclides, though the technology has been used for volume reduction of low level radwastes composed primarily of combustible material (such as paper or graphite). The technology is not applicable to materials containing volatile or semivolatile metals.

Advantages and Disadvantages

Fluidized bed incineration is applicable to a wide variety of organic constituents. It is a well understood, commercially available technology. The high degree of turbulence in fluidized bed incinerators allows them to achieve the same degree of combustion efficiency with lower operating temperatures. Because of this, fluidized beds frequently have lower operating costs than other incinerators under similar conditions.

The technology has a neutral effect on most inorganics. It is not applicable to volatile or semivolatile metals nor to wastes with low softening points. Operating costs are moderately high because of the power required to fluidize the bed media. Wastes with little or no heating value require addition of supplemental fuel. Pilot testing is readily accomplished through a number of vendors, but bench testing is uncommon and of guestionable value.

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- US EPA September 1989 Forum of Innovative Hazardous Waste Technologies Domestic and International Atlanta, Georgia June 19-21, 1989 EPA/540/2-89/055

GLYCOLATE DECHLORINATION

Description

Dechlorination chemically removes chlorine from chlorinated organics such as polychlorinated biphenyls (PCBs) and dioxins. Polyethylene glycol (PEG), (a sodium or potassium-based reagent), is employed by the system. This process reduces the toxicity of materials but increases the volume. Dimethyl sulfoxide (DMSO), when added to the potassium polyethylene glycol (KPEG) process, can improve the extraction of dioxin from the organic phase into the immiscible aqueous reagent phase. The reagent reacts with the chlorinated organic and displaces a chlorine molecule to produce a lower toxicity, water-soluble material. The mechanism for dechlorination research indicates that the alkali metal, potassium, is substituted for sodium in order to improve reactivity. By-products of this process include chloride salts, polymers, and occasionally heavy metals.

Typically, the mixture is heated to reduce the viscosity of the reagent. Radio frequency or microwave heating is used for in situ heating, and preheating the reagent is typically used for a removal/treatment/disposal process. In situ dechlorination should be used for uniform, shallow, soil-contaminated areas in which conventional agricultural equipment can mix the soil and reagent. If, however, the contaminated soil is deeper than 1 to 2 feet or if high concentrations are apparent, it is more suitable to excavate the soil and then dechlorinate it after it is made into a slurry. One advantage of removing the soil to dechlorinate it is that the reagent can be recovered and recycled. This will eliminate some of the cost of removal, especially if larger amounts of reagent are required to dechlorinate the waste stream.

Applications

This process can be used to treat chlorinated organic compounds such as PCBs and dioxins, chlorinated hydrocarbons, and chlorinated acids and thiols. It can be used to treat wastewater, sludges, non-aqueous liquids, and soils

Advantages and Disadvantages

This process will detoxify highly toxic compounds such as dioxins and PCBs

Treatment is limited to wastes with less than 5,000 ppm PCBs. Concentrations greater than 5% chlorinated organics require excessive volume of reagent (low ppm is optimum). High moisture content (greater than 20%) may also require excessive reagent. High humic content in soil increases reaction time. Clay and sandy soils as well as high organic content soils can be treated with increased reaction time. There is no expected effectiveness for treatment of volatile organics, non-volatile metals, and volatile metals.

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GRAVIMETRIC PHYSICAL SEPARATION (TRU CLEAN™)

Description

TRU Clean™ is a proprietary soil washing system that uses a mechanically aquitated gravimetric separator to reduce the volume of actinide-contaminated soils by concentrating the contaminants. A volume reduction of 80% has been achieved on plutonium-contaminated coral sands in a Johnson Atoll pilot plant. Volume reductions of up to 95% are projected after system improvements.

Applications

The process is applicable to soils and sludges contaminated with radionuclides TRU Clean™ can operate on-site to decontaminate soils, reducing the volume of radioactive waste

Advantages and Disadvantages

After processing, there is a volume reduction which may result in substantial cost savings in disposing of contaminated soil

The primary disadvantage is that the process is based on a proprietary soil washing system, which would have to be purchased from a single supplier

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INFRARED THERMAL TREATMENT

Description

The infrared thermal treatment process uses infrared radiation (IR, or heat) to volatilize organic constituents in a waste feed. The off-gas from the process is then treated by an afterburner and particulate and acid gas scrubbers. Different types of infrared electric furnaces are available. The type which has been most thoroughly demonstrated uses a moving woven wire belt to move the waste through a furnace. The furnace is heated by electric elements which generate radiant heat. The waste is spread on the belt in a layer approximately one inch thick. Objects fed to the infrared electric furnace should be less than two inches in diameter. Some waste materials will require pretreatment prior to feed to the furnace. In most applications, no combustion takes place in the furnace. Organics are volatilized, and possibly pyrolyzed, in the furnace and oxidized in the afterburner.

Applications

The infrared thermal treatment process is applicable to organic constituents in sludges and solids. Wastes containing large objects will require feed preparation prior to treatment in the infrared electric furnace. Because little excess air is used in the furnace, energy requirements of the infrared electric furnace are lower than for other thermal treatment technologies. Wastes containing metals may require treatment of solid residuals to immobilize the metals.

The process has a neutral effect on metals and radionuclides The technology is not applicable to materials containing volatile metals

Advantages and Disadvantages

The process is applicable to a wide variety of organic constituents. It is a developed, commercially available technology. The technology has relatively low operating costs compared with other thermal technologies because it has lower fuel consumption due to the smaller volume of off-gas generated. Off-gas cleanup costs are less in some cases because particulate carried out of the furnace is lower than other thermal technologies. The infrared electric furnace may be better suited for treatment of wastes containing semivolatile metals than other thermal methods because it operates at a lower temperature. It is likely that the infrared electric furnace may be successfully bench tested.

The technology has a neutral effect on most inorganics. It is not applicable to volatile metals. The technology may not be effective for some non-volatile or semivolatile organics.

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IN SITU VITRIFICATION

Description

In situ vitrification (ISV) involves the electric melting of contaminated soils in place. Four electrodes, placed in a square pattern and at the desired depth, are used to electrically heat and melt contaminated soils and solids at temperatures up to 2000 °C. Off-gases generated by the melting process are collected and treated prior to release. ISV breaks down organics and physically and chemically contains inorganics, heavy metals, and radionuclides.

The residuals of ISV are a monolithic, obsidian-like solid and the secondary waste from the off-gas system, which is incorporated into subsequent melts. Based on chemical and physical similarity with obsidian, durability is estimated at 18 million years. Delisting as a hazardous waste is probable and delisting as a TRU waste is possible because actinides are microencapsulated.

Application

This process is applicable to a wide variety of organic and inorganic contaminants located in the soil above the water table

ISV requires the use of off-gas processing equipment that has limits relative to the amount of heat load and the volume of gasses it can process. These limits are associated with the concentration of organics and other gas-generating materials that may be treated per unit time by the equipment. A rule-of-thumb organic concentration limit of 5 to 10 percent is used for initial application screening.

The presence of volatile metals such as mercury, makes the use of this process more complicated

Advantages and Disadvantages

This process destroys waste organic contaminants and immobilizes inorganics. The process is commercially available

Off-gasses are produced that require additional treatment

References

A Guide to Innovative Thermal Hazardous Waste Treatment Processes In Situ Vitrification Hazardous Waste Consultant November/December 1990

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MAGNETIC SEPARATION

Description

Magnetic separation removes magnetic or recovers nonmagnetic materials. Magnetic separation can be accomplished on either wet or dry wastestreams. There are several types of separators that operate at various intensities, including belt, induced-roll, and drum. The force of the magnetic field is supplied by either electromagnets or permanent magnets. Utilizing a pretreatment can artificially convert nonmagnetic materials to magnetic materials. A V-shaped pole opposite a flat bar is the preferred method for producing a converging field. Drum separators are used for low-intensity magnetic separation. There are three types of drum separators concurrent, counter-rotation, and counter-current. Concurrent drum separators extract an extremely clean magnetic concentrate from relatively coarse materials. It is often used in heavy medium recovery systems. The counter-rotation type is often utilized in roughing operations because it can handle occasional surges, hold magnetic material losses to a minimum, and can handle high solids loading. The counter-current drum separator is utilized in finishing operations. Typically, it operates on fine materials with particle sizes less than 250 μ m. Crossbelt separators are used on dry materials for low-intensity magnetic separation. This separator is used to concentrate moderately magnetic ores. A disc separator is a modified cross-belt separator that provides even greater selectivity.

Induced-roll separators are high-intensity separators. They are primarily used to separate magnetic materials from beach sands, wolframite, tin ores, glass sands, phosphate rock, and iron ores. One specific type of roll separator is the Permroll. Dry separation is utilized on materials with particles greater than 75 μ m.

Wet magnetic separators for high-intensity fields include induced roll machines and the Jones separator. One type of induced roll machine is the Gill, which has been effective for separating highly magnetic ilmenite from heavy mineral concentrates. The Jones separator is effective in separating fine hematite ores. Other applications of wet, high-intensity separators include separating magnetic particles from cassiterite concentrates, asbestos, scheelite concentrates, talc, flotation tailings, beach sand, and cyanidation residues.

Another magnetic separation process is Eddy-Current Separation Eddy currents are currents that are induced in electrically conducting particles when exposed to a changing magnetic field. The interaction between the magnetic field and eddy-currents causes a force to be exerted on a conducting particle. The magnitude of this force is dependent upon the magnetic field, the currents and the motion of the particles relative to the magnetic field. If a mixture of conducting and non-conducting particles are passed over suitable magnetic fields, a different lateral particle deflection will result in the two types of particles being separated. Two eddy-current separators are the Ramp Separator and the Linear Motor

Applications

This technology will work with any waste containing magnetic particles that can be separated. The process can be used on water, slurries, soils, sludges, and sediments

Removes particles with diameters as small as 1 micron. Flow rates are 100 times greater than ordinary filtration. When particles get below 0.5 cm, wet methods are utilized instead of dry methods. Eddy currents remove particles in the range of 1 to 4 in

Advantages and Disadvantages

This process can reduce the volume of soils requiring further processing and/or treatment

Disadvantages include the need for extensive materials handling and processing Fugitive dust emissions is also a problem

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PHYSICAL SEPARATION

Description

Soil contaminants are often found to be associated with particular size fractions of soils, most often the fine particle sizes. Fractionation of the soil based on particle size can, therefore, be an effective means of reducing the volume of the material that requires treatment. The processes effective for performing soil size fractionation include screening, classification, flotation, and gravity concentration (U.S. EPA 1988b).

Screening This process is the mechanical separation of materials based on their size. This separation is usually obtained using a uniformly perforated surface. The material is passed over the screen. The larger particles are retained on the surface and the smaller particles pass through. Screening is usually limited to particles larger than 250 μ m in diameter (Perry and Chilton 1973)

Classification This process is used to separate particles based on their settling rate in a fluid, such as water. A single stage classifier will typically make a single separation, with faster settling materials going out the underflow and the slower going out the overflow. There are three types of classifiers nonmechanical, mechanical, and hydraulic (Perry and Chilton 1973).

Flotation The injection of air into a liquid suspension can cause low-density solids and hydrocarbon solids to float to the surface for removal. This method is used extensively in the mining industry for concentration of minerals. Microbubbles formed by injection of air attach to particles, become trapped under larger particles, or become part of flocs. These particles with the attached air bubbles have a combined specific gravity less than that of water and float to the surface (Ives 1984).

Gravity Concentration This technique uses density differences of materials to effect separation. Gravity concentration can be implemented using sluices, shaking tables, and the traditional miner's pan. All of these devices keep the particles slightly apart so that they can move relative to each other and separate into layers of light and dense materials (Burt 1984)

Applications

Flotation and other physical separation techniques are used to recover copper, uranium, zirconium, and magnetite by the Palabora Mining Company in South Africa (Burt 1984). The method has also been used for removal of radium from uranium mill tailings in Elliot Lake (Raicevic 1970). During laboratory testing, flotation was found to reduce radium concentrations from 290 pCI/g to 57 pCI/g

Several soil decontamination processes in the Netherlands use gravity concentration and flotation for removal of fine particles and organics from extracting agents (Assink 1985, U S EPA 1988b) Systems

similar to this are in the pilot-stage in the United States (Hazardous Waste Consultant 1989) Pilot plant testing at Rocky Flats in the early 1970s (Garnett et al. 1980) showed that soils contaminated with 45, 284, and 7,515 pCi/g plutonium were reduced to 0.5, 12, and 86 pCi/g, respectively, using physical separation. The cleaned soil fraction ranged from 58 percent to 87 percent of the original volume

Advantages and Disadvantages

Screening is an inexpensive method for separating particles, but screens are subject to plugging, which can greatly decrease their efficiencies. The use of dry screening generates dust emissions that must be controlled.

Classifiers have high continuous processing capabilities and are very reliable, but soils containing clay or sandy soils containing humus materials can be difficult to process

Flotation can achieve very high separation rates if the materials are suited to such treatment, but it is a complex and expensive process

Gravity concentration is a highly efficient and well proven technique, but it has a relatively low process capacity

Wet processes may produce a liquid waste stream requiring treatment or disposal

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POLYMERIZATION-POLYETHYLENE

Description

This process consists of mixing the waste with the liquid polyethylene (a thermoplastic) and allowing it to cool. This can be accomplished using several techniques including batch mixing and extrusion processing. Polyethylene is an organic polymer material of crystalline-amorphous structure, generally categorized as low, medium, or high density. Low density polyethylene (LPDE) is preferred over high density because of the ease of processibility.

Applications

This process is used to treat low level radioactively contaminated wastes. It can be used to treat sediment, soils, sludges, and slurries

Advantages and Disadvantages

The process reduces the mobility of contaminants, but does not remove or destroy them

The process results in increased volume of contaminant

References

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ROTARY KILN INCINERATION

Description

A rotary kiln consists of an inclined, refractory lined, hollow cylinder which is rotated around its axis by an external drive mechanism. Material is fed into the kiln at the high end. The rotation of the kiln mixes the solids in the kiln and causes the solids to migrate to the low end of the kiln where they are removed. Rotary kilns are available in a variety of configurations, depending on the application and the nature of the feed material. Kilns may be fired co-currently (gas flow in the same direction as solids feed) or countercurrently. Operating temperatures may range from 1,400 to 2,000 degrees Fahrenheit for a normal operation, or from 2,200 to 2,500 degrees Fahrenheit for a slagging kiln. Combustion air and fuel (if required) are fed into one end of the kiln and off-gas is recovered from the other end. The off-gas requires treatment for control of emissions.

Applications

Rotary kiln incineration is applicable to organic constituents in a variety of waste matrices, including liquids, sludges and slurries, solids and gases. Slagging rotary kilns are applicable to solids with low softening point temperatures. Rotary kilns may be fired countercurrently to increase combustion zone turbulence, or co-currently to reduce particulate emissions. Some rotary kiln applications may require an afterburner in addition to off-gas treatment. Wastes containing metals may require treatment of solid residuals to immobilize the metals.

Rotary kiln incineration has a neutral effect on metals and non-volatile radionuclides. The technology is not applicable to materials containing volatile or semivolatile metals.

Advantages and Disadvantages

Rotary kiln incineration is applicable to a wide variety of organic constituents. It is a well understood, commercially available technology. Rotary kilns may be adapted for use with a wide variety of waste types.

The technology has a neutral effect on most inorganics. It is not applicable to volatile or semivolatile metals not to wastes with low softening points. Operating costs are moderately high because wastes with little or no heating value require addition of supplemental fuel. Pilot testing is readily accomplished through a number of vendors, but bench testing is uncommon and of questionable value.

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SLURRY PHASE BIOREACTOR

Description

This is a biological remediation process in which contaminated soils and/or sediments are mixed with water to form a slurry. This is done in an agitated reaction tank. Nutrient and air are added to the tank as necessary to facilitate the biological reactions.

After the contaminants have been destroyed, the slurry is pumped out of the reactor and sent to dewatering equipment. The remediated soil/sediment can be returned to the site. Water removed during the dewatering step can be reused for the next batch or sent to a treatment system.

Application

This process is applicable to soils and/or sediments that are contaminated with biodegradable organic compounds. The process could be operated either aerobically or anaerobically.

The process would not be effective for metals and radionuclides

Advantages and Disadvantages

The process destroys the toxic contaminants, converting them into carbon dioxide, methane, water, and biomass

This technology requires a considerable amount of materials handling equipment and solids dewatering equipment. Its potential economic advantage would only be realized if high initial concentrations of contaminants were present.

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SOIL WASHING

Description

Soil washing is based on the principle of contaminant removal from soil by washing with a solution Washing agents can include water, acids, surfactants, solvents, or chelating agents. Contaminated soil is excavated and placed in a reactor for mixing with the extracting solution. Sorbed contaminants are transferred to the liquid phase by dissolving, by forming an emulsion, or by a chemical reaction with the solution. When extraction is complete, the soil particles are physically separated from the solution, and the treated soil can be returned to the excavation. The extractant containing the contaminants requires further treatment for recycling or disposal.

Applications

By selecting the appropriate washing solution, soil washing technology can potentially be used to treat inorganics, metals, organics, or radionuclides in soil. Application of a soil washing reactor system at four sites in the Netherlands demonstrated greater than 80 percent removal efficiencies for polynuclear aromatic hydrocarbons (PNAs), cyanides, heavy metals, mineral oil, and halogenated hydrocarbons (Assink 1985). Soil structure and chemistry are important variables in applying the technology successfully and require evaluation on a site-by-site basis.

Inorganics that can be washed from soil with water include soluble salts such as carbonates of nickel, zinc, and copper. Dilute solutions of sulfuric, hydrochloric, nitric, phosphoric, and carbonic acid have been widely used in industry to extract metal ions by dissolving basic metal salts including hydroxides, oxides, and carbonates. Heavy metals can be removed from soils by complexing and chelating agents such as citric acid, ethylenediaminetetraacetic acid (EDTA), and diethylenetriaminepentaacetic acid (DTPA) (U.S. EPA 1985, 1987c). Arsenic and selenium removal can be enhanced with the addition of oxidizers such as hydrogen peroxide (U.S. EPA 1986a).

Organics that can be removed from soil by water washing include low to medium molecular weight aldehydes, ketones, and aromatics and lower molecular weight hydrocarbons such as trichloroethylene and tetrachloroethylene. Other basic organic groups like amines, ethers, and anilines can be flushed from soil by washing with an acidic solution. Surfactants have been employed to enhance the recovery of petroleum products and PCBs (U.S. EPA 1985). Removal of organochlorine compounds by extraction with a solvent mixture o toluene, kerosene, and octanol was demonstrated in laboratory experiments on sludges from Rock' Mountain Arsenal (A.D. Little 1988).

The use of water, inorganic salts, mineral acids, and complexing reagents to extract radionuclides from soils and tailings was reviewed by the EPA (U.S. EPA 1988b). These extraction techniques have been applied as bench-scale or pilot-plant testing for removal of radium and thorium but have not been

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implemented for remediation of a radiologically contaminated site. Water was shown to be ineffective, removing only 10 percent of the radium and virtually none of the thorium from soils tested. Inorganic salt solutions, mineral acids, and complexing reagents all showed high removal percentages in some applications (U.S. EPA 1988b).

Advantages and Disadvantages

The primary advantage of soil washing is that a variety of types of contaminants can potentially be removed from soils in a reactor under relatively controlled conditions. The process is flexible and can be designed for specific mixtures of contaminants, although treatment of mixtures may require multiple stages using different washing solutions.

Contaminants are not destroyed but are transferred to the aqueous phase. The technology requires a subsequent separation process for liquids and solids and treatment of the resulting solution for recycling or disposal. Soil washing may require the addition of potentially hazardous substances as washing agents. Residual soil washing chemicals remaining in the soil may also be a problem.

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SOLAR

Description

A system that uses solar energy to destroy hazardous organic wastes is being developed by VEDA Inc of Alexandria, Virginia. The heart of this system is an array of sun-tracking mirrors as heliostats, referred to as a unified heliostat array. Each heliostat concentrates and reflects the sun's radiant energy to a windowed reactor vessel. The heat and UV radiation provided by the unified heliostat array are used to destroy the organic contaminants.

A system for processing PCB or dioxin contaminated soil includes a desorption reactor, which heats the soil to 750°F. The high temperature vaporizes the organic contaminants from the soil. The heat for the desorption reactor is provided by cooling air from the windowed reactor.

The vaporized contaminants from the desorption reactor are injected into the windowed reactor where they are irradiated through a quartz window with concentrated solar energy from the unified heliostat array. The reactor temperature is maintained at 1,300°F (700°C) and is controlled by air flow around the reactor's ceramic liner. Inside the windowed reactor, organic compounds are decomposed by the high temperature and UV radiation. Some of the resulting exhaust gas is recirculated through the desorption reactor to provide additional heat needed to raise the temperature of the contaminated soil. The remainder of the exhaust gas is treated in a scrubber to remove hydrogen chloride, sulfur dioxide, and particulates before it is discharged to the atmosphere.

Applications

This process is applicable to soils and sediments that are contaminated with volatile and semivolatile organics. The process may also be applied to aqueous streams

Advantages and Disadvantages

The process offers high destruction efficiencies for organic contaminants
Efficiencies as high as 99 9999% have been achieved

The system is not commercially available. However, a prototype system designed to process 500 pounds of contaminated soil per hour is being developed. Additional research is in progress to determine the temperature and condition necessary to volatilize and desorb PCBs and dioxins from soil

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SOLIDIFICATION/STABILIZATION TECHNOLOGIES

Description

Solidification is a process that mechanically binds contaminants to the solidification agents to reduce the contaminant mobility. The process produces a solid matrix of waste with high structural integrity. Stabilization usually involves the addition of a chemical reagent to react with the contaminant producing a less mobile or less toxic compound. Solidification and stabilization are usually used together to immobilize a waste. Two major forms of solidification/stabilization, pozzolanic-based and cement-based, have been used extensively to treat hazardous waste (U.S. EPA 1985, 1986d). More innovative solidification/stabilization technologies include mixing with organic polymers and asphalt

Pozzolanic-Based This solidification method uses materials that form a solid mass when mixed with hydrated lime Pozzolanic materials include diatomaceous earth, blast-furnace slag, ground brick, and some fly ashes After mixing of the waste and pozzolan, hydrated lime is blended into the mixture. The resulting moist mixture is packed into a mold and allowed to cure

Cement-Based Cements are often used as binding agents, along with pozzolanic materials, to improve the strength and chemical resistance of solidified waste. The types of cement used for solidification can be selected to emphasize a particular cementing reaction. Portland cement has been commonly applied to stabilization of metals. Masonry cement has been tested for stabilization of radionuclides.

Polymer Based Various organic polymers to produce a stable matrix for stabilizing and solidification of wastes. This method is innovative. Polymer materials which have been applied include epoxies and polyesters.

Asphalt Based The waste may be stabilized by mixing with bitumen a mixture of high molecular weight asphaltene and malthene hydrocarbons

Applications

Solidification/stabilization is being used for low-level radioactive and RCRA mixed wastes at the Hanford nuclear reservation (Sferrazza 1990). After mixing the wastes with portland cement, fly ash, and clay, the cemented wastes are poured into specially constructed near-surface concrete vaults that isolate the cement product from the environment (Collins 1988). The combination of waste solidification and placement in concrete vaults is designed to contain the waste materials for at least 10,000 years.

Record of Decision (ROD) documents for at least seven Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) sites have identified solidification/stabilization as the remedial technology of choice for immobilization of heavy metal contaminants. These sites include the Selma Pressure Treating Company, CA, Flowood, MS, York Oil, NY, Chemtronics, NC, Bailey Waste Disposal, TX, Mid-State Disposal Landfill, WI, and Love Canal, NY

Various solidification/stabilization techniques have been used at DOE sites throughout the United States The 513 Solidification Unit at Lawrence Livermore National Laboratory uses cement, Envirostone[™], Petroset[™], and Aquaset[™] to solidify liquid wastes. The Los Alamos National Laboratory uses an in-drum solidification technique for immobilization of TRU solid and liquid wastes. Plutonium precipitation sludge is immobilized in-drum at Mound using portland cement. The Oak Ridge Facility uses a fly ash cement to immobilize a treatment pond sludge containing uranium, chromium, nickel, cadmium, and technetium. Portland cement is used to immobilize waste sludge in Rocky Flats pondcrete and saltcrete processes (Sferrazza 1990)

Advantages and Disadvantages

Solidification/stabilization is a well established process for reducing the mobility and toxicity of hazardous wastes. Solid wastes containing radioactive contaminants are well suited for this process as it contains and reduces the mobility of the radioactive materials. Solidification/stabilization processes increase the volume of the treated wastes. Organic compounds, if present, often interfere with the desired solidification and stabilization process.

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SURFACTANT WASHING

Description

Surfactant washing is based on the principle of contaminant removal from soil by washing with a surfactant solution. Contaminated soil is excavated and placed in a reactor for mixing with the solution. The surfactant, which is soluble in both the contaminant and water, removes the contaminant from the soil and transfers it to the solution.

When the washing process is complete, the soil particles are physically separated from the solution, and the treated soil can be returned to the excavation

Applications

This process has been used to treat soil contaminated with petroleum products, organics, and PCBs

Advantages and Disadvantages

This may be a cost effective method to reduce the volume of contaminated material into a small volume of liquid. This technology is still at the innovative stage of development

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VITRIFICATION

Description

Vitrification of wastes involves combining the wastes with molten glass at a temperature of 1,350°C or greater. However, the encapsulation might be done at temperatures significantly below 1,350°C (a simple glass polymer such as boric acid can be poured at 850°C). This melt is then cooled into a stable, noncrystalline solid (U.S. EPA 1985).

One variation on this process is in situ vitrification (ISV) in which wastes and soils or sludges are melted in-place to bind the waste in a glassy, solid matrix resistant to leaching. In the ISV process, four electrodes are inserted into the soil to the desired depth. A glass frit is placed between the electrodes to act as a starter path for the initial melt to form. As the melt grows downward and outward, it incorporates non-volatile elements and destroys organic components by pyrolysis. The pyrolyzed by-products migrate to the surface of the melted zone where they combust in the presence of oxygen linerganic materials are dissolved into or are encapsulated in the melt. Convective currents within the melt uniformly mix materials that are present in the soil. When the electric current ceases, the molten volume cools and solidifies into a vitrified mass. A hood placed over the processing area provides confinement for the combustion gases, drawing the gases into an off-gas treatment system.

Applications

Vitrification is best used for soils with a high concentration of contaminants or with contaminants that must be completely immobilized (such as radioactive species). To be considered for vitrification, the wastes should be either stable or totally destroyed at the process temperature (U.S. EPA 1985).

In situ vitrification will work with fully saturated soils, however, the water in the soil must be evaporated before the soil will begin to melt. Soils with permeabilities greater than 10⁻⁴ cm/sec are difficult to vitrify in the presence of flowing groundwater and, therefore, some type of groundwater diversion may be necessary. If buried metals, such as drums, occupy over 90 percent of the linear distance between electrodes, a conduction path that leads to electrical shorting between electrodes may result

Several vitrification facilities for treatment of radioactive wastes are currently under development. The Hanford Waste Vitrification Plant is designed to fuse high-level radioactive mixed wastes into a glass product. The facility was expected to be completed by mid-1991. The Defense Waste Processing Facility will use vitrification for the immobilization of high-level waste from the Savannah River Site. This facility is almost complete, with cold testing scheduled for September 1990 and hot start-up planned for January 1992. The West Valley Nuclear Services Co. has constructed a vitrification system as part of the West Valley Demonstration Project. The vitrification system has completed a 5-year period of testing.

using simulated wastes and is currently being renovated. West Valley is preparing a Part A Radioactive Mixed Hazardous Waste permit for the facility (Sferrazza 1990).

The Idaho National Engineering Laboratory is evaluating the feasibility of using in situ vitrification for treatment of buried wastes at this facility. The process has undergone laboratory and engineering scale tests at the Pacific Northwest Laboratory, where the equipment was developed, and has been applied once at the Idaho National Engineering Laboratory on a small test area. Starting in 1992, three larger scale tests are planned (Sferrazza 1990)

Advantages and Disadvantages

The primary advantage of vitrification is that it effectively immobilizes non-volatile species in a solid that is very durable and resistant to leaching. Disadvantages of this technology are related to its high cost, which is the result of the large amount of power that is required to melt the glass or soil and the need for specialized equipment and trained personnel (U.S. EPA 1985). The presence of high moisture content or high organics may also hinder operation. Significant concentrations of combustible gases may also produce a safety hazard. This process may need an off-gas collection and treatment system for volatile and semivolatile organics and volatile metals.

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WET AIR OXIDATION

Description

Wet air oxidation is a thermal treatment technology that breaks down (by oxidation) suspended and dissolved inorganic and organic materials in a high-temperature, high-pressure, aqueous environment. Waste is combined with compressed air (the oxidizing agent), passes through the cold side of the heat exchanger, and enters a reactor where exothermic reactions elevate the temperature and pressure of the mixture to a desired value. Oxygen in the air reacts with oxidizable material in the waste. In the heat exchanger, the raw waste and air mixture is heated to reaction conditions by an indirect heat exchange with the hot-oxidized effluent. In cases where the heat of reaction is insufficient to maintain the design operating temperature, additional heat may be necessary.

After exiting the reactor, the waste air mixture enters the heat up side of the heat exchanger and is directed to the separator. The spent process vapors (noncondensible gasses) are separated from the oxidized liquid phase and are directed into a two-stage water scrubber-carbon bed absorber, vapor treatment system.

Organic substances are oxidized to yield highly oxygenated products and water. Organic carbon-hydrogen compounds oxidize to carbon dioxide and water, organic sulfur compounds and inorganic sulfides oxidize to inorganic sulfate, inorganic and organic cyanides oxidize to carbon dioxide, ammonia, or molecular nitrogen. Nitrogen oxides such as NO or NO₂ are not formed in wet air oxidation because reaction temperatures are not high enough.

The process has been tested on phenolic wastes, organic sulfur wastes, general organic wastes, cyanide wastes, pesticide wastes, and solvent still-bottom wastes. Operating condition ranges are 175-600 C, and 2-200 atm. Catalysts may be used to enhance oxidation, especially of chlorinated aromatics. The oxidation reaction is usually self-sustaining due to the exothermic oxidation reactions. Wet air oxidation is a very specialized process not currently used on hazardous wastes to any great extent. However, it has been used commercially to regenerate spent powdered carbon from biological treatment systems.

Applications

The process is applicable to organics, including phenolic and organic sulfur wastes, petroleum refinery spent caustic wastewater, cyanide waste, pesticide waste, solvent still-bottoms waste, and general organic waste. Contaminants treated by the Zimpro/Passavant (vendor) process include inorganic and organic cyanides, aliphatic and chlorinated aliphatic compounds, and aromatic and halogenated aromatic compounds.

Advantages and Disadvantages

A primary advantage of this process is that it destroys the applicable contaminants rendering them harmless to the environment. It is effective on a wide range of contaminants and may offer economic advantages in specific cases.

The process is complex and requires high operating temperatures and pressures Expensive equipment is required, as well as highly trained operators

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APPENDIX D STATEMENTS OF WORK FOR TECHNOLOGIES SELECTED FOR TREATABILITY TESTS

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OZONATION

Introduction

This statement of work covers the bench-scale testing of the Ozonation process to destroy PCBs in surface water at RFP. The review of existing site characterization data indicates the concentration of the PCB Aroclor-1254 exceeds ARARs for surface water at two or more OUs. This species is potentially amenable to treatment by oxidation using ozone. Treatability testing will be performed on site at the RFP or at an off-site laboratory possessing the necessary licenses, approvals, and notifications to perform hazardous waste treatability studies.

Test Objectives

The primary objective of this testing will be to evaluate the effectiveness of the ozone oxidation process for destruction of PCBs in water. The test will evaluate the percent destruction of PCBs which can be achieved in comparison to the likely effluent concentration which would be required for discharge of treated waters to surface water or to a sewage treatment system. The dependence of destruction efficiency on ozone dose, residence time and vessel configuration and mixing properties will be investigated.

Test Approach

The test program will use a small bench scale oxidation reactor to run batch tests on samples of PCB contaminated water. Ozone will be used as the oxidant at a number of different concentrations. Tests will be run at different mixing conditions. The water will be sampled at the start of the test and at multiple time intervals during the course of the test. These samples will be chemically analyzed to determine PCB destruction and the presence of any intermediates.

POTASSIUM FERRATE PRECIPITATION

Introduction

This statement of work covers the bench-scale testing of the Potassium Ferrate Precipitation (TRU/ClearTM) process to remove radionuclides from surface water and groundwater at RFP TRU/ClearTM is the brand name for a proprietary precipitating agent based on the use of ferrate ions. The review of existing site data indicate that total gross alpha emitters such as uranium, plutonium, and americium are present in groundwaters and surface waters at RFP in concentrations which exceed possible action levels. All of these species are potentially amenable to treatment using TRU/ClearTM. Treatability testing will be performed on site at the RFP or at an off-site laboratory possessing the necessary licenses, approvals, and notifications to perform hazardous waste treatability studies and handle radioactive materials.

Test Objectives

The primary objective of this testing will be to evaluate the effectiveness of the use of TRU/Clear[™] in removal of radionuclides from water. The tests will also have the objective of establishing the correct dosage and operating pH for the use of TRU/Clear[™] and to determine the removal efficiencies which can be obtained by a combination of addition of TRU/Clear[™] with either solids settling or filtration

Test Approach

The test program will use small bench scale tests to remove the radionuclides using TRU/Clear Initial testing will involve multiple jar tests using different dosages of TRU/Clear at a number of different pH levels. In one round of tests the solids will be allowed to settle and the supernatant water analyzed for radionuclides to determine removal efficiencies. In a second round, of tests the samples will be filtered and the filtered water analyzed for radionuclides again to determine removal efficiencies. The most effective operating conditions for the TRU/Clear process will be established in this fashion

SLURRY PHASE BIOREACTOR

Introduction

This statement of work covers the pilot-scale testing of the slurry phase bioreactor process to destroy PCBs in soils at RFP. The review of existing site characterization data indicates the concentration of the PCB Aroclor-1254 exceeds ARARs for soils at two or more OUs. This species is potentially amenable to treatment by biological degradation using slurry phase bioreactors. Treatability testing will be performed on site at the RFP or at an off-site laboratory possessing the necessary licenses, approvals, and notifications to perform hazardous waste treatability studies.

Test Objectives

The primary objective of this testing will be to evaluate the effectiveness of the slurry phase biological process for destruction of PCBs in soil. The test will evaluate the percent destruction of PCBs which can be achieved in comparison to the likely cleanup levels for placement of the soil back on site or disposal at a landfill. Aerobic and anaerobic biological processing will likely be investigated. The dependence of destruction efficiency on nutrient and oxygen addition, residence time and vessel configuration and mixing properties will be investigated.

Test Approach

The test program will use a pilot scale biological reactors to run tests on samples of PCB contaminated soil. Tests will be run under aerobic and anaerobic conditions at different levels of nutrient addition and mixing conditions. The soil will be sampled at the start of the test and at multiple time intervals during the course of the test. These samples will be chemically analyzed to determine PCB destruction and the presence of any intermediates.

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ULTRAVIOLET OXIDATION

Introduction

This statement of work covers the bench-scale testing of the UV Oxidation process to destroy PCBs in surface water at RFP. The review of existing site characterization data indicates the concentration of the PCB Aroclor-1254 exceeds ARARs for surface water at two or more OUs. This species is potentially amenable to treatment by UV oxidation. Treatability testing will be performed on site at the RFP or at an off-site laboratory possessing the necessary licenses, approvals, and notifications to perform hazardous waste treatability studies.

Test Objectives

The primary objective of this testing will be to evaluate the effectiveness of the UV oxidation process for destruction of PCBs in water. The test will evaluate the percent destruction of PCBs which can be achieved in comparison to the likely effluent concentration which would be required for discharge of treated waters to surface water or to a sewage treatment system. The use of the potential oxidation agents hydrogen peroxide and ozone will be investigated and the dependence of oxidizing agent dose on destruction efficiency will be investigated. The removal efficiency dependency on UV wavelength and intensity will be investigated as well as the dependence on residence time and vessel configuration and mixing properties. The potential for fouling of the UV lamp will be investigated as well as the formation of toxic intermediates.

Test Approach

The test program will use a small bench scale UV photolysis reactor to run batch tests on samples of PCB contaminated water. Hydrogen peroxide and ozone will be used as oxidants at a number of different concentrations. Tests will be run at varying UV wavelengths and intensities and under different conditions of mixing. The water will be sampled at the start of the test and at multiple time intervals during the course of the test. These samples will be chemically analyzed to determine PCB destruction and the presence of any intermediates.

ULTRAVIOLET PHOTOLYSIS

Introduction

This statement of work covers the bench-scale testing of the UV photolysis process to destroy PCBs in surface water at RFP. The review of existing site characterization data indicates the concentration of the PCB Aroclor-1254 exceeds ARARs for surface water at two or more OUs. This species is potentially amenable to treatment by UV photolysis. Treatability testing will be performed on site at the RFP or at an off-site laboratory possessing the necessary licenses, approvals, and notifications to perform hazardous waste treatability studies.

Test Objectives

The primary objective of this testing will be to evaluate the effectiveness of the UV photolysis process for destruction of PCBs in water. The test will evaluate the percent destruction of PCBs which can be achieved in comparison to the likely effluent concentration which would be required for discharge of treated waters to surface water or to a sewage treatment system. The removal efficiency dependency on UV wavelength and intensity will be investigated as well as the dependence on residence time and vessel configuration and mixing properties. The potential for fouling of the UV lamp will be investigated as well as the formation of toxic intermediates.

Test Approach

The test program will use a small bench scale UV photolysis reactor to run batch tests on samples of PCB contaminated water. Tests will be run at varying UV wavelengths and intensities and under different conditions of mixing. The water will be sampled at the start of the test and at multiple time intervals during the course of the test. These samples will be chemically analyzed to determine PCB destruction and the presence of any intermediates.